

Zr-Gallic acid based metal organic compound as adsorbent for extraction of Uranium (VI) from Nitrate solution: Adsorption behaviors and mechanisms

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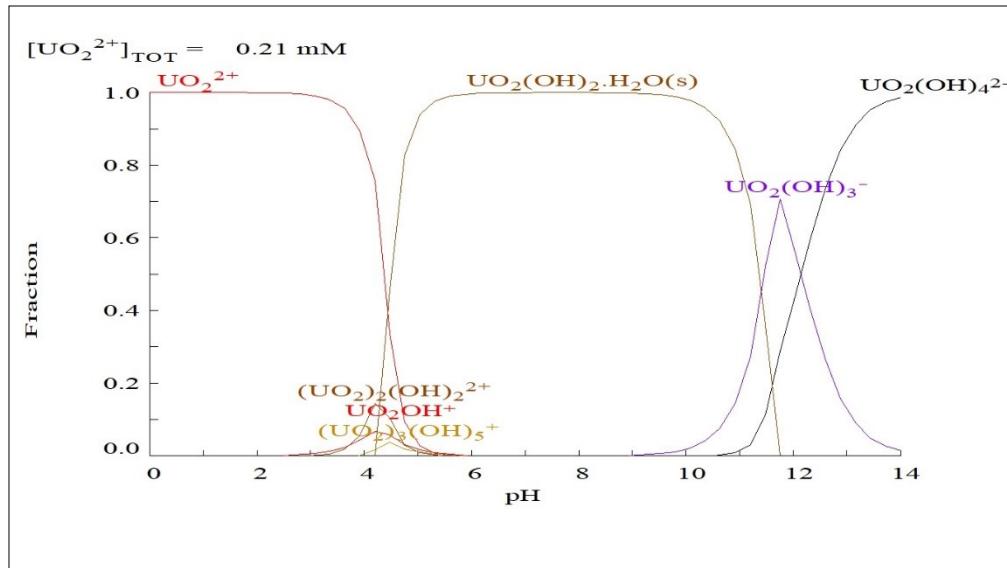


Figure S1: *U(VI) speciation as a function of solution pH, calculated using Hydra-MEDUSA equilibrium calculation program [1].*

1) Hussein AEM, Taha MH (2013) Uranium removal from nitric acid raffinate solution by solvent immobilized PVC cement. *J Radioanal Nucl Chem* 295:709–715. [https://doi.org/10.1007/S10967-012-2158-3/TABLES/2](https://doi.org/10.1007/S10967-012-2158-3)

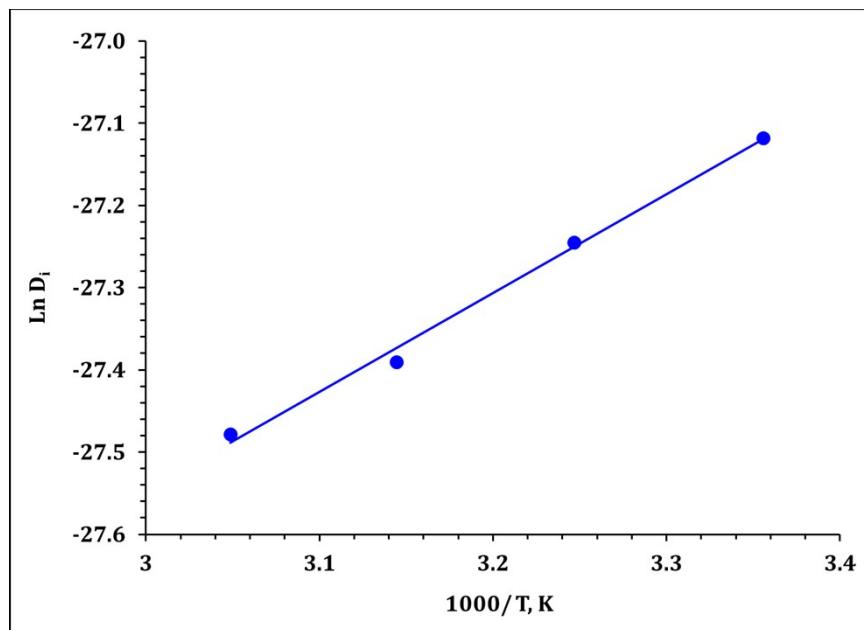


Figure S2: Arrhenius plot for U(VI) sorption onto prepared composite

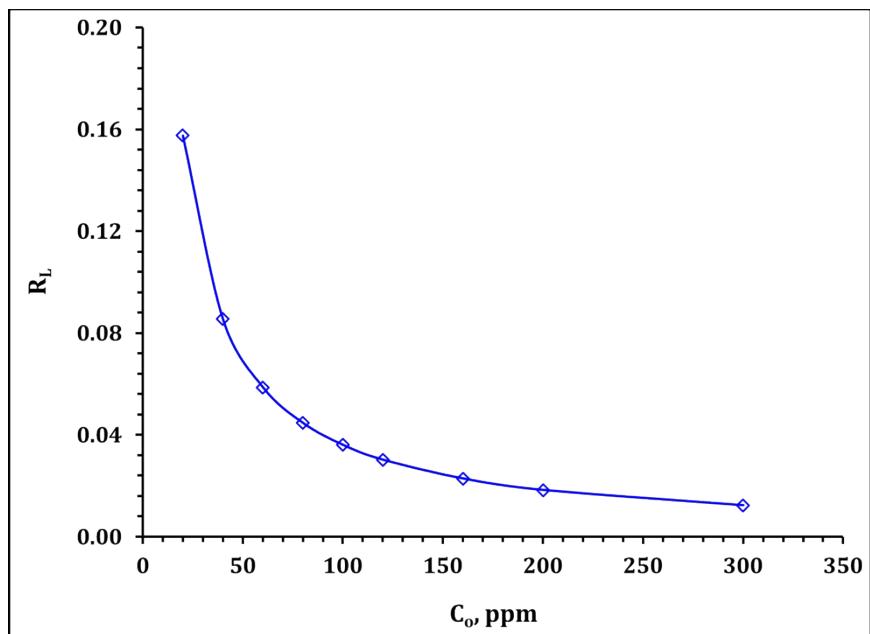


Figure S3: Separation factor R_L of U(VI) adsorption process.

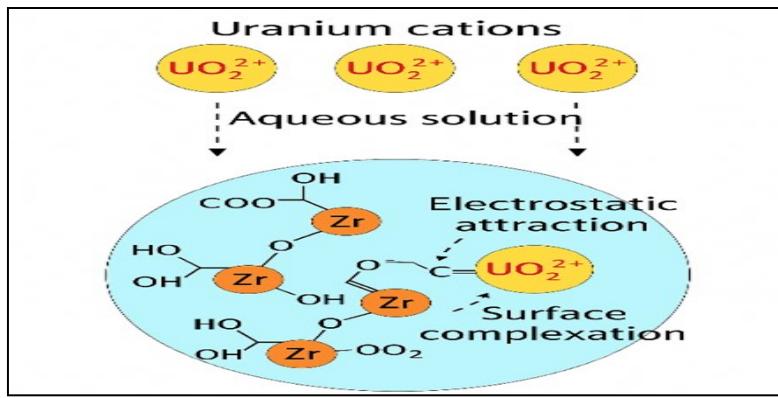


Figure S4. Schematic representation of the proposed adsorption mechanism of U(VI) onto Zr-GA

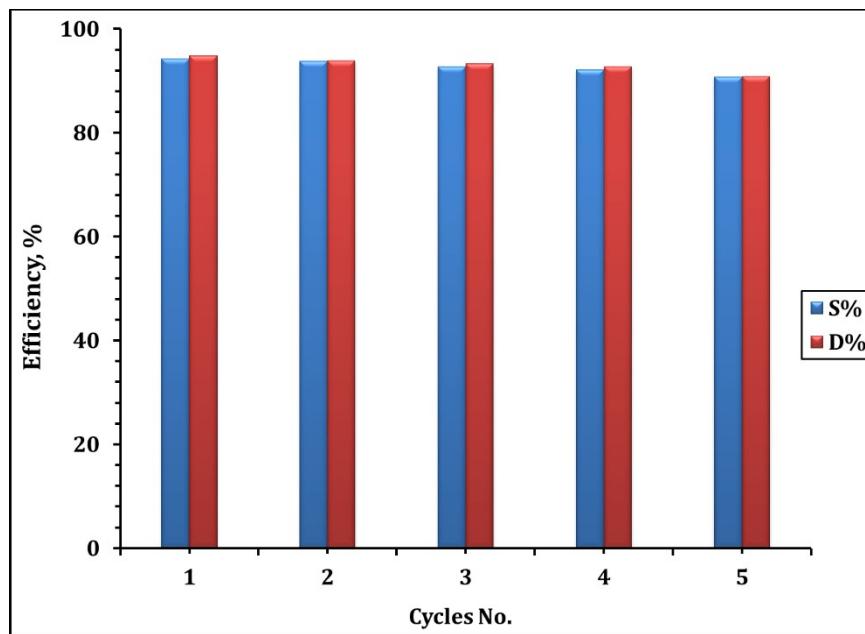


Figure S5: Sorption/ desorption cycles for uranium capture process.

Table S1: Kinetic, isotherm, and thermodynamics equations for U(VI) adsorption process [1-8].

Kinetics	Equations
Pseudo-first-order	$q_t = q_1 (1 - e^{-k_1 t})$
Pseudo-second-order	$q_t = \frac{1}{(1 k_2 q_2^2) + (t q_2)}$
Intra-particle diffusion model (IPD)	$q_t = K_{id} t^{0.5} + C_i$
Boyd model	$Bt = -0.4977 - \ln(1 - F)$
Isotherms	Equations
Langmuir model	$q_e = \frac{q_m k_L C_e}{1 + k_L C_e}$
Freundlich model	$q_e = K_F C_e^{1/n_F}$
Sips model	$q_e = \frac{q_S (k_S C_e)^{mS}}{1 + (k_S C_e)^{mS}}$
Thermodynamics	Equations
	$\log K_C = -\frac{\Delta H^o}{2.303 R} X \frac{1}{T} + C$ $-\Delta G^o = 2.303 RT \log K_C$ $\Delta G^o = \Delta H^o - T \Delta S^o$
Fitting	Equations
Coordination coefficient (R^2)	$R^2 = 1 - \frac{\sum_1^n (q_{exp} - q_{pred})^2}{\sum_1^n (q_{exp} - \bar{q}_{exp})^2}$

q_e (mg g⁻¹) is the equilibrium concentration of U(VI) species, and q_t (mg g⁻¹) is the adsorbed amount of U(VI) species ions after time t (min), C_e (mg L⁻¹) is equilibrium concentration of U(VI) species. k_1 (min⁻¹) and k_2 (min⁻¹) are the rate constants for the pseudo first and second order, respectively. K_{id} (mg/g, min^{0.5}) is a rate constant, and C is the thickness of the boundary layer. F is

the ratio of the sorbed quantity at time t and that sorbed at equilibrium; B is the time constant and it equals $\pi^2 D_i / r_o^2$ [4]; D_i is the effective diffusion coefficient of metal ions; r_o is the radius of the solid particles; and n is an integer. q_m and q_s are the maximum sorption capacity (mg. g^{-1}) of Langmuir and Sips models. k_L (L. mg^{-1}), K_F (L/ mg), and K_S (L/ mg) are represent the constants of Langmuir, Freundlich, and Sips models. n refer to the sorption intensity, q_s is the theoretical isotherm saturation capacity (mg/g). K_C is a non-dimensional equilibrium constant and it equals $K_d \times 1000 \times \rho$ [5]; T is the temperature (K), R is the universal gas constant ($8.314 \text{ J mol}^{-1} \text{ K}^{-1}$), ρ is solution density g/ L , and C is a constant. R^2 is the coordination coefficient, the number of test points is n , the experimental equilibrium capacity is q_{exp} (mg g^{-1}), while the predicted capacity is q_{pred} (mg g^{-1}).

Table S2: Surface charges and mean particle sizes of Zr-GA before and after adsorption process

<i>Analysis</i>	<i>Before</i>	<i>After</i>
<i>DLS analysis, nm</i>	549.5	1116.1
<i>Zeta potential, mV</i>	-46.69	-26.49

Table S3: The values of Morris-Weber model parameters.

		25 °C	35 °C	45 °C	55 °C
Weber and Morris model	k_i ($\text{mg/g min}^{1/2}$)	1.06	0.88	0.67	0.44
	C	20.5	13.5	10.4	5.3
	R^2	0.98	0.97	0.98	0.96

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