

Comparative evaluation of electro-oxidation coupled with UV irradiation (UV/EO) and conventional oxidation processes (UV irradiation, chlorination, electro-oxidation, UV/Chlorine) for atenolol removal: Role of operating parameters, energy performance, and toxicity

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Supplementary text-1 •OH and •Cl calculation

•OH concentration

$$\frac{d[pCBA]}{dt} = -k_{pCBA-\bullet OH}[\bullet OH][pCBA] \quad (1)$$

Comparing with the pseudo 1st-order equation for pCBA removal,

$$k'_{pCBA} = k_{pCBA-\bullet OH}[\bullet OH] \quad (2)$$

where $k_{pCBA-\bullet OH}$ is the 2nd-order reaction rate constant for pCBA with •OH ($5 \times 10^9 \text{ M}^{-1}\text{s}^{-1}$) (Rosenfeldt, Linden, Canonica, & von Gunten, 2006). k'_{pCBA} is the observed kinetic data of pCBA removal (pseudo 1st-order degradation rate constant). [•OH] and [pCBA] are concentrations of •OH and pCBA, respectively.

Substitute the k'_{pCBA} of 0.0220 min^{-1} or $3.67 \times 10^{-4} \text{ s}^{-1}$ in the equation 2,

$$3.67 \times 10^{-4} \text{ s}^{-1} = 5.00 \times 10^9 \text{ M}^{-1}\text{s}^{-1} \times [\bullet OH]$$

$$\text{Thus, } [\bullet OH] = 7.34 \times 10^{-14} \text{ M}$$

RCS concentration

$$\frac{d[BA]}{dt} = -(k_{BA-\bullet OH}[\bullet OH] + k_{BA-Cl\bullet}[Cl\bullet])[BA] \quad (3)$$

Comparing with the pseudo 1st-order equation for BA removal,

$$k'_{BA} = k_{BA-\bullet OH}[\bullet OH] + k_{BA-Cl\bullet}[Cl\bullet] \quad (4)$$

where $k_{BA-\bullet OH}$, and $k_{BA-Cl\bullet}$ are 2nd-order reaction rate constants for BA with •OH ($5.9 \times 10^9 \text{ M}^{-1}\text{s}^{-1}$) and BA with Cl• ($1.8 \times 10^{10} \text{ M}^{-1}\text{s}^{-1}$), respectively (Wang, Wu, Huang, Wang, & Hu, 2016; Hoang, et al., 2022). k'_{BA} is the observed kinetic data of BA degradation (pseudo 1st-order degradation rate constant). [•OH] and [Cl•] are amount of •OH and Cl•, respectively.

Substitute the k'_{BA} of 0.0286 min^{-1} or $4.77 \times 10^{-4} \text{ s}^{-1}$ in the equation 4,

$$4.77 \times 10^{-4} \text{ s}^{-1} = (5.90 \times 10^9 \text{ M}^{-1}\text{s}^{-1})(7.34 \times 10^{-14} \text{ M}) + 1.80 \times 10^{10} \text{ M}^{-1}\text{s}^{-1}[Cl\bullet]$$

$$\text{Thus, } [\text{Cl}\cdot] = 2.42 \times 10^{-15} \text{ M}$$

Supplementary text-2 Calculation of kinetic degradation rate of ATL by $\text{Cl}\cdot$ ($k_{\text{ATL-Cl}\cdot}$)

$$\frac{d[\text{ATL}]}{dt} = -(k_{\cdot\text{OH}}[\cdot\text{OH}] + k_{\text{Cl}\cdot}[\text{Cl}\cdot] + k_{\text{FAC}}[\text{FAC}] + k_{\text{UV}}[\Phi\epsilon\text{I}])[\text{ATL}] \quad (5)$$

Comparing with the pseudo 1st-order kinetic model of ATL removal,

$$k'_{\text{UV/EO-ATL}} = k_{\cdot\text{OH}}[\cdot\text{OH}] + k_{\text{Cl}\cdot}[\text{Cl}\cdot] + k_{\text{FAC}}[\text{FAC}] + k_{\text{UV}}[\Phi\epsilon\text{I}] \quad (6)$$

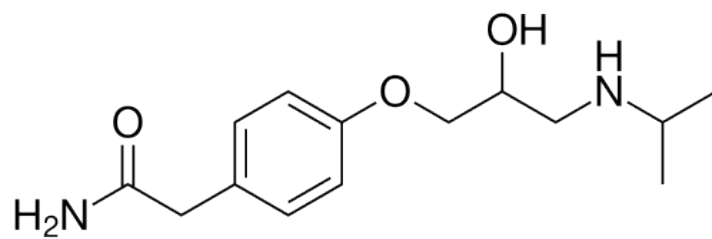
$$k'_{\text{FAC-ATL}} = k_{\text{FAC}}[\text{FAC}] \quad (7)$$

$$k'_{\text{UV-ATL}} = k_{\text{UV}}[\Phi\epsilon\text{I}] \quad (8)$$

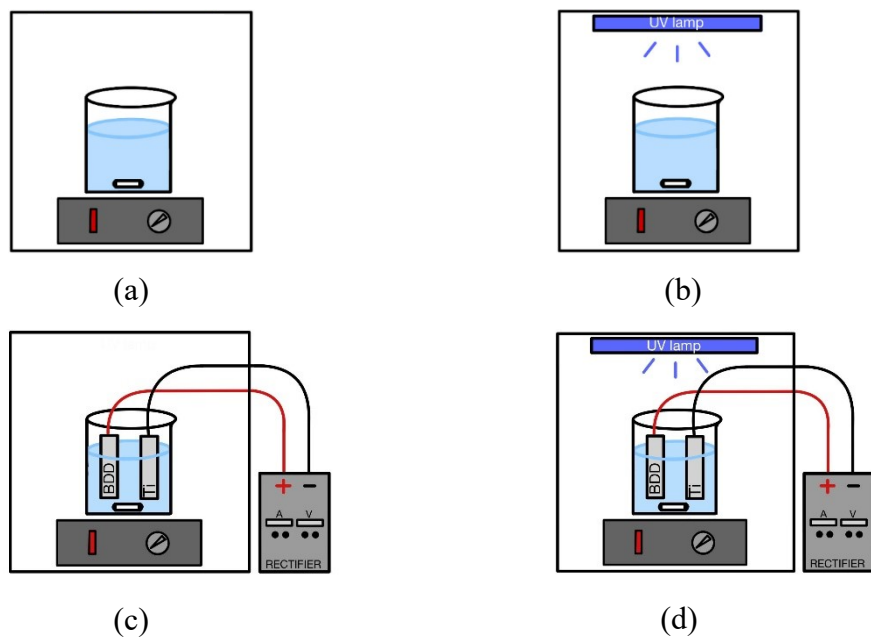
where $k'_{\text{UV/EO-ATL}}$, $k'_{\text{FAC-ATL}}$, and $k'_{\text{UV-ATL}}$ are the observed kinetic data of ATL degradation by the UV/EO process, chlorination, and UV irradiation, respectively. $k_{\cdot\text{OH}}$, $k_{\text{Cl}\cdot}$, k_{FAC} , and k_{UV} are 2nd-order reaction rate constants of ATL to $\cdot\text{OH}$, $\text{Cl}\cdot$, FAC, and UV light, respectively. $[\cdot\text{OH}]$, $[\text{Cl}\cdot]$, and $[\text{FAC}]$ are concentrations of $\cdot\text{OH}$, $\text{Cl}\cdot$, and FAC, respectively. Φ , ϵ , and I are quantum yield of ATL, molar absorption of ATL, and the UV fluence rate, respectively.

From the supplementary figure-1, $k'_{\text{UV/EO-ATL}}$, $k'_{\text{UV-ATL}}$, and $k'_{\text{FAC-ATL}}$ were 0.0599 min^{-1} ($9.98 \times 10^{-4} \text{ s}^{-1}$), 0.0025 min^{-1} ($4.17 \times 10^{-5} \text{ s}^{-1}$), 0.0035 min^{-1} ($5.83 \times 10^{-5} \text{ s}^{-1}$), respectively. $k_{\cdot\text{OH-ATL}}$ was $7.10 \times 10^9 \text{ M}^{-1}\text{s}^{-1}$ (Wols, Harmsen, Beerendonk, & Hofman-Caris, 2014). Substitute all values in the equation 6;

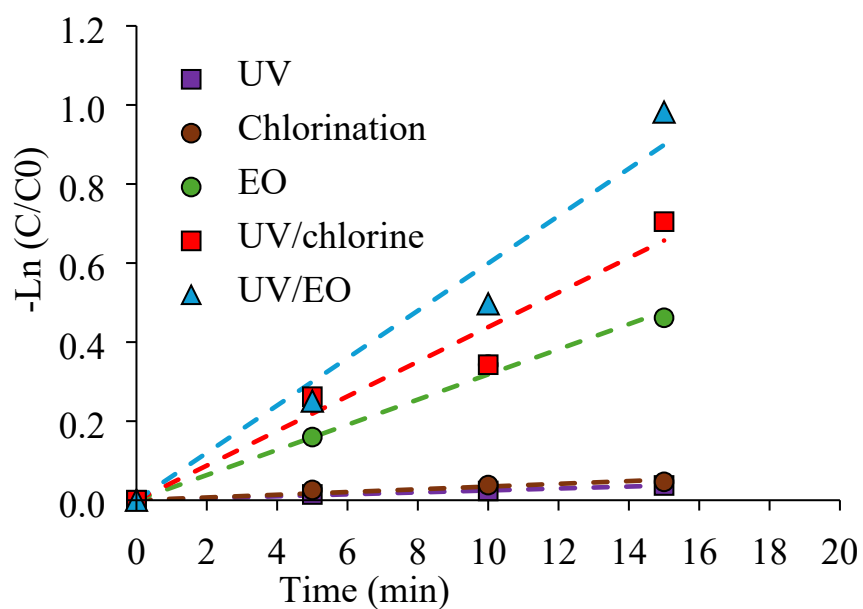
$$\begin{aligned} 9.98 \times 10^{-4} \text{ s}^{-1} &= (7.10 \times 10^9 \text{ M}^{-1}\text{s}^{-1})(7.34 \times 10^{-14} \text{ M}) + k_{\text{Cl}\cdot}(2.42 \times 10^{-15} \text{ M}) \\ &\quad + (5.83 \times 10^{-5} \text{ s}^{-1}) + (4.17 \times 10^{-5} \text{ s}^{-1}) \\ k_{\text{Cl}\cdot\text{-ATL}} &= 1.55 \times 10^{11} \text{ M}^{-1}\text{s}^{-1} \end{aligned}$$



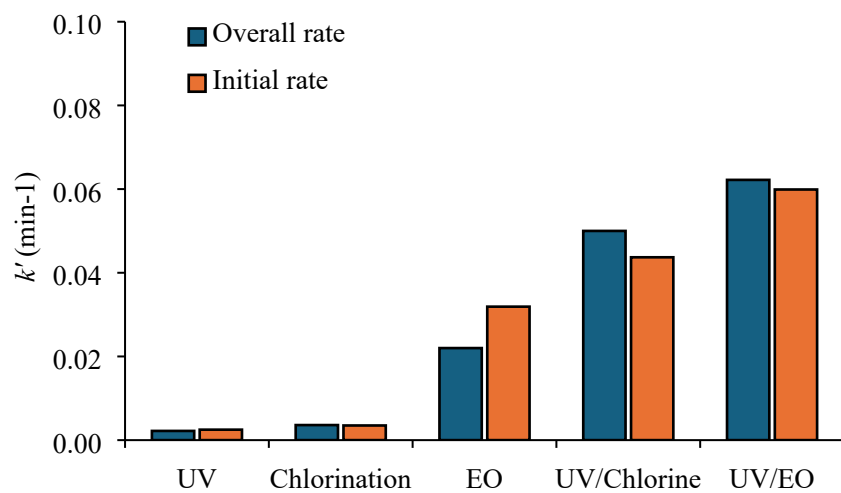
Supplementary figure-1 ATL structure



Supplementary figure-2 Experimental setup (a) Chlorination, (b) UV irradiation and UV/chlorine, (c) EO process, and (d) UV/EO process

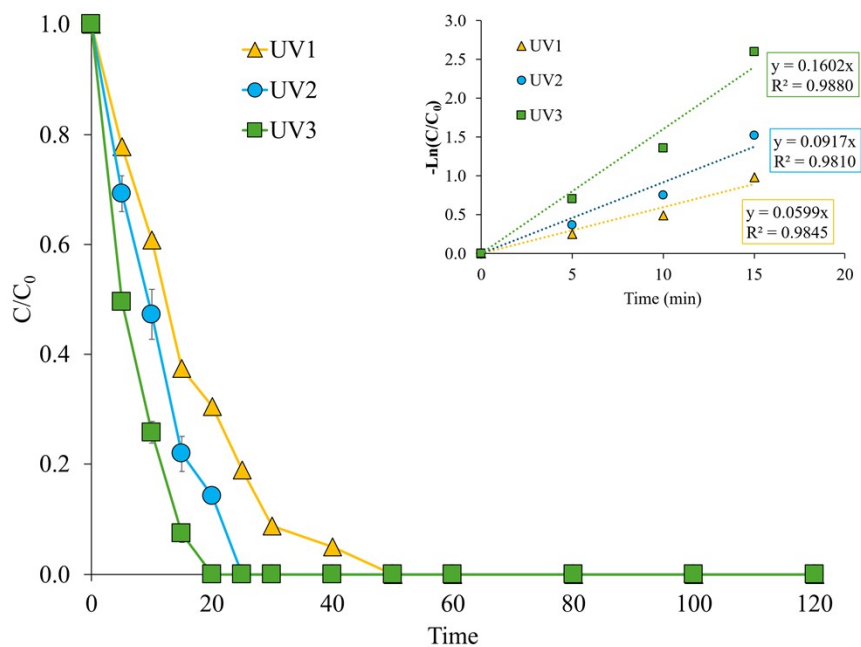


(a)

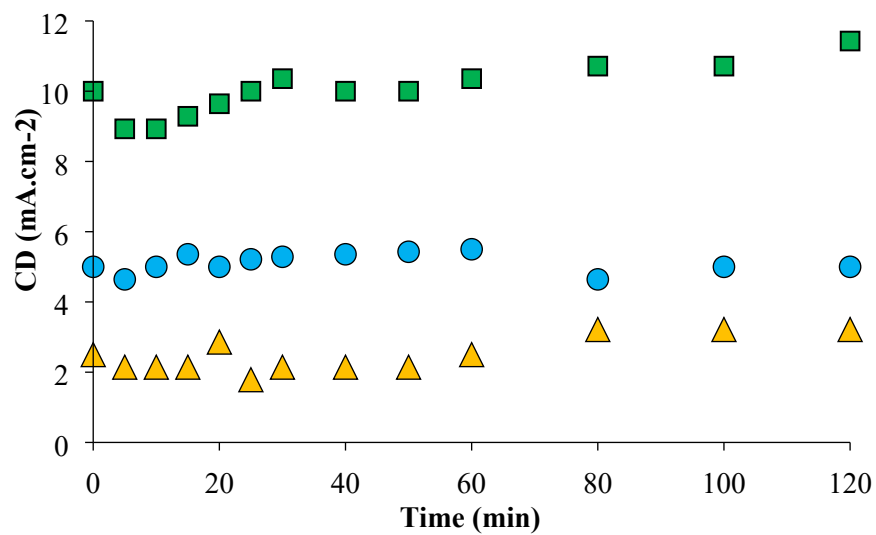


(b)

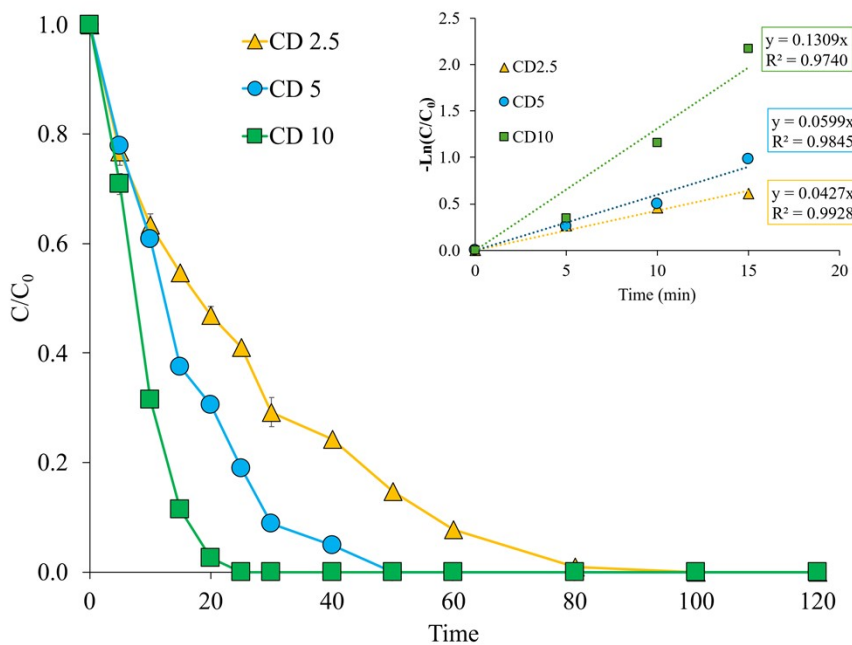
Supplementary figure-3 Kinetic ATL degradation by the initial rate method (a) and overall rate (b) for chlorination, UV irradiation, EO, UV/Chlorine, and UV/EO



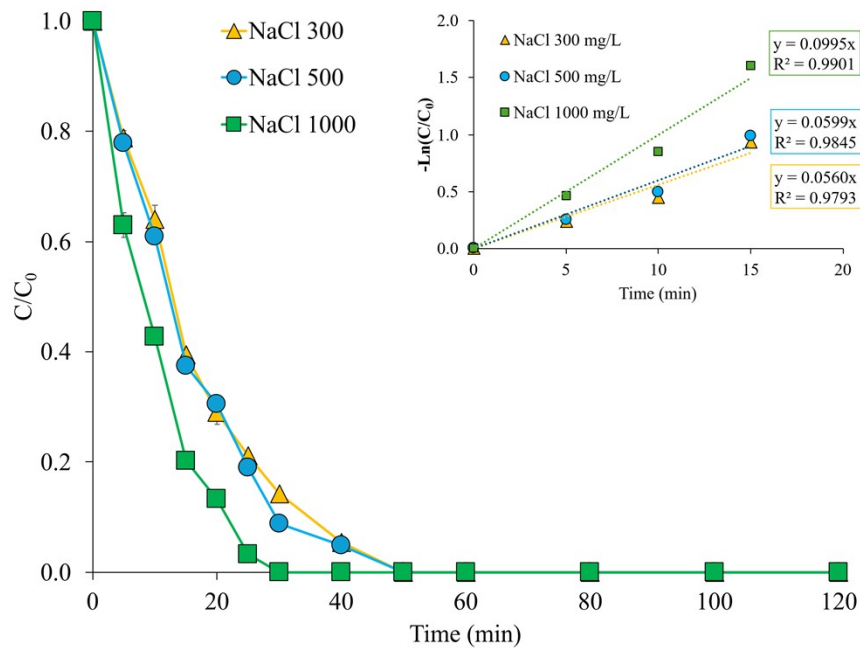
Supplementary figure-4 Effect of UV lamp on kinetic degradation of ATL in UV/EO



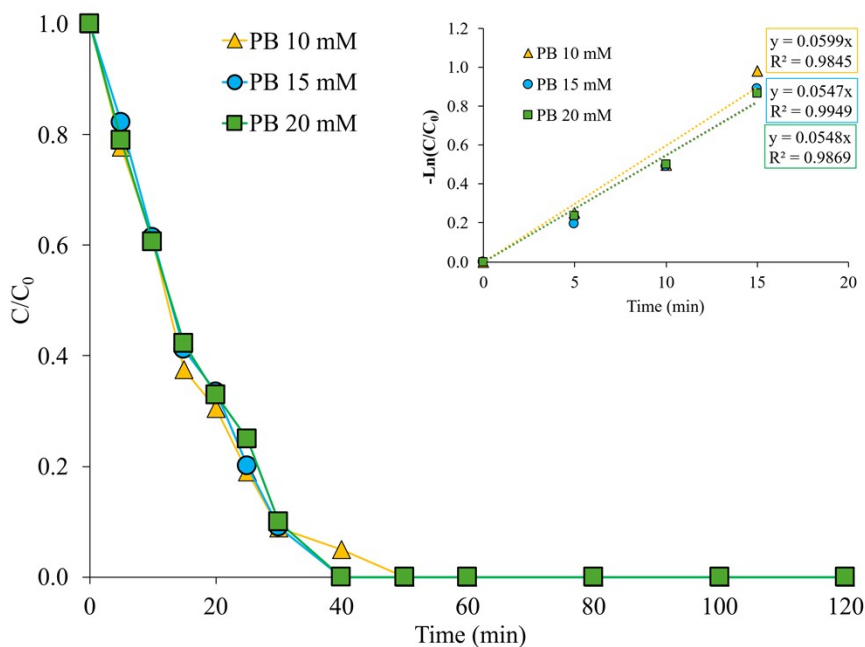
Supplementary figure-5 The CD profile of UV/EO



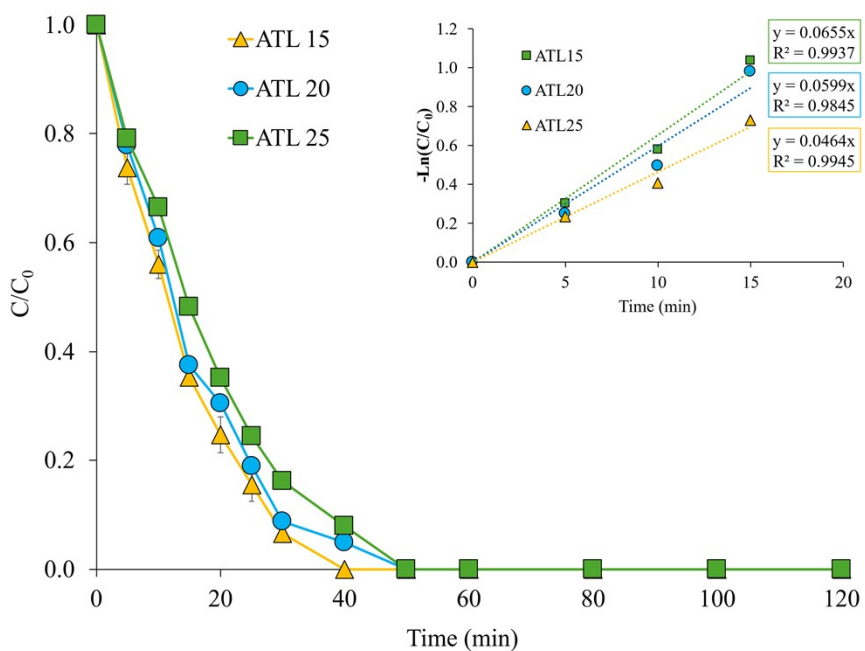
Supplementary figure-6 Effect of CD on kinetic degradation of ATL in UV/EO



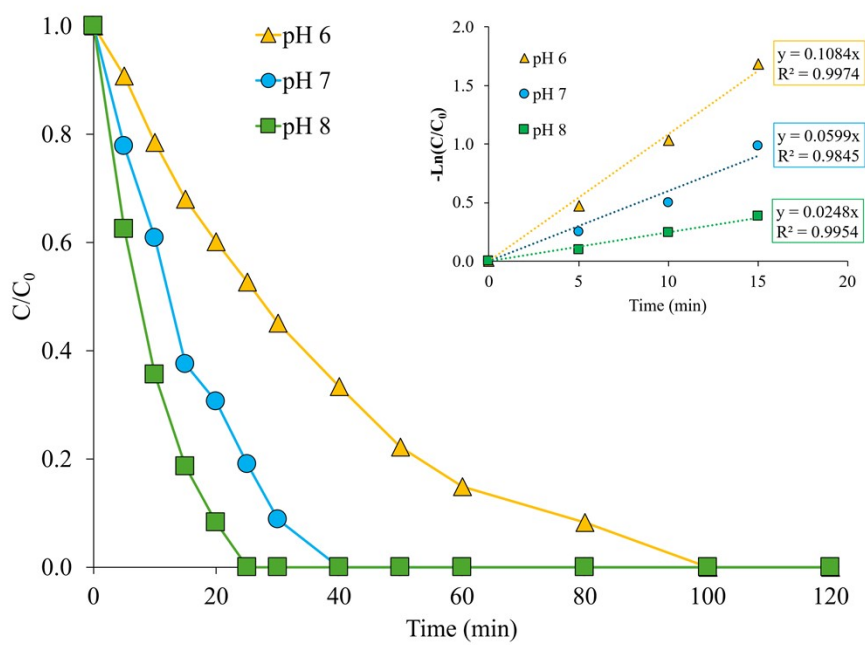
Supplementary figure-7 Effect of NaCl on kinetic degradation of ATL in UV/EO



Supplementary figure-8 Effect of phosphate buffer concentration on kinetic degradation of ATL in UV/EO



Supplementary figure-9 Effect of ATL concentrations on kinetic degradation of ATL in UV/EO



Supplementary figure-10 Effect of pH on kinetic degradation of ATL in UV/EO