

## Supporting Information

### Molecular Mechanism on the Fracture Property of Slide- Ring Crosslinked Elastomer

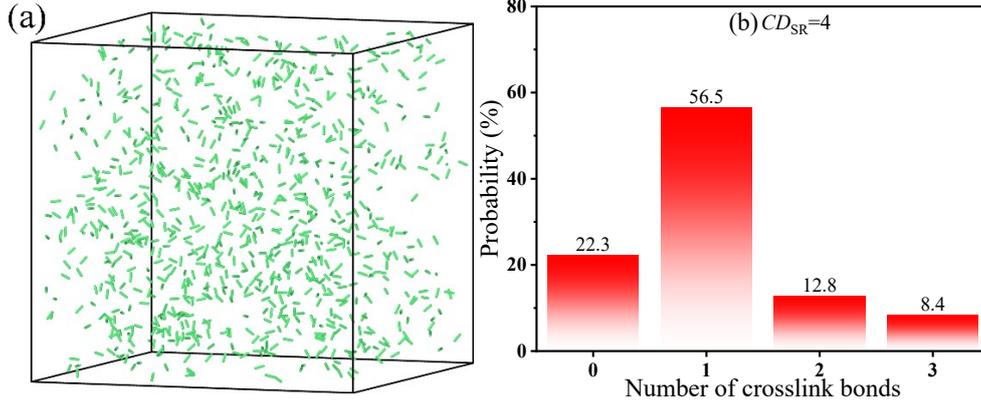
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**Figure S1. (a) Snapshots of crosslink bonds and (b) the probability distribution of number of formed crosslink bonds per slide ring (SR) at the crosslink density  $CD_{SR}=4.0$  of SR.**

## 1. Structure and dynamics properties

The influence of crosslink density ( $CD_{SR}$ ) and coverage ( $C_{SR}$ ) of slide ring (SR) on the structure and dynamics properties of the SR crosslinked elastomer (SRCE) is explored in this section. Firstly, the distribution ( $P(R_g^2)$ ) of mean squared radius of gyration of chains and its average ( $\langle R_g^2 \rangle$ ) are calculated for different  $CD_{SR}$  and  $C_{SR}$ .

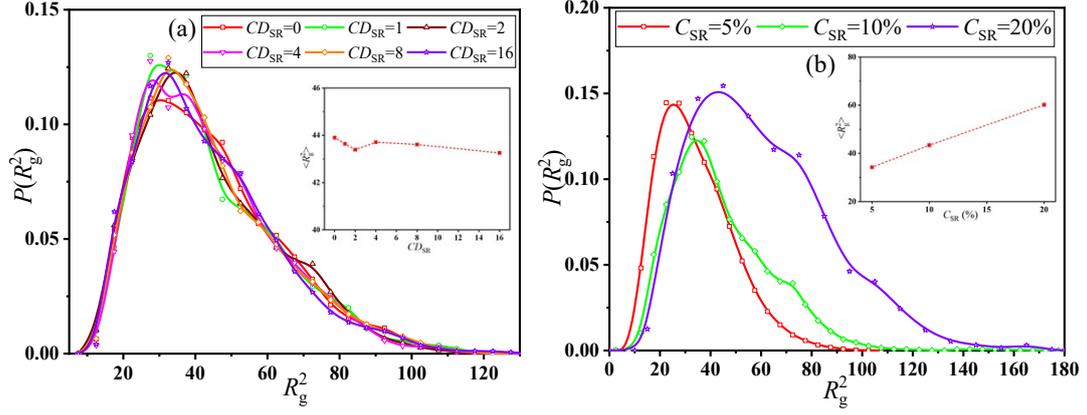
$\langle R_g^2 \rangle$  is calculated by  $\langle \frac{1}{N} \sum_{i=1}^N (r_i - r_{cm})^2 \rangle$  where  $r_i$  and  $r_{cm}$  denote the position vectors of backbone beads and chain center, and  $N$  is the number of backbone beads.

As presented in Figure S2(a),  $P(R_g^2)$  and  $\langle R_g^2 \rangle$  are nearly not influenced by  $CD_{SR}$ , which indicates that the crosslink bonds between SRs will not change the chain size.

However, the peak position of  $P(R_g^2)$  rises with increasing  $C_{SR}$  which improves  $\langle R_g^2 \rangle$ . This is because the chain backbone is imposed by geometrical constraints of

SRs which inhibit the free rotation of chains. Furthermore, asphericity factor ( $A_d$ ) of

chains is characterized via  $A_d = \frac{\sum_{i>j}^3 \langle (\lambda_i^2 - \lambda_j^2)^2 \rangle}{2 \langle \left( \sum_{i=1}^3 \lambda_i^2 \right)^2 \rangle}$  which can understand the anisotropy



**Figure S2.** Distribution ( $P(R_g^2)$ ) of mean squared radius of gyration of chains and its average ( $\langle R_g^2 \rangle$ ) for different (a) crosslink densities ( $CD_{SR}$ ) and (b) coverages ( $C_{SR}$ ) of SR.

of chains.<sup>1</sup> Three eigenvalues (set  $\lambda_1 > \lambda_2 > \lambda_3$ ) are obtained by diagonalizing the radius

of gyration tensor of chains which is  $G = \begin{bmatrix} R_{xx} & R_{xy} & R_{xz} \\ R_{yx} & R_{yy} & R_{yz} \\ R_{zx} & R_{zy} & R_{zz} \end{bmatrix}$ .  $R_{ab}$  is

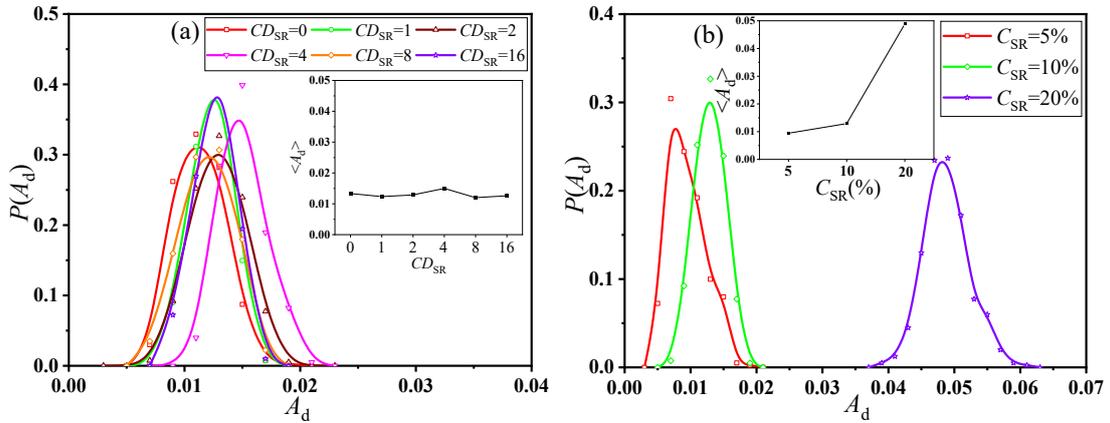
$$\frac{1}{N} \sum_{i=1}^N (a_i - a_{cm})(b_i - b_{cm})$$

where  $a$  and  $b$  denote  $x$ ,  $y$  or  $z$  coordinates of a bead respectively.  $(x_i, y_i, z_i)$  and  $(x_{cm}, y_{cm}, z_{cm})$  are the respective coordinates of  $i$ th bead and

chain center.  $A_d=0.0$  and  $1.0$  stand for a perfect spherical and stick shape of chains

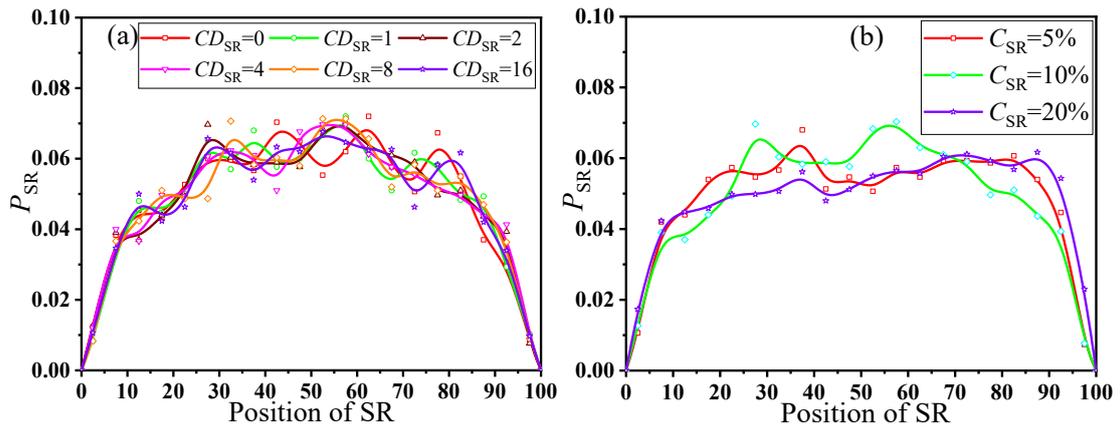
respectively. In general,  $A_d$  is between  $0.0$  and  $1.0$ . Figure S3 presents the distribution

( $P(A_d)$ ) of asphericity factor and its average ( $\langle A_d \rangle$ ) for different  $CD_{SR}$  and  $C_{SR}$ . Both



**Figure S3.** Distribution ( $P(A_d)$ ) of asphericity factor of chains and its average ( $\langle A_d \rangle$ ) for different (a) crosslink densities ( $CD_{SR}$ ) and (b) coverages ( $C_{SR}$ ) of SR.

$P(A_d)$  and  $\langle A_d \rangle$  are similar for different  $CD_{SR}$  which reflects the same anisotropy of chains. However, they exhibit a first slow and then quick rise with increasing  $C_{SR}$  which means a more pronounced anisotropy of chains. This reflects that the geometrical constrains imposed by SRs improve the conformational anisotropy of chains. Furthermore, the position distribution of SR on the chain backbone is explored where the position of SR is defined as the index of nearest backbone bead from the mass center of SR. From Figure S4, the position distribution ( $P_{SR}$ ) of SR is relatively uniform in the middle of chains while there are few SRs at the end of chains which is mainly due to the entropy effect. Meanwhile,  $P_{SR}$  is similar for different  $CD_{SR}$  and  $C_{SR}$  which means



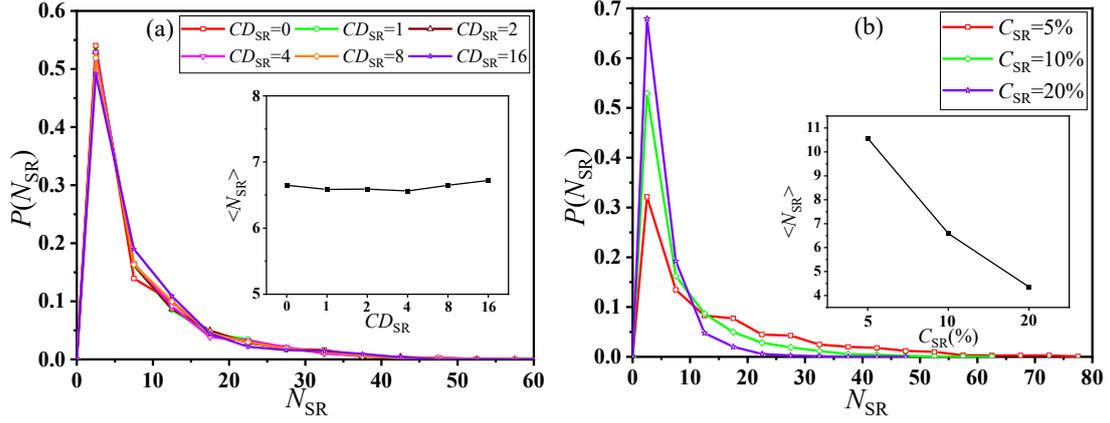
**Figure S4. Position distribution ( $P_{SR}$ ) of slide ring (SR) on the chain backbone for different (a) crosslink densities ( $CD_{SR}$ ) and (b) coverages ( $C_{SR}$ ) of SR.**

the same distribution state of SR. Moreover, the distribution ( $P(N_{SR})$ ) of number of beads between two continuous SRs and its average ( $\langle N_{SR} \rangle$ ) are presented in Figure S5.

It is observed that both  $P(N_{SR})$  and  $\langle N_{SR} \rangle$  are similar which are independent on  $CD_{SR}$ .

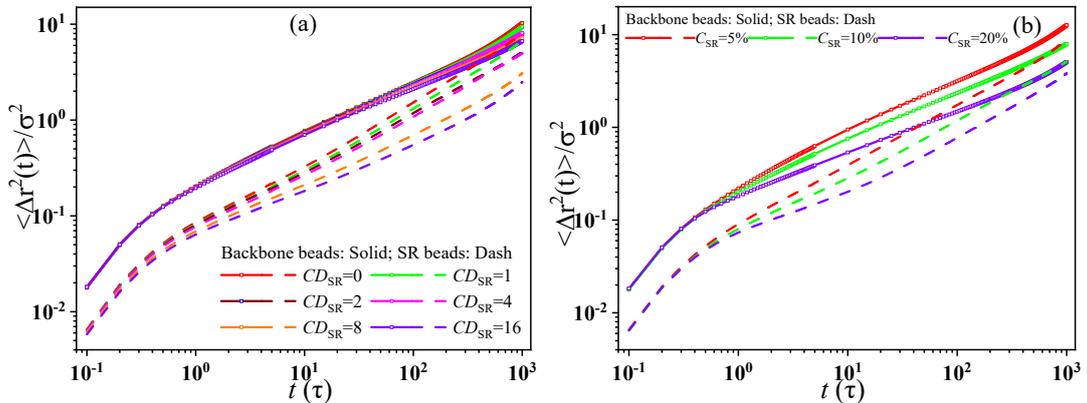
However, the peak height of  $P(N_{SR})$  rises with increasing  $C_{SR}$  which reduces  $\langle N_{SR} \rangle$ .

This is mainly attributed to more SRs on the chain backbone.



**Figure S5.** Distribution of average number of beads ( $N_{\text{SR}}$ ) between two continuous slide rings (SRs) and its average ( $N_{\text{ave}}$ ) for different (a) crosslink densities ( $CD_{\text{SR}}$ ) and (b) coverages ( $C_{\text{SR}}$ ) of SR.

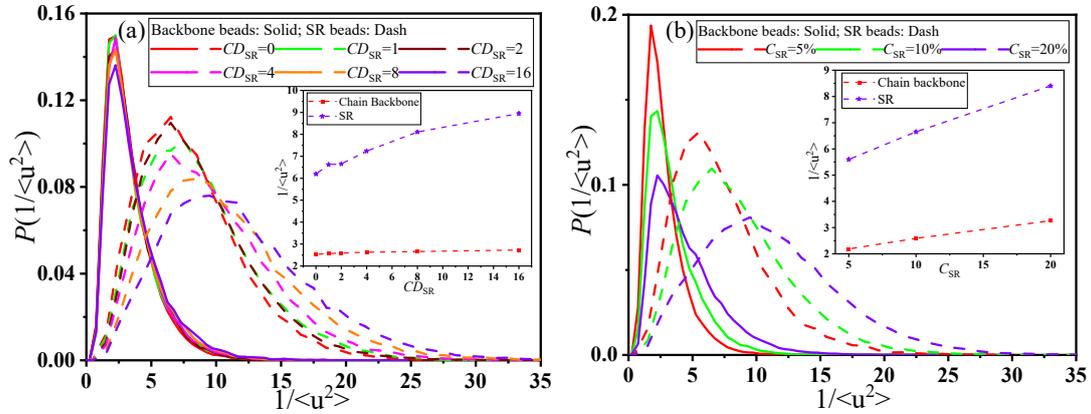
Following it, the mean squared displacement (MSD) of backbone beads and SR beads are analyzed for different  $CD_{\text{SR}}$  and  $C_{\text{SR}}$  which is calculated via equation  $\langle \Delta r^2(t) \rangle = \langle [r_i(t+t_0) - r_i(t_0)]^2 \rangle$ . Here,  $r_i(t_0)$  and  $r_i(t+t_0)$  are the position vectors of a bead  $i$  at times  $t_0$  and  $t+t_0$  respectively. As shown in Figure S6,  $\langle \Delta r^2(t) \rangle$  of both backbone beads and SR beads decreases with increasing  $CD_{\text{SR}}$  or  $C_{\text{SR}}$ . This is because the crosslink bonds between SRs and SRs themselves impose the geometrical constraints which reduces the mobility of both chain backbone and SR. Meanwhile,  $\langle \Delta r^2(t) \rangle$  of chain backbone is larger than that of SR. This indicates that SR shows a



**Figure S6.** Mean square displacement  $\langle \Delta r^2(t) \rangle$  of backbone beads and slide rings (SR) beads and with the time  $t$  for different (a) crosslink densities ( $CD_{\text{SR}}$ ) and (b) coverages ( $C_{\text{SR}}$ ) of SR.

more significant mobility reduction than the chain backbone which is due to the greater

stiffness of SR. Moreover, the Debye-Waller factor ( $\langle u^2 \rangle$ ) is characterized which measures the average MSD of beads in its caging regime. Thus,  $\langle u^2 \rangle$  is defined as the plateau value of MSD at  $t=3\tau$  which roughly corresponds to a caging time scale.<sup>2,3</sup> The inverse of  $\langle u^2 \rangle$  is analyzed which reflects the local molecular stiffness. As shown in Figure S7(a), the distribution ( $P(1/\langle u^2 \rangle)$ ) of local molecular stiffness and its average ( $1/\langle u^2 \rangle$ ) for chain backbone are similar for different  $CD_{SR}$  which reflects the same local molecular stiffness. However, the peak height of  $P(1/\langle u^2 \rangle)$  for SR decreases while the peak position rises with increasing  $CD_{SR}$  which improves  $1/\langle u^2 \rangle$ . This is due to the crosslink bonds between SRs. From Figure S7(b),  $1/\langle u^2 \rangle$  rises for both chain backbone and SR with increasing  $C_{SR}$ . This reflects the increased local molecular stiffness which is attributed to the topological limitations imposed by a large number of



**Figure S7. Distribution ( $P(1/\langle u^2 \rangle)$ ) of local molecular stiffness for chain backbone and slide ring (SR) and its average ( $1/\langle u^2 \rangle$ ) for different (a) crosslink densities ( $CD_{SR}$ ) and (b) coverages ( $C_{SR}$ ) of SR.**

SRs. Finally, the sliding dynamics of SR is analyzed which is defined as the mean squared displacement ( $MSD_{acb}$ ) of SR along the chain backbone. As shown in Figure S8, it is found that  $MSD_{acb}$  decreases with increasing  $CD_{SR}$  or  $C_{SR}$  which reflects the reduced sliding motion along the chain backbone.

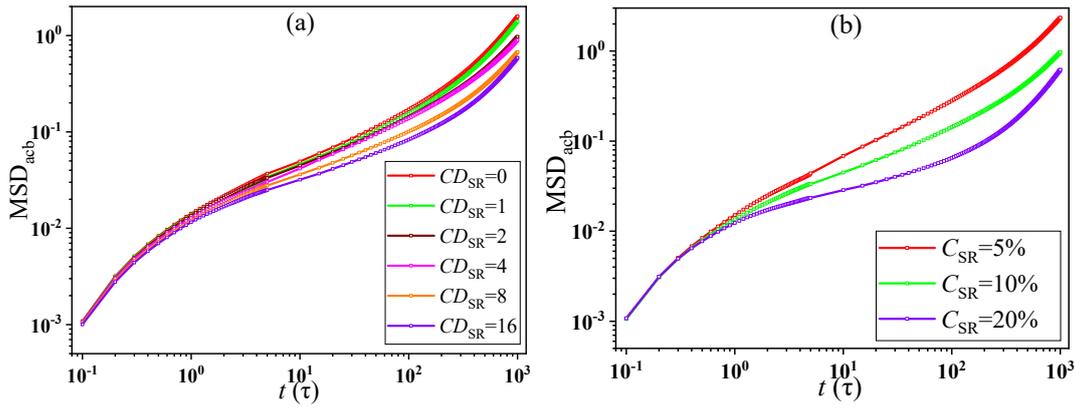


Figure S8. Mean square displacement ( $MSD_{ach}$ ) of backbone beads and slide ring (SR) beads with the time  $t$  for different (a) crosslink densities ( $CD_{SR}$ ) and (b) coverages ( $C_{SR}$ ) of SR.

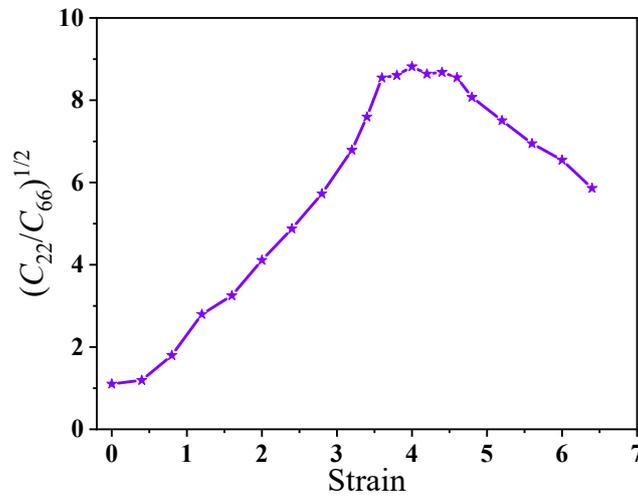


Figure S9. The calculated  $\sqrt{C_{22}/C_{66}}$  with strain before the maximum stress. ( $CD_{SR}=8$ )

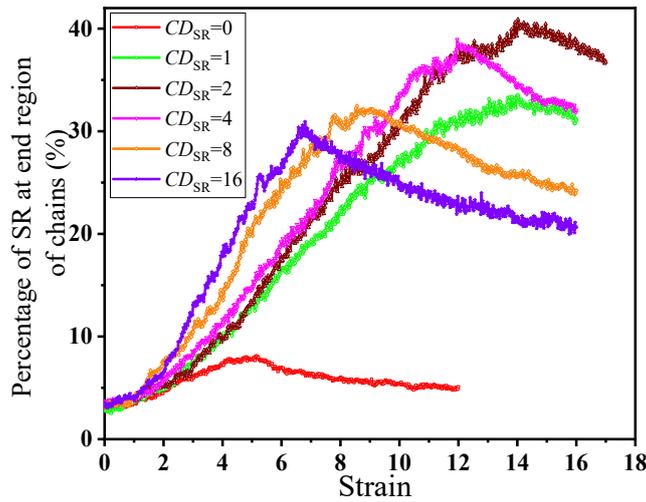


Figure S10. The percentage of slide ring (SR) at the end region of chains by normalizing the total number of existing SR with respect to the strain for different crosslink densities ( $CD_{SR}$ ) of SR.

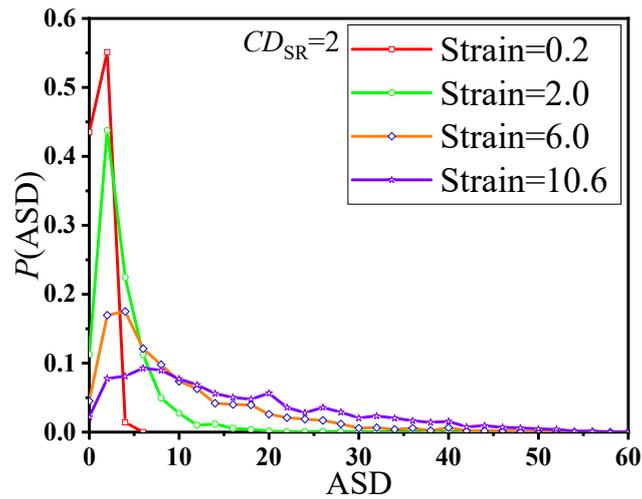


Figure S11. The distribution of the average sliding distance (ASD) of slide ring (SR) at four typical strains.

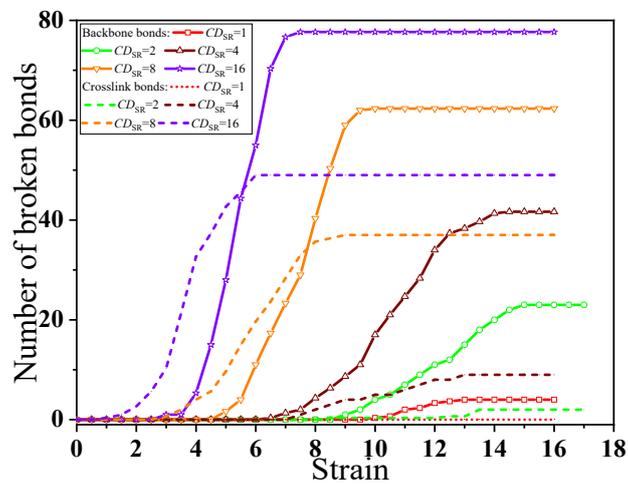


Figure S12. Number of broken backbone or crosslink bonds with respect to the strain for different crosslink densities ( $CD_{SR}$ ) of slide ring.

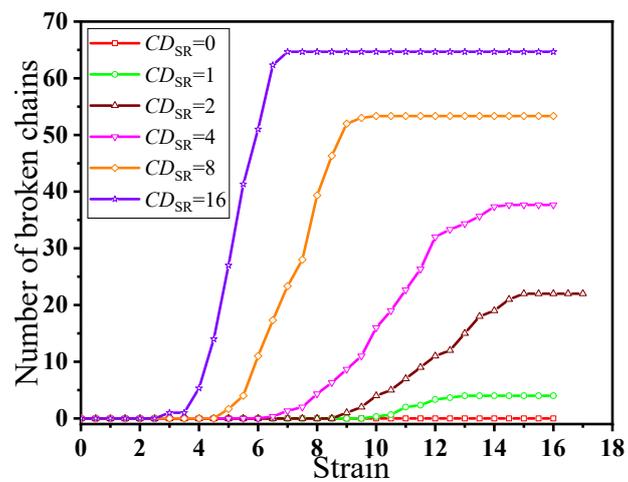


Figure S13. Number of broken chains with respect to the strain for different crosslink densities ( $CD_{SR}$ ) of slide ring.

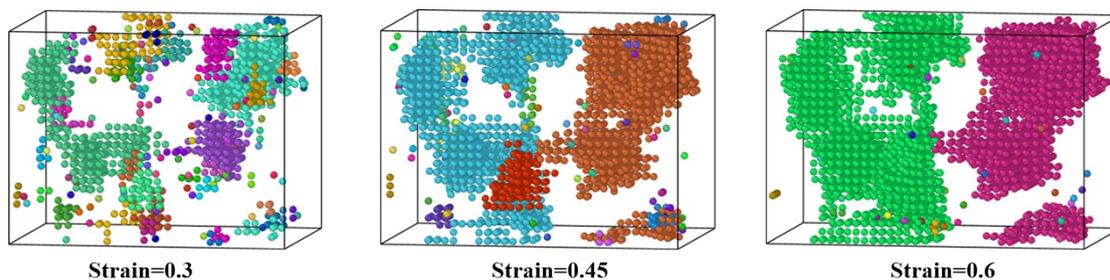


Figure S14. Snapshots of voids at three typical strains for crosslink density  $CD_{SR}=2$ .

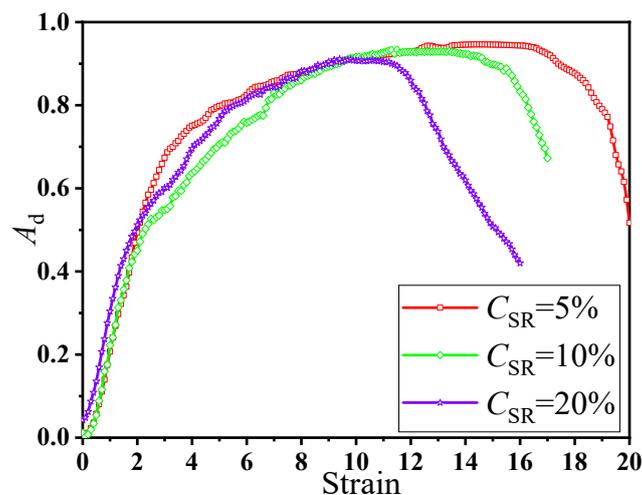


Figure S15. The asphericity factor ( $A_d$ ) of unbroken chain backbone with respect to the strain for different coverages ( $C_{SR}$ ) of slide ring.

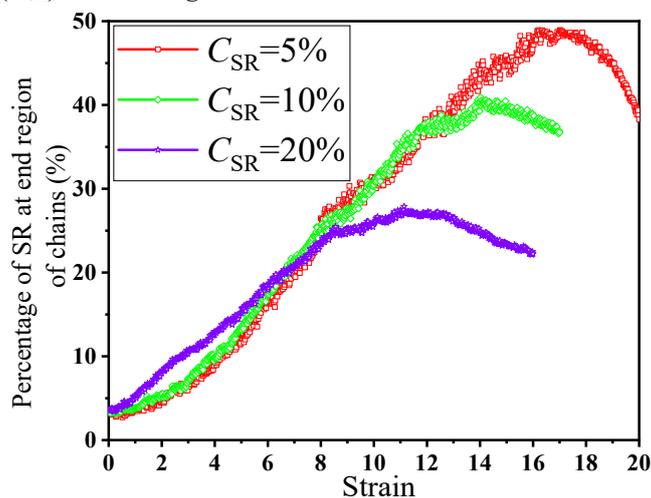


Figure S16. The percentage of slide ring (SR) at the end region of chains by normalizing the total number of existing SR with respect to the strain for different coverages ( $C_{SR}$ ) of SR.

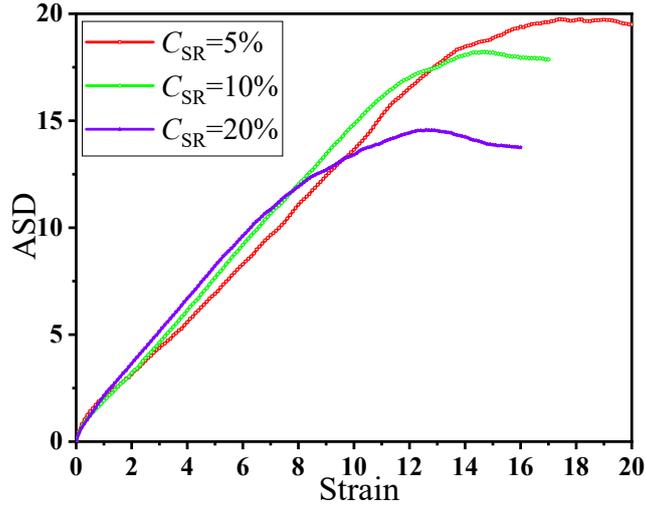


Figure S17. The average sliding distance (ASD) of slide ring (SR) with respect to the strain for different coverages ( $C_{SR}$ ) of SR.

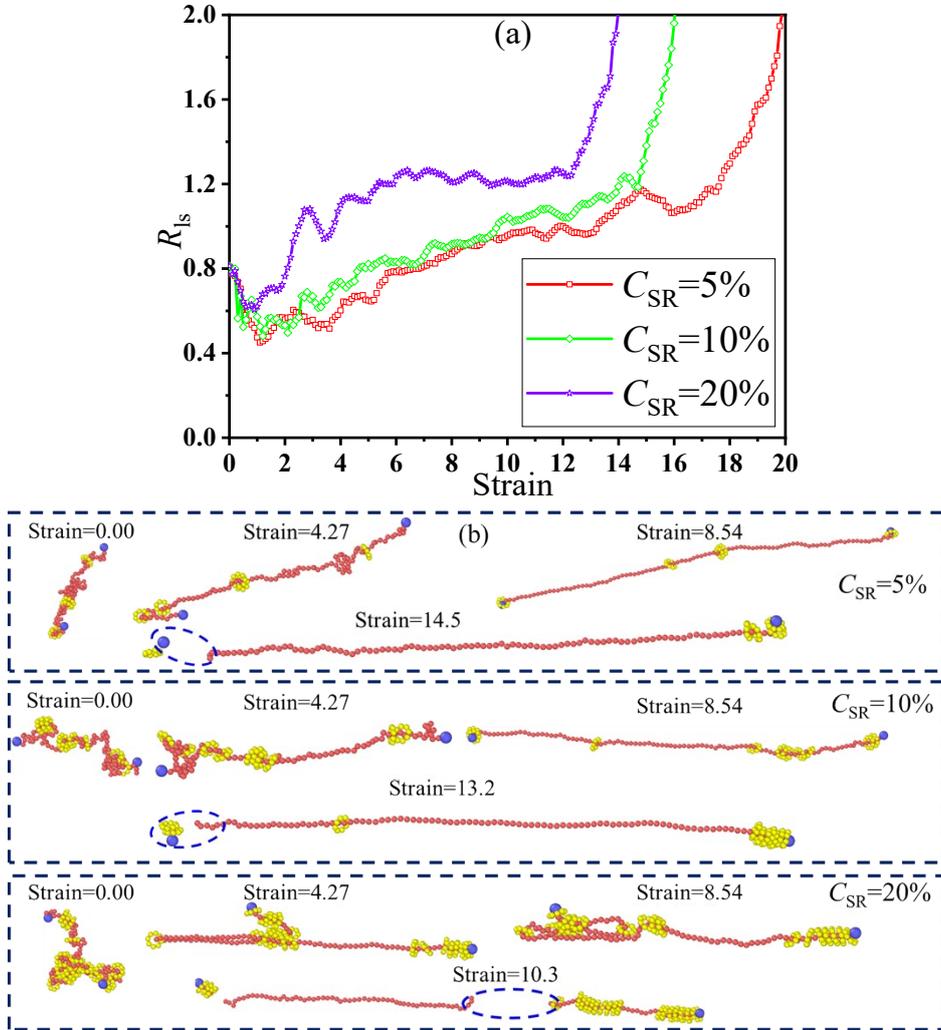


Figure S18. (a) Ratio ( $R_{ls}$ ) of local stress by one end bead to that by one inner bead with respect to the strain (b) snapshots of a typical chain at some strains for different coverages ( $C_{SR}$ ) of slide ring.

## REFERENCES

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**Table SI Parameters of each simulation model**

Crosslink density ( $CD_{SR}$ )	Coverage ( $C_{SR}$ )	Number of slide rings ( $N_{SR}$ ) in each chain	Chain length ( $L_c$ )	Number of chains ( $N_c$ )
0	0%	0	100	300
1	10%	10	100	300
2	10%	10	100	300
4	10%	10	100	300
8	10%	10	100	300
16	10%	10	100	300
2	5%	5	100	300
2	20%	20	100	300

**Table SII The nonbonded interaction parameters of each simulation model**

Nonbonded interaction pairs	$\epsilon_{ij}$	$\Delta$ ( $\sigma$ )	$r_c$ ( $\sigma$ )
A A	1.0	0.0	2.5
A B	1.0	0.0	2.5
A C	2.0	0.5	2.5
B B	1.0	0.0	2.5
B C	2.0	0.5	2.5
C C	1.0	1.0	2.5

**Table SIII Calculated parameters for each simulation system**

Crosslink density ( $CD_{SR}$ )	Coverage ( $C_{SR}$ )	$S$	$S_{max}$	$\lambda$	$D$	$\sqrt{C_{22}/C_{66}}$
0	0%	0.27	0.30	2.68	23.13	1.83±0.08
1	10%	0.35	0.41	5.85	21.92	5.81±0.12
2	10%	0.33	0.82	8.71	18.94	10.3±0.11
4	10%	0.43	1.34	7.53	16.61	10.2±0.10
8	10%	0.58	2.01	4.84	13.79	8.66±0.09
16	10%	0.72	2.62	3.72	11.11	7.54±0.08
2	5%	0.30	0.92	8.78	20.58	9.61±0.09
2	20%	0.36	0.65	5.88	18.56	6.11±0.11

**Table SIV Fracture energy ( $G_c$ ) for different defined void sizes ( $D$ )**

Crosslink density ( $CD_{SR}$ )	Coverage ( $C_{SR}$ )	$G_c$ (Mean $D$ )	$G_c$ (Median $D$ )	$G_c$ (70th percentile $D$ )
0	0%	55.4±2.4	59.9±2.6	65.1±2.8
1	10%	318.6±6.6	344.6±7.1	368.2±7.6
2	10%	2204.3±23.6	2354.5±25.2	2512.8±26.9
4	10%	3873.8±37.8	4130.3±40.3	4456.5±43.4
8	10%	4146.8±43.1	4402.4±45.8	4549.8±47.3
16	10%	3669.1±38.9	3873.9±41.1	4005.9±42.5
2	5%	3106.6±29.1	3355.3±32.4	3520.2±32.9
2	20%	694.0±12.5	753.7±13.6	775.3±14.0