

Supporting Information

Investigating Anisole/Cu(II)-Macroligand-complex Pair to Broaden Solubility Scope and Catalyst Recycling for Atom Transfer Radical Polymerization

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Materials

Methyl methacrylate (MMA, $\geq 99\%$, Shanghai Macklin Biochemical Co. Ltd), was purified by passing through a column packed with activated neutral alumina. 2,2- azobisisobutyronitrile (AIBN, $\geq 97\%$, Tianjin Guanfu Fine Chemical Research Institute) was purified from ethanol, dried and then stored in a refrigerator at about $-2\text{ }^{\circ}\text{C}$. Other chemical reagents such as poly(ethylene glycol)-300-methyl ether methacrylate (PEG₃₀₀MMA) (Macklin, China), ethyl bromide (99%, Yonghua Chemical Co. Ltd), ethyl 2-bromoisobutyrate (EBiB, 98%, Energy Chemical, China), acryloyl chloride (96%), 2-[(dimethylamino)ethyl] methacrylate (99%), ethanolamine (97%), acetonitrile (+99.9 analytical grade), benzene (+99%), 1,3,5-trimethylbenzene (97%), dimethyl sulfoxide (DMSO, analytical grade), triethylamine (99%), anisole (99%), acetonitrile (99%) were all acquired from Shanghai Macklin Biochemical Co. Ltd, while 2-(chloromethyl)-4-methoxy-3,5-dimethylpyridine·HCl (98%, Shanghai Yuanye Bio-Technology Co. Ltd), copper(II)bromide (CuBr₂, 99.95%, Aladdin Chemistry Co. Ltd), anhydrous methanol (+99.5%), toluene ($\geq 99.5\%$), tetrahydrofuran (THF, +99.5%), dichloromethane (+97.5%) from Sinopharm Chemical Reagent Co. Ltd., anhydrous sodium carbonate (+99.8%), anhydrous potassium carbonate (+99%), anhydrous magnesium sulphate (+99%), xylene ($\geq 99.0\%$) from Shanghai Lingfeng Chemical reagent Co. Ltd., were all used as received.

Characterization

The dispersity (M_w/M_n) and number-average molecular weight ($M_{n,\text{GPC}}$) of the polymers were analyzed using an Agilent Technologies PL-220 gel permeation chromatography (GPC) system equipped with a refractive index detector. Separation was performed on a PLgel 5 μm MIXED-C column (300 \times 7.5 mm) with a molecular weight detection ranging from 6×10^2 to 5×10^5 g/mol. Tetrahydrofuran (THF) was used as the mobile phase at a flow rate of 1.0 mL/min and a temperature of $40\text{ }^{\circ}\text{C}$. The sample injection was carried out automatically using an Agilent Technologies autosampler, and the system was calibrated with polystyrene standards. The obtained polymers were further characterized by ^1H NMR spectroscopy on an INOVA 600 MHz spectrometer using CDCl₃ and DMSO-d₆ as solvents with tetramethylsilane (TMS) as the internal reference. The residual copper content in the polymer solutions was determined by inductively coupled plasma mass spectrometry (ICP-MS). The polymerization mechanism was investigated using a Shimadzu UV-2600 UV-Vis spectrometer over a wavenumber range of 200–900 cm^{-1} .

Equation S1: Calculating the percentage conversion of monomer

$$\% \text{ conv} = (1 - \text{ratio volume of } M_{[\text{rxn}]} \times \text{peak area of } V_{\text{H}} \times \text{ratio volume of } A_{[\text{rxn}]}) \times 100\%$$

where;

$M_{[\text{rxn}]}$ = Monomer reaction mixture

V_{H} = Vinyl Hydrogen of Monomer after polymerization

$A_{[\text{rxn}]}$ = Anisole before/after reaction

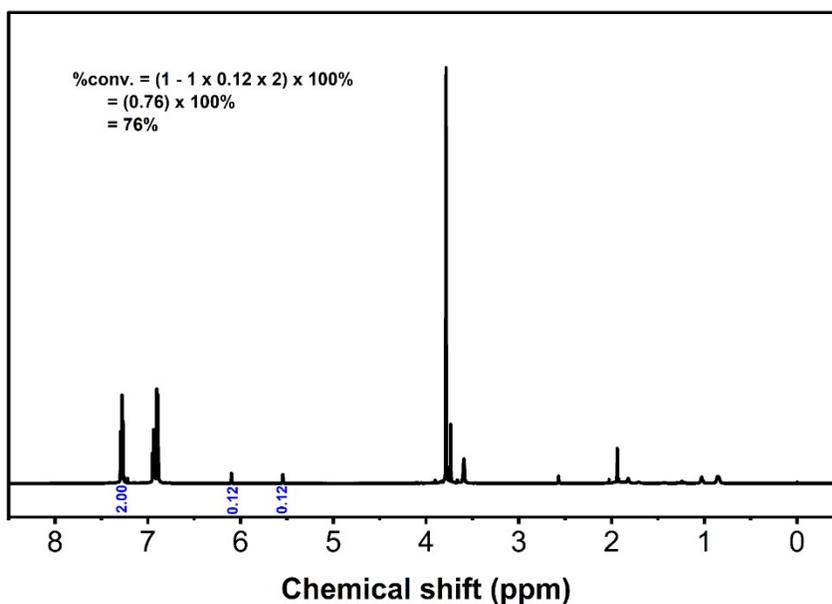


Fig. S1 ^1H NMR spectrum of the representative polymerization reaction mixture used in all the calculations for the percentage conversion

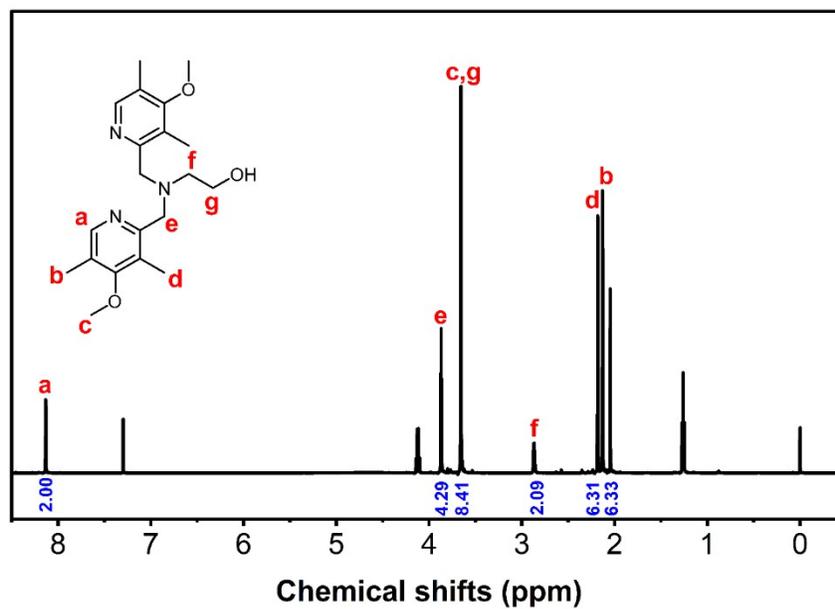


Fig. S2 ^1H NMR analysis of intermediate product **1** performed in CDCl_3 employing TMS as an internal reference

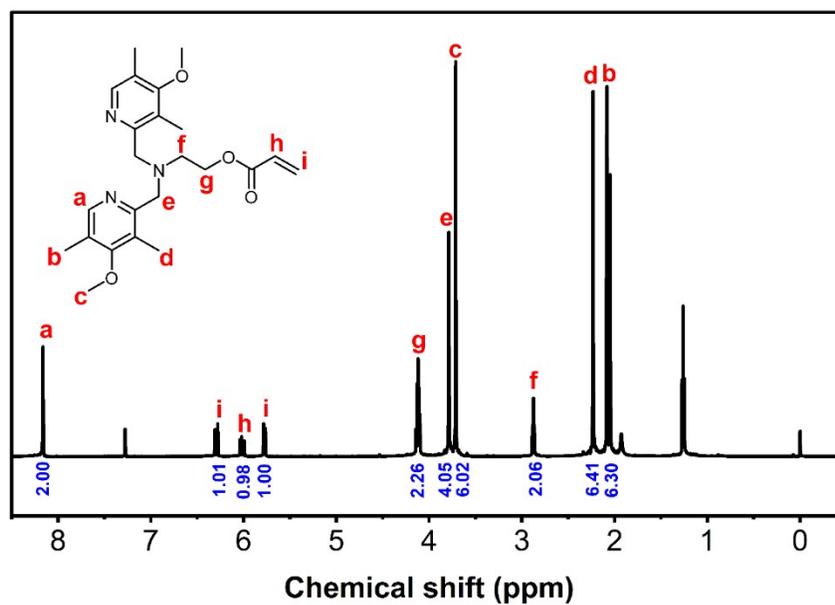


Fig. S3 ^1H NMR analysis of intermediate product **2** performed in CDCl_3 employing TMS as an internal reference

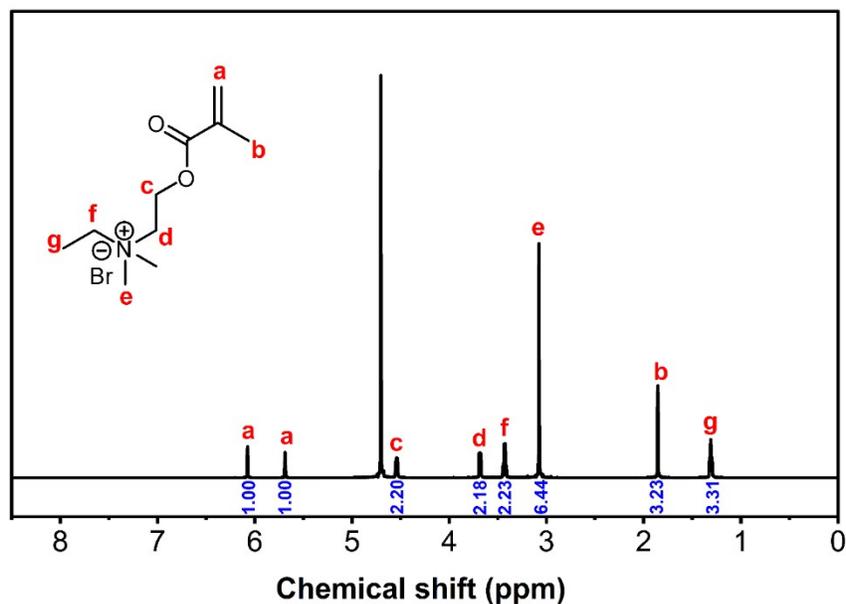


Fig. S4 ^1H NMR analysis of intermediate product **3** performed in D_2O employing TMS as an internal reference

Table S1 Different batches of $\text{PEG}_{300}\text{MMA}$ obtained from the same company and their ratios to attain the TPSC-based ICAR ATRP system

| Entry | Company | Anisole (mL) | MMA (mL) | CuBr_2 (mg) | AIBN (mg) | MA- sLN | ILM | PEG300 MMA | rt^{a} | 80 $^{\circ}\text{C}$ | rt^{b} | No. of Batches |
|-------|----------------------|-----------------|-------------|-------------------------|--------------|------------|-----|---------------|------------------------|-----------------------|------------------------|-------------------|
| 1 | Macklin ^a | 2.0 | 1.0 | 1.0 | 7.8 | 1 | 4.2 | 5.0 | M | M | I | 18 |
| 2 | Macklin ^b | 2.0 | 1.0 | 1.0 | 7.8 | 1 | 3.2 | 5.0 | M | M | I | 4 |
| 3 | Macklin ^c | 2.0 | 1.0 | 1.0 | 0.0 | 1 | 2.9 | 5.0 | M | M | I | 3 |

I = Immiscibility and M = Miscibility; rt^{a} = At room temperature and rt^{b} = After Cooling cycle to room temperature; ^{a,b,c} $\text{PEG}_{300}\text{MMA}$ batches

Table S2 Sustainability assessment guide of 4 selected organic solvents based on safety, health, and environmental scores¹⁻³

| Entry | Solvent | Boiling point (°C) | Safety score | Health score | Environmental score | Solvent sustainability ranking | Overall score |
|-------|---------|--------------------|--------------|--------------|---------------------|--------------------------------|---------------|
| 1 | Anisole | 154 | 4 | 1 | 5 | Recommended | 1 |
| 2 | Benzene | 80 | 6 | 10 | 3 | Hazardous | 4 |
| 3 | Xylene | 140 | 4 | 2 | 5 | Problematic | 2 |
| 4 | Toluene | 111 | 5 | 6 | 3 | Problematic | 3 |

The color code represents the scoring index: green for 1–3, yellow for 4–6, and red for 7–10

Table S3 Effects of varying Macroligand (PILLL1) for TPSC-based ICAR ATRP system

| Entry | x | x (mg) | Time (h) | Conv. (%) | $M_{n,th}$ (g/mol) | $M_{n,GPC}$ (g/mol) | M_w/M_n |
|-------|---|--------|----------|-----------|--------------------|---------------------|-----------|
| 1 | 5 | 279 | 4 | 80 | 16200 | 13700 | 1.36 |
| 2 | 4 | 223 | 4 | 88 | 17800 | 13400 | 1.09 |
| 3 | 3 | 167 | 4 | 74 | 15000 | 13000 | 1.20 |
| 4 | 2 | 112 | 4 | 72 | 14600 | 14100 | 1.13 |
| 5 | 1 | 56 | 4 | 68 | 13800 | 11600 | 1.27 |

Polymerization conditions: $[MMA]_0/[EBiB]_0/[CuBr_2]_0/[PILLL1]_0/[AIBN]_0 = 200/1/1/x/1$, $V_{MMA} = 1$ mL, $V_{anisole} = 2$ mL, temperature = 80 °C. $M_{n,th} = ([M]_0/[M]) \times [MMA] \times Conv.\% + M_{w,EBiB}$

Table S4 Effects of varying AIBN for TPSC-based ICAR ATRP system

| Entry | x | x (mg) | Time (h) | Conv. (%) | $M_{n,th}$ (g/mol) | $M_{n,GPC}$ (g/mol) | M_w/M_n |
|-------|------|-----------|-------------|--------------|-----------------------|------------------------|-----------|
| 1 | 1.25 | 0.980 | 4 | 92 | 18600 | 15300 | 1.11 |
| 2 | 1.00 | 0.780 | 4 | 88 | 17800 | 13400 | 1.09 |
| 3 | 0.50 | 0.390 | 4 | 68 | 13800 | 12600 | 1.14 |
| 4 | 0.25 | 0.195 | 4 | 40 | 8200 | 7400 | 1.16 |
| 5 | 0.10 | 0.078 | 4 | * | * | * | * |

Polymerization conditions: $[MMA]_0/[EBiB]_0/[CuBr_2]_0/[PILLL1]_0/[AIBN]_0 = 200/1/1/4/x$, $V_{MMA} = 1$ mL, $V_{anisole} = 2$ mL, temperature = 80 °C. $M_{n,th} = ([M]_0/[M]) \times [MMA] \times Conv.\% + M_{w,EBiB}$.

*No polymer formed

Table S5 Effects of varying $CuBr_2$ for TPSC-based ICAR ATRP system

| Entry | x | x (mg) | Time (h) | Conv. (%) | $M_{n,th}$ (g/mol) | $M_{n,GPC}$ (g/mol) | M_w/M_n |
|-------|------|-----------|-------------|--------------|-----------------------|------------------------|-----------|
| 1 | 1.00 | 10.4 | 4 | 88 | 17800 | 13400 | 1.09 |
| 2 | 0.50 | 5.2 | 4 | 80 | 16200 | 10500 | 1.21 |
| 3 | 0.25 | 2.6 | 4 | 92 | 18600 | 16900 | 1.25 |
| 4 | 0.13 | 1.3 | 4 | 90 | 18200 | 15500 | 1.13 |

Polymerization conditions: $[MMA]_0/[EBiB]_0/[CuBr_2]_0/[PILLL1]_0/[AIBN]_0 = 200/1/1/4/1$, $V_{MMA} = 1$ mL, $V_{anisole} = 2$ mL, temperature = 80 °C. $M_{n,th} = ([M]_0/[M]) \times [MMA] \times Conv.\% + M_{w,EBiB}$.

Table S6 Effects of varying volume of solvent for TPSC-based ICAR ATRP system

| Entry | Anisole (x) (mL) | Time (h) | Conv. (%) | $M_{n,th}$ (g/mol) | $M_{n,GPC}$ (g/mol) | M_w/M_n |
|-------|---------------------|-------------|--------------|-----------------------|------------------------|-----------|
| 1 | 3.0 | 4 | 82 | 16600 | 13700 | 1.30 |
| 2 | 2.5 | 4 | 75 | 15200 | 13500 | 1.35 |
| 3 | 2.0 | 4 | 88 | 17800 | 13400 | 1.09 |

Polymerization conditions: $[MMA]_0/[EBiB]_0/[CuBr_2]_0/[PILLL1]_0/[AIBN]_0 = 200/1/1/4/1$, $V_{MMA} = 1$ mL, $V_{anisole} = x$ mL, temperature = 80 °C. $M_{n,th} = ([M]_0/[M]) \times [MMA] \times Conv.\% + M_{w,EBiB}$.

Table S7 Effects of varying Temperature for TPSC via ICAR ATRP system

| Entry | Temperature (x) (°C) | Time (h) | Conv. (%) | $M_{n,th}$ (g/mol) | $M_{n,GPC}$ (g/mol) | M_w/M_n |
|-------|-------------------------|-------------|--------------|-----------------------|------------------------|-----------|
| 1 | 70 | 4 | 65 | 13200 | 10700 | 1.28 |
| 2 | 80 | 4 | 88 | 17800 | 13400 | 1.09 |
| 3 | 90 | 4 | 87 | 17600 | 15900 | 1.16 |

Polymerization conditions: $[MMA]_0/[EBiB]_0/[CuBr_2]_0/[PILLL1]_0/[AIBN]_0 = 200/1/1/4/1$, $V_{MMA} = 1$ mL, $V_{anisole} = 2$ mL, temperature = x °C. $M_{n,th} = ([M]_0/[M]) \times [MMA] \times Conv.\% + M_{w,EBiB}$

Table S8 Effects of varying alkyl halide initiator (EBiB) for TPSC-based ICAR ATRP system

| Entry | x | x (μ L) | Time (h) | Conv. (%) | $M_{n,th}$ (g/mol) | $M_{n,GPC}$ (g/mol) | M_w/M_n |
|-------|-----|-----------------|-------------|--------------|-----------------------|------------------------|-----------|
| 1 | 1.5 | 10.2 | 4 | 82 | 11100 | 13100 | 1.18 |
| 2 | 1.0 | 6.8 | 4 | 88 | 17800 | 13400 | 1.09 |
| 3 | 0.5 | 3.4 | 4 | 76 | 30400 | 21700 | 1.43 |

Polymerization conditions: $[MMA]_0/[EBiB]_0/[CuBr_2]_0/[PILLL1]_0/[AIBN]_0 = 200/x/1/4/1$, $V_{MMA} = 1$ mL, $V_{anisole} = 2$ mL, temperature = 80 °C. $M_{n,th} = ([M]_0/[M]) \times [MMA] \times Conv.\% + M_{w,EBiB}$

Table S9 Recycling performance of the PILL1/CuBr₂ catalyst in TPSC-based ICAR ATRP system

| Entry | Recycling times | Time (h) | Conv. (%) | $M_{n,th}$ (g/mol) | $M_{n,GPC}$ (g/mol) | M_w/M_n | CR ^a (ppm) |
|-------|-----------------|----------|-----------|--------------------|---------------------|-----------|-----------------------|
| 1 | 1 | 7 | 64 | 13000 | 18000 | 1.40 | 187 |
| 2 | 2 | 7 | 52 | 10600 | 17400 | 1.38 | 114 |
| 3 | 3 | 7 | 16 | 3400 | * | * | * |

Polymerization conditions: $[MMA]_0/[EBiB]_0/[CuBr_2]_0/[PILL1]_0/[AIBN]_0 = 200/1/0.1/1.2/0.2$, $V_{MMA} = 1$ mL, $V_{anisole} = 2$ mL, temperature = 80 °C. $M_{n,th} = ([M]_0/[M]) \times [MMA] \times Conv.\% + M_{w,EBiB}$. CR^a refers to the residual catalyst present in the organic polymer solution phase, measured by ICP-MS. *No monomer formed, and the reaction mixture became homogeneous

Table S10 Recycling performance of the PILL1/CuBr₂ catalyst in TPSC-based ICAR ATRP system under varied time and AIBN concentration

| Entry | Recycling times | Time (h) | Conv. (%) | $M_{n,th}$ (g/mol) | $M_{n,GPC}$ (g/mol) | M_w/M_n | CR ^a (ppm) |
|-------|-----------------|----------|-----------|--------------------|---------------------|-----------|-----------------------|
| 1 | 1 | 7 | 64 | 13000 | 41300 | 1.37 | 34.5 |
| 2 | 2 | 6 | 84 | 17000 | 84100 | 1.31 | 32.9 |
| 3 | 3 | 5 | 85 | 17200 | 68300 | 1.20 | 28.9 |
| 4 | 1* | 7 | 65 | 13200 | 45600 | 1.55 | 17.5 |
| 5 | 2* | 6 | 83 | 16800 | 83500 | 1.27 | 16.7 |
| 6 | 3* | 5 | 84 | 17000 | 94100 | 1.24 | 14.2 |

Polymerization conditions: $[MMA]_0/[EBiB]_0/[CuBr_2]_0/[PILL1]_0/[AIBN]_0 = 200/1/0.1/4/x = 0.2, 0.3, 0.4$, and $*[MMA]_0/[EBiB]_0/[CuBr_2]_0/[PILL1]_0/[AIBN]_0 = 200/1/0.05/4/x = 0.2, 0.3, 0.4$, $V_{MMA} = 1$ mL, $V_{anisole} = 2$ mL, temperature = 80 °C. $M_{n,th} = ([M]_0/[M]) \times [MMA] \times Conv.\% + M_{w,EBiB}$. CR^a refers to the residual catalyst present in the organic polymer solution phase, measured by ICP-MS

Table S11 Recycling performance of the PILL1/CuBr₂ catalyst in TPSC-based ICAR ATRP system under varied time and AIBN concentration

| Entry | Recycling times | Time (h) | Conv. (%) | $M_{n,th}$ (g/mol) | $M_{n,GPC}$ (g/mol) | M_w/M_n | CR ^a (ppm) |
|-------|-----------------|----------|-----------|--------------------|---------------------|-----------|-----------------------|
| 1 | 1 ^a | 7 | 68 | 13800 | 45300 | 1.58 | 10.3 |
| 2 | 2 ^b | 6 | 80 | 16200 | 41000 | 1.48 | 9.0 |
| 3 | 3 ^c | 5 | 88 | 17800 | 35500 | 1.48 | 5.8 |
| 4 | 4 ^c | 5 | 88 | 17800 | 30500 | 1.44 | 4.4 |
| 5 | 5 ^c | 5 | 84 | 17000 | 33000 | 1.25 | 3.4 |

Polymerization conditions: $[MMA]_0/[EBiB]_0/[CuBr_2]_0/[PILL1]_0/[AIBN]_0 = 200/1/0.025/4/x = 0.2^a, 0.3^b, 0.4^c$, $V_{MMA} = 1$ mL, $V_{anisole} = 2$ mL, temperature = 80 °C. $M_{n,th} = ([M]_0/[M]) \times [MMA] \times \text{Conv.}\% + M_{w,EBiB}$. CR^a refers to the residual catalyst present in the organic polymer solution phase, measured by ICP-MS

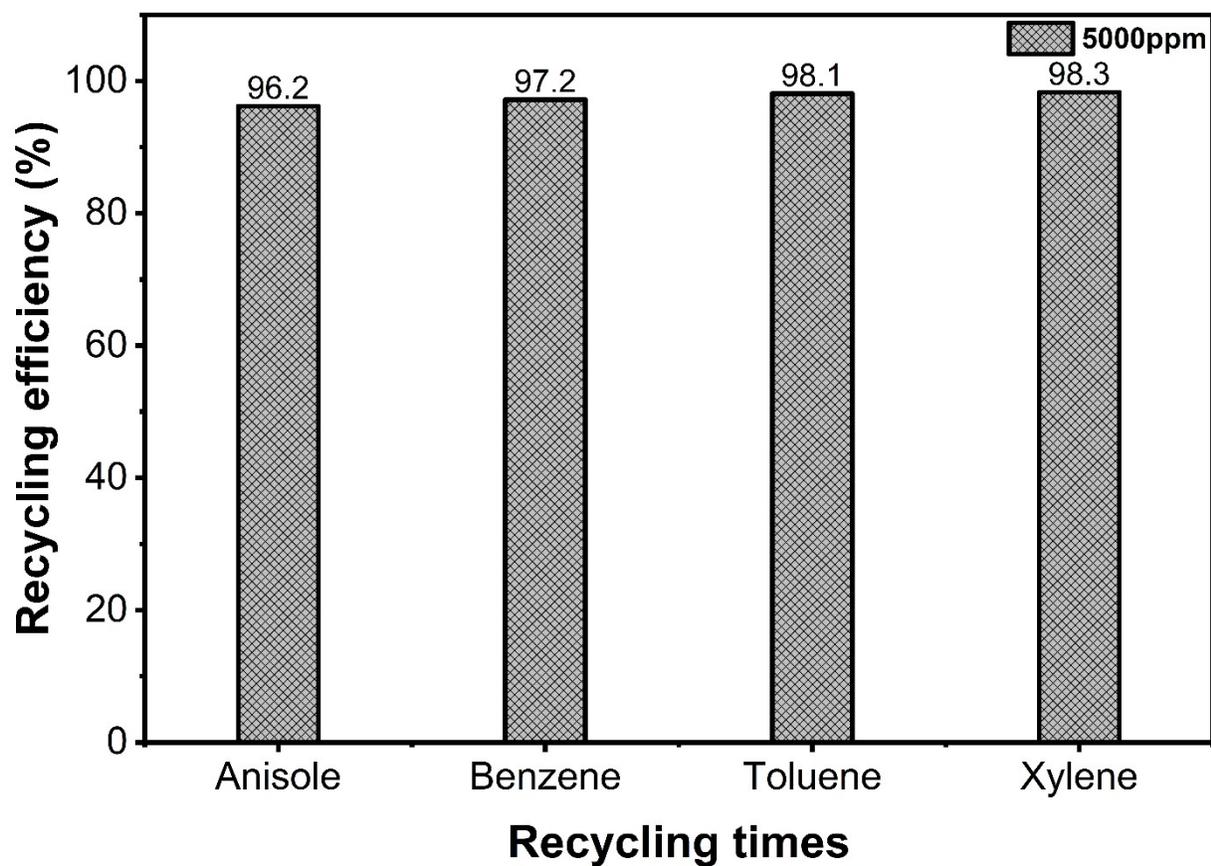


Fig. S5 Recycling efficiency represented as a percentage of residual copper catalyst retained in the PILL1 phase relative to initial copper catalyst content, determined by ICP-MS, in four different solvents. Polymerization conditions: $[MMA]_0/[EBiB]_0/[CuBr_2]_0/[PILL1]_0/[AIBN]_0 = 200/1/1/4/1$, $V_{MMA} = 1$ mL, $V_{anisole} = 2$ mL, temperature = 80 °C

References

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