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Supporting Information

2 MoSe₂/SWNT core–shell hybrids with space-charge-limited conduction 3 and nonlinear dynamics for in-materio reservoir computing

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13 **S1. Fabrication of a 16-electrode device**

14 **S1.1. Electrode patterning**

15 The 16-electrode device was fabricated on a silicon/silicon dioxide (Si/SiO₂) substrate. The device
16 consists of 16 square aluminum (Al) electrodes arranged in a pattern (as shown in **Figure 1**), with
17 a maximum opposing gap size of 100 μ m. The electrodes were patterned using a standard
18 photolithography and lift-off process. This process begins with substrate cleaning, in which the
19 Si/SiO₂ substrate was sequentially cleaned in an ultrasonic bath of isopropyl alcohol (IPA) and DI
20 water, each for 3 minutes, and then dried. Then, the resist was coated, in which a bi-layer resist
21 was prepared for the lift-off process. First, a lift-off resist (LOR-10A) was spin-coated onto the
22 substrate at 3,000 rpm for 50 s and baked on a hot plate at 180 °C for 5 minutes. Subsequently, a
23 photoresist (S18186) was spin-coated on top at 4,000 rpm for 2 s and baked at 90 °C for 3 minutes.
24 After this patterning was achieved by using a chromium photomask with the electrode pattern
25 placed over the substrate. The device was then exposed to UV light for 10 s at an intensity of 19
26 mW/cm² using a mask aligner. The exposed resist was developed in an MF-319 developer for 90
27 s, rinsed with DI water, and hard-baked at 120 °C for 5 minutes to define the pattern. Then,
28 metallization and lift-off were performed, in which a 50 nm layer of aluminum (Al) was deposited
29 over the substrate via sputtering at a base pressure of 10⁻⁵ Torr. The lift-off was then performed by
30 submerging the substrate in a dimethyl sulfoxide (DMSO) bath at 60 °C for 30 minutes. This step
31 dissolves the underlying LOR and removes the excess metal. Finally, the completed electrode array
32 was rinsed with IPA and DI water and dried, resulting in the patterned device.

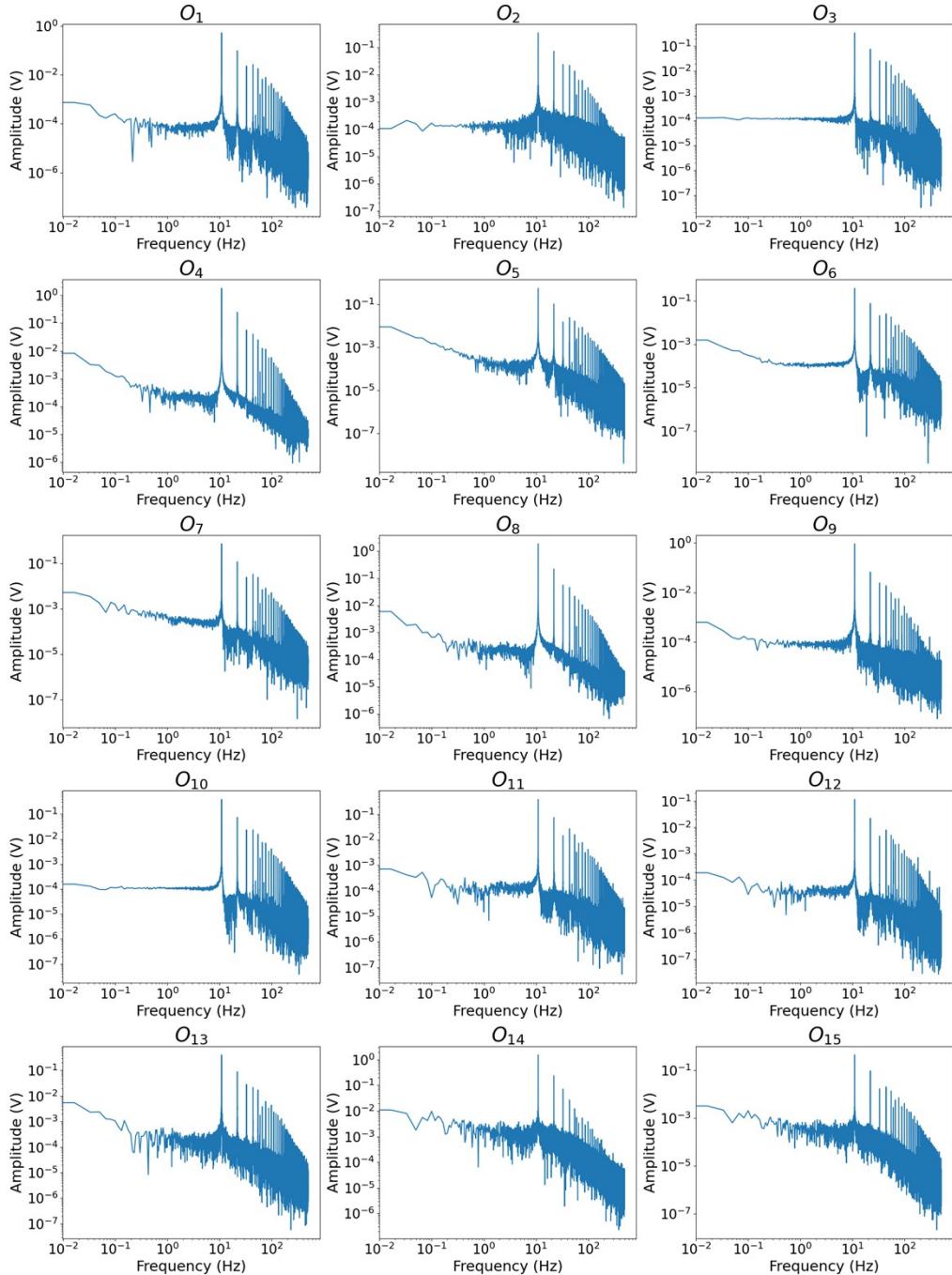
33 **S1.2. Material Deposition and Device Packaging**

34 The synthesized MoSe₂/SWNT composite powder (with SWNT loadings of 1, 5, and 10 mg) was
35 dispersed in ethanol to create a suspension with a concentration of 40 mg/mL. The suspension was

36 then homogenized via ultrasonication for 10 minutes. The active material was deposited by drop-
37 casting three 1 μ L drops (approximately 3 μ L total volume) from a micropipette onto the central
38 100 μ m gap of the electrode array. During this process, the substrate was held on a hot plate at 70
39 $^{\circ}$ C to facilitate controlled solvent evaporation. After the material was fully dried, the Si/SiO₂ chip
40 was mounted onto a custom-designed printed circuit board (PCB). Electrical connections from the
41 16 aluminum electrode pads to the corresponding PCB contacts were then established using silver
42 paste for wire bonding. The fully packaged device was then ready for electrical characterization
43 and reservoir computing experiments.

44 **S2. FFT Analysis and High-Dimensional Representation**

FFT of Output Signals O_1 to O_{15}



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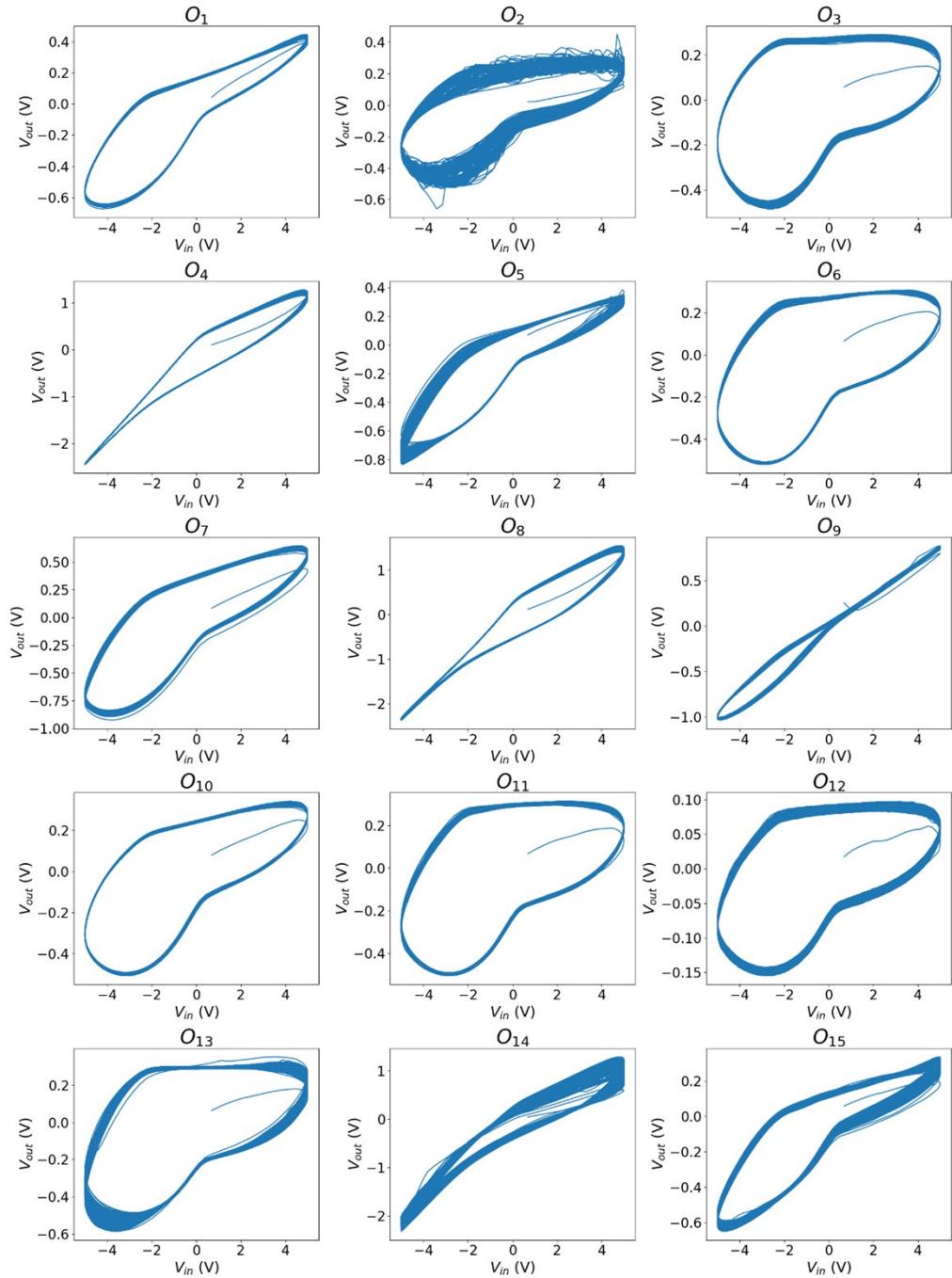
46 **Figure S1.** FFT amplitude spectra of the 15 device output signals O_1 to O_{15} obtained under an 11 Hz sinusoidal input voltage. The
 47 spectra exhibit pronounced peaks at the fundamental frequency of 11 Hz and at higher harmonic frequencies such as 22 Hz and 33
 48 Hz. The generation of these integer multiples confirms the nonlinear dynamical response of the MoSe₂/SWNT reservoir.

49 FFT analysis of the device outputs clearly shows pronounced peaks at the fundamental and
50 harmonic frequencies as shown in **Figure S2**. By feeding a sine wave with a fundamental
51 frequency of 11 Hz into the device, we observed its output through FFT analysis which revealed
52 the presence of harmonics at integer multiples of the input frequency such as 22 Hz and 33 Hz.
53 This harmonic generation indicates nonlinearity in the device response which is a desirable
54 characteristic for effective reservoir computing³⁻⁵. The raw input and output signals used for this
55 analysis are provided in **Figure S4**. Across the output signals (O_1 to O_{15}), significant peaks appear
56 at the fundamental frequency and its harmonics, which aligns with the device's demonstrated
57 ability to generate accurate representations of complex waveforms. The amplitude spectrum
58 reveals a concentration of energy at harmonic frequencies, indicating that the device is introducing
59 nonlinear transformations to the input signals. These transformations, driven by the device's
60 nonlinear behavior, are critical for mapping the input signals into a higher-dimensional space. In
61 the context of waveform reconstruction, this harmonic content is particularly important. For
62 instance, the successful regression results for waveforms such as the triangle and square waves,
63 which are rich in harmonic content, are reflected in the pronounced harmonic peaks in the FFT
64 plots. This suggests that the device can capture the essential harmonic components that define
65 these waveforms, further confirming its role as a nonlinear reservoir. The FFT analysis also
66 provides insight into the device's ability to handle signals composed of higher-order harmonics,
67 such as $\text{Sin}2\omega$ and $\text{Sin}3\omega$. While higher harmonics typically introduce more spectral complexity,
68 the device demonstrated strong regression performance for both cases. Notably, in the $\text{Sin}3\omega$ case,
69 where more complex harmonic content is present, the FFT plots still reveal well-defined peaks
70 with limited degradation in harmonic amplitude. This is consistent with the observed regression
71 accuracy of 95.1%, indicating that the device maintains sufficient precision even at higher

72 harmonic orders. Overall, the FFT results support the conclusion that the device not only
73 transforms input signals nonlinearly but does so in a way that retains essential spectral features
74 critical for accurate waveform reconstruction.

75 **S3. Lissajous Plots and Nonlinear Dynamics**

Lissajous Plots: Output Signals O_1 to O_{15}



76

77 **Figure S2.** Lissajous plots of all 15 outputs from the device showing asymmetric and hysteresis shape suggesting rich non-linearity

78 and phase shifts

79 The Lissajous plots, depicted in the attached figures, provide a clear visualization of the nonlinear
80 relationship between the input and output signals of the MoSe₂/SWNT core-shell device. These
81 plots were generated by plotting the output voltage (V_{out}) against the input voltage (V_{in}) for each
82 of the device's output channels (O_1 to O_{15}) as shown in **Figure S3**. The resulting shapes,
83 predominantly asymmetrical ellipses, are indicative of phase shifts and nonlinear dynamics
84 introduced by the device. The elliptical shapes seen in the Lissajous plots typically emerge when
85 the input and output signals share the same frequency, but the asymmetry of these ellipses reveals
86 that the device is introducing significant phase shifts and nonlinear transformations to the input
87 signal. This is a direct consequence of the nonlinearities in the device, which are essential for the
88 reservoir computing framework. Nonlinear transformations enrich the dynamics of the system,
89 enabling the reservoir to map input signals into a high-dimensional space, facilitating the
90 separation and classification of complex patterns.

91 The Lissajous plots vary across different output signals, with some displaying more pronounced
92 asymmetry (e.g., O_2 , O_5 , O_{11}) while others exhibit tighter, more elliptical shapes. These variations
93 reflect the device's ability to apply different degrees of phase shifts and nonlinear modifications
94 depending on the specific output channel. For example, output O_2 shows a highly irregular and
95 overlapping Lissajous figure, suggesting that the device has introduced a significant nonlinear
96 distortion to the input. In contrast, outputs like O_1 and O_3 maintain a clearer elliptical shape with
97 slight asymmetry, indicating more moderate nonlinear transformations.

98 These asymmetrical elliptical shapes are critical for reservoir computing applications. The
99 nonlinearity they represent ensures that the input signal is transformed into a rich, high-
100 dimensional representation, which is necessary for the system to perform tasks such as pattern
101 recognition and time-series prediction. The phase shifts alter the orientation and size of the

102 Lissajous figures, further emphasizing the device's capability to introduce complex dynamics.
103 These dynamics, captured in the Lissajous plots, provide a visual confirmation of the nonlinear
104 behavior observed in both the FFT analysis and waveform reconstruction tasks discussed
105 previously.

106 **S4. Total harmonic distortion**

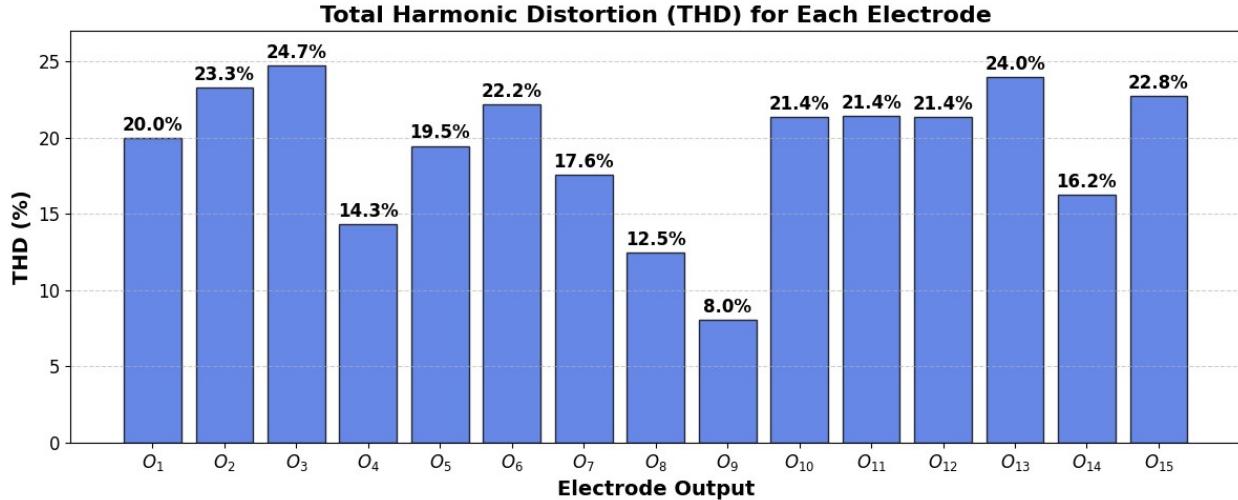
107 Total Harmonic Distortion (THD) is another metric for quantifying the nonlinearity of a reservoir
108 computing system, particularly in physical implementations where the reservoir transformation is
109 governed by material properties^{1,2}. In an ideal linear system, a pure sinusoidal input should only
110 contain its fundamental frequency. However, a nonlinear system such as a memristive reservoir
111 naturally generates higher harmonics at integer multiples of the input frequency. The degree of
112 harmonic generation is quantified by THD, defined as:

$$113 \quad THD = \frac{\sqrt{A_2^2 + A_3^2 + A_4^2 + \dots + A_{15}^2}}{A_1} \quad \#(11)$$

114

115 where A_1 is the amplitude of the fundamental frequency, and $[A_2, A_3, A_4, \dots, A_{15}]$ represent the
116 amplitudes of the harmonic components. In the context of waveform reconstruction, THD provides
117 insight into how the reservoir expands the input signal into a richer feature space, enabling the
118 readout layer to synthesize complex waveforms from a single sinusoidal input. This is linked to
119 Fourier series decomposition, where any periodic function can be represented as a sum of sinusoids
120 at different frequencies. Since many target waveforms (e.g., triangle, square, and sawtooth waves)
121 require specific harmonic components as from equations (12) – (15), the ability of the reservoir to
122 generate these harmonics is crucial for achieving high reconstruction accuracy. Figure S3 presents
123 the measured THD across the 15 output electrodes, revealing a heterogeneous nonlinearity
124 distribution with values spanning from 8.0% O₉ to 24.7% O₃. This variation indicates that different
125 nodes within the reservoir provide diverse harmonic components, rather than a uniform
126 transformation. By correlating THD with waveform reconstruction performance, as shown in
127 **Figure S3**, we demonstrate that the memristive reservoir not only exhibits strong nonlinear

128 transformation capabilities but also provides an effective basis for encoding diverse time-series
 129 signals.



131 **Figure S3.** Total harmonic distortion of all 15 outputs of the reservoir.

132 $\text{Cosine wave } f(x) = \sin\left(\frac{\pi}{2} - x\right) \#(12)$

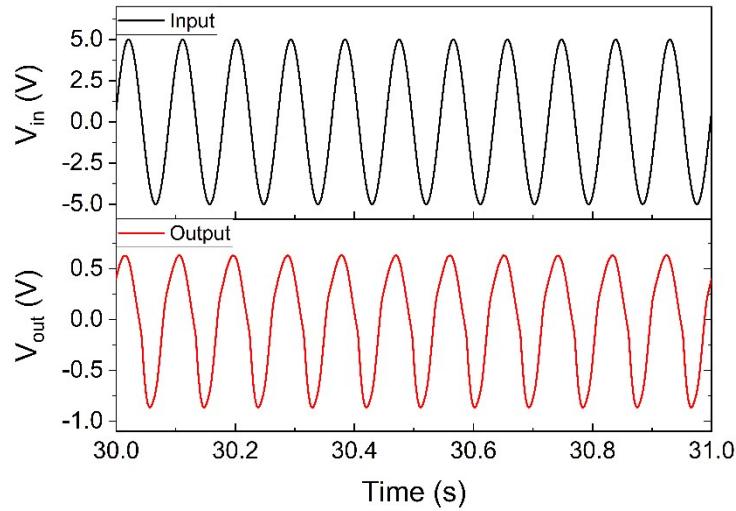
133 $\text{Triangle wave } f(x) = \frac{8}{\pi^2} \sum_{i=1,3,5,\dots}^{\infty} \frac{(-1)^{\frac{n-1}{2}}}{n^2} \sin\left(\frac{n\pi x}{L}\right) \#(13)$

134 $\text{Sawtooth wave } f(x) = \frac{1}{2} - \frac{1}{\pi} \sum_{i=1}^{\infty} \frac{1}{n} \sin\left(\frac{n\pi x}{L}\right) \#(14)$

135 $\text{Square wave } f(x) = \frac{4}{\pi} \sum_{i=1,3,5,\dots}^{\infty} \frac{1}{n} \sin\left(\frac{n\pi x}{L}\right) \#(15)$

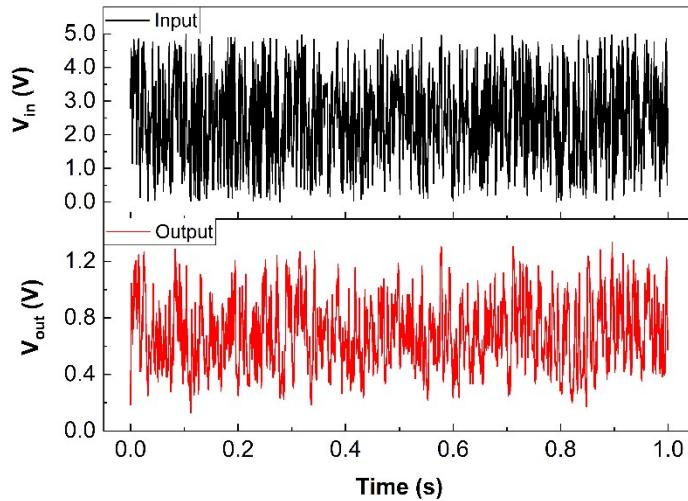
136 **S5. Input and Output representations of benchmark tasks**

137 The input and output of waveform reconstruction tasks is 11 Hz sine wave as shown in **Figure S4**.
 138 We observed one of the outputs of their reservoir is a little bit distorted, an indication of the
 139 nonlinear transformation by the reservoir on the input signal.



140

141 **Figure S4.** Input and output representation of waveform reconstruction task.



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143 **Figure S5.** Input and output representation of NARMA2 and MC task.

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