

Supplementary Information

Highly efficient CO₂ hydrogenation to long-chain linear α -olefins via CO intermediate enrichment over Na/FeMn/ZrO₂ catalysts

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1. Catalyst preparation

The Na/FeMn/ZrO₂ catalyst was prepared via a pre-coordination anchoring strategy. Typically, 2.02 g Fe(NO₃)₃·9H₂O (AR, Sinopharm Chemical Reagent Co., Ltd), 1.26 g Mn(NO₃)₂·6H₂O (AR, Sinopharm Chemical Reagent Co., Ltd), and 11.69 g ethylene diamine tetraacetic acid (AR, Sigma Aldrich) was dissolved into 37.28 g of deionized water under stirring to form a solution, to which 6.52 g of ZrO₂ (AR, Sinopharm Chemical Reagent Co., Ltd) was added with continuous stirring for 5 h. Subsequently, the mixture was heated to 120 °C for evaporation and drying under stirring, and then calcined at 650 °C for 6 h to obtain the FeMn/ZrO₂ sample. The Na/FeMn/ZrO₂ catalyst was fabricated by an impregnation method. In brief, 0.05 g Na₂CO₃ (AR, Sinopharm Chemical Reagent Co., Ltd) was dissolved into 2.0 g of deionized water. The resultant solution was added dropwise to 1.0 g of FeMn/ZrO₂ sample under ultrasonic condition. After drying in vacuum at 60 °C for 12 h, the Na/FeMn/ZrO₂ catalyst was obtained. Unless specified otherwise, Na and FeMn loading were fixed at 2 wt% and 30 wt%, respectively. The ZrO₂ used in the aforementioned catalysts is monoclinic ZrO₂.

The reference of Na/FeMn/SiO₂ catalysts were prepared using pre-coordination anchoring strategy. The pre-coordination anchoring strategy primarily involved the formation of metal complexes through ligand-metal ion coordination. The carboxyl groups on the complex surface esterify with hydroxyl groups on the support surface, anchoring the metal ions to the support. Subsequently, reduction and carbonization treatments were applied to form the interfacial structure. In brief, a certain amount of Fe(NO₃)₃·9H₂O (AR, Sinopharm Chemical Reagent Co., Ltd), Mn(NO₃)₂·6H₂O (AR, Sinopharm Chemical Reagent Co., Ltd), ethylene diamine tetraacetic acid (AR, Sigma Aldrich) were dissolved into deionized water under stirring. Then,

SiO₂ (AR, Sigma Aldrich) was added to the above solution with continuous stirring for 5 h. Subsequently, the solution was heated to 120 °C for evaporation and drying, and then calcined at 650 °C for 6 h to obtain the FeMn/SiO₂ sample. Na/FeMn/ZrO₂ catalyst was prepared by impregnating method. Typically, Na₂CO₃ (AR, Sinopharm Chemical Reagent Co., Ltd) was dissolved into deionized water, and then the above solution was added dropwise to FeMn/SiO₂ sample under ultrasonic condition, followed by drying in vacuum at 60 °C for 12 h to obtain Na/FeMn/SiO₂ catalyst. The weight percent of Na and FeMn are fixed at 2 wt% and 30 wt%, respectively.

The reference Na/FeMn catalyst were prepared by sol-gel method. Typically, a certain amount of Fe(NO₃)₃·9H₂O, Mn(NO₃)₂·6H₂O, and ethylene diamine tetraacetic acid were dissolved into deionized water to form uniform solution under stirring. After that, evaporation dried at 120 °C under stirring, and then calcined at 650 °C for 5 h to obtain FeMn samples. Na/FeMn catalyst was prepared by impregnating method. Na₂CO₃ was dissolved into deionized water, and then was dropped in the FeMn sample, dried at 60 °C in vacuum for overnight. The final catalyst was denoted as Na/FeMn. The Fe and Na/Fe were prepared by the above-mentioned process.

2. Catalyst characterization

X-ray diffraction (XRD) spectra were performed on a Rigaku RINT 2400 X-ray diffractometer equipped using Cu K α radiation at 40 kV and 20 mA with a scanning speed of 2 °·min⁻¹ and step width of 0.02 °. *In situ* XRD analysis was conducted on a Rigaku SmartLab equipped with Cu K α radiation. Samples were reduced in flowing H₂ (30 mL·min⁻¹) with programmed heating from room temperature to 600 °C. To monitor catalyst phase evolution during the

reaction process, the catalyst was first reduced at 400 °C for 1 h. After pretreatment, the sample was cooled down to 100 °C, followed by reaction gas introduction and data recording.

Scanning electron microscopy (SEM) images were taken on a JEOL JSM-6360LV microscope operated at an accelerating voltage of 1.5 kV. Transmission electron microscopy (TEM) and elemental mapping images were obtained on a JEOL JEM-2100F at an acceleration voltage of 200 kV.

N₂ sorption was conducted on a Micromeritics NOVA2200e analyzer. Prior to the measurement, the sample was degassed in vacuum at 200 °C for 5 h. The surface area was calculated by the Brunauer-Emmett-Teller (BET) method. The average pore size and pore volume were determined by the Barrett-Joyner-Halenda (BJH) method.

Hydrogen temperature-programmed reduction (H₂-TPR) measurements were performed on a BELCAT-II-T-SP with a thermal conductivity detector (TCD). Specifically, 50 mg catalyst was loaded into a U-shaped quartz tube reactor and pretreated at 150 °C for 2 h in flowing He. After that, the sample was cooled down to 100 °C, followed by reduction in flowing H₂ (30 mL·min⁻¹) at 10 °C·min⁻¹ up to 600 °C.

Temperature-programmed desorption (TPD) was performed on a BELCAT-II-T-SP instrument with a TCD. Specifically, 50 mg sample was loaded into a quartz tube reactor and reduced at 400 °C for 2 h in flowing H₂ (30 mL·min⁻¹). After that, the sample was cooled down to 50 °C and saturated with CO₂ or CO. The sample was flushed in flowing He for 0.5 h to remove the gaseous CO₂ or CO. Then, TPD was carried out in flowing He (30 mL·min⁻¹) from 60 to 300 °C at 10 °C·min⁻¹.

X-ray photoelectron spectroscopy (XPS) analysis was performed on a Thermo Fisher

Scientific ESCALAB 250Xi instrument using an Al K α X-ray radiation source. The binding energy was calibrated by C 1s of adventitious carbon (284.6 eV).

The ^{57}Fe Mössbauer spectra (MES) were carried out on a wissel spectrometer driving with a proportional counter at room temperature. The radioactive source was $^{57}\text{Co(Pd)}$ moving in a constant acceleration mode. The components of iron phases were identified based on their Mössbauer parameters including isomer shift, quadruple splitting and magnetic hyperfine field.

H_2 -temperature programmed surface reaction (H_2 -TPSR) experiments were performed on a Micromeritics AutoChem II 2920 instrument. Specifically, the spent catalyst was purged with Ar at 320 °C for 1 h, followed by *in situ* reduction with H_2 for 1 h. After cooling to 50 °C, the catalyst was exposed to a 5%CO/Ar mixture gas for 30 min. The sample was then purged with Ar at 50 °C for 30 min. Subsequently, H_2 was introduced into the reactor with a programmed temperature ramp from 50 °C to 800 °C. Mass spectrometry (MS) signals for CO ($m/z = 28$) and H_2 ($m/z = 2$) were recorded.

In situ diffuse reflectance infrared fourier transform spectroscopy (DRIFTS) was performed on a Nicolet Nexus 470 FTIR spectrometer equipped with a diffuse reflectance attachment and a mercury cadmium telluride (MCT) detector. Prior to the test, 20 mg sample was placed in a diffuse reflectance infrared cell with a ZnSe window. The sample was reduced at 400 °C for 1 h with a pure H_2 flow of 30 mL/min, and then cooled down to 320 °C and the background spectrum was recorded. After the feedstock was introduced into the cell with flow of 30 mL/min, and the spectra were recorded by collecting 32 scans at 4 cm^{-1} resolution.

CO-DRIFTS was performed on a Nicolet 6700 spectrometer equipped with a diffuse reflectance cell and a liquid nitrogen-cooled high sensitivity MCT detector to detect the

adsorption and desorption of CO on the catalyst surface. The samples were first loaded into a reaction chamber and reduced by 10 % H₂/Ar at a flow rate of 30 mL·min⁻¹ at 400 °C. Subsequently, 10 % CO/Ar was introduced into the reaction chamber and spectral data were collected.

3. DFT calculations

All calculations employed spin-polarized density functional theory (DFT) using the VASP software [1,2]. The exchange–correlation functional was treated within the generalized gradient approximation (GGA) using the Perdew-Burke-Ernzerhof (PBE) functional [3]. A plane-wave cutoff energy of 450 eV was applied. Valence electrons were described using the projector-augmented wave (PAW) method [4]. A Hubbard *U* correction of 5.0 eV was applied to the Ce 4f orbitals to accurately describe electron localization [5]. Ionic relaxation was performed until the maximum force on atom was below 0.05 eV/Å. van-der-Waals interactions were accounted for using the DFT-D3 method [6]. The bottom two atomic layers were fixed in position, while all other atoms were allowed to relax. Transition states were located using the climbing image nudge elastic band (CI-NEB) method. The results in Figure 7c and Figure 7d were obtained using this method.

4. Catalytic evaluation

CO₂ hydrogenation reactions were performed in a stainless steel fixed-bed reactor. In brief, 0.4 g catalyst was evenly mixed with 0.5 g quartz sand, which was then loaded in a reactor with internal diameter of 6 mm. Prior to reaction, the catalyst was *in situ* reduced at 400 °C for 8 h in flowing H₂ (60 mL·min⁻¹) at atmospheric pressure. After reduction, the catalyst was cooled down to 320 °C, and then the reactant gas mixture (gas composition as 25.03 % CO₂, 70.0 %

H₂, Ar balance) was fed into the reactor. The reaction was carried out at 320 °C, 1.5 MPa, and 7500 mL·g_{cat}⁻¹·h⁻¹. Reaction effluents were quantitatively analyzed using online gas chromatograph (GC-2014C, Shimadzu) equipped with TCD and active charcoal column (TDX-01) for Ar, CO, CH₄, and CO₂ analysis together with flame ionization detector (FID) and Rtx-1 capillary column (60 m × 0.32 mm × 5 μm) for hydrocarbon analysis. The hydrocarbon distribution was calculated from total carbon moles.

CO₂ conversion and CO selectivity were calculated as follows:

$$\text{CO}_2 \text{ conversion} = \frac{CO_{2 \text{ inlet}} - CO_{2 \text{ outlet}}}{CO_{2 \text{ inlet}}} \times 100\% \quad (1)$$

$$\text{CO selectivity} = \frac{CO_{\text{outlet}}}{CO_{2 \text{ inlet}} - CO_{2 \text{ outlet}}} \times 100\% \quad (2)$$

where, CO₂ inlet, CO₂ outlet, and CO outlet represent the moles of CO₂ at the inlet and outlet, and the moles of CO at the outlet, respectively.

The selectivity of hydrocarbon in total hydrocarbons was calculated as follows:

$$C_i \text{ hydrocarbon selectivity} = \frac{\text{mole of } C_i \text{ hydrocarbon} \times i}{\sum_{i=1}^n \text{mole of } C_i \text{ hydrocarbon} \times i} \times 100\% \quad (3)$$

5. Results and discussion

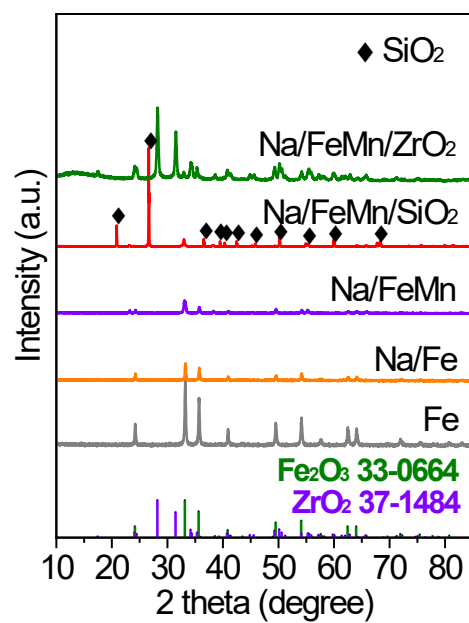


Figure S1. XRD patterns of the fresh catalysts

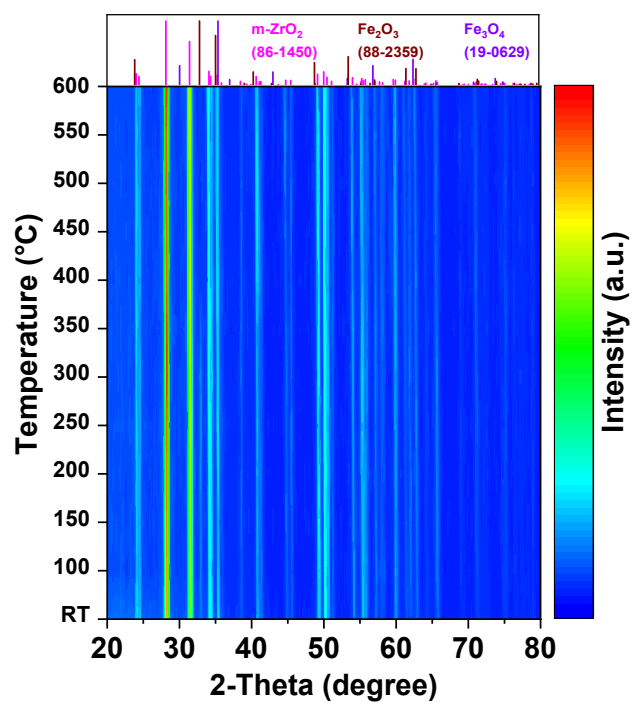


Figure S2. *In situ* XRD patterns of the Na/FeMn/ZrO₂ catalyst for H₂ reduction process.

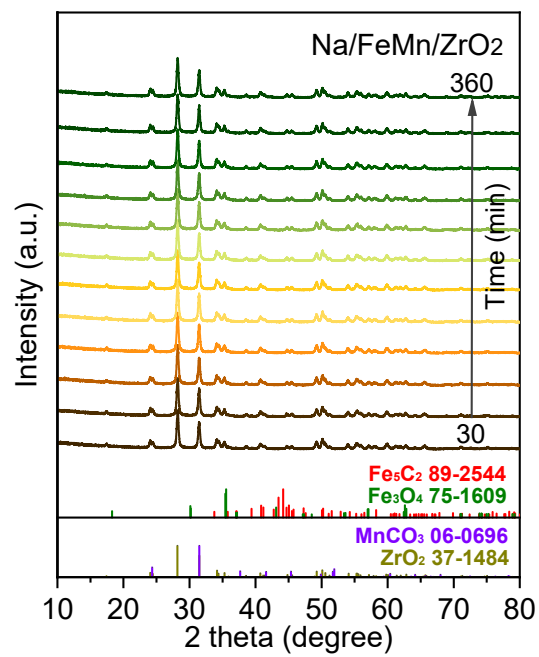


Figure S3. *In situ* XRD patterns of Na/FeMn/ZrO₂ for CO₂ hydrogenation.

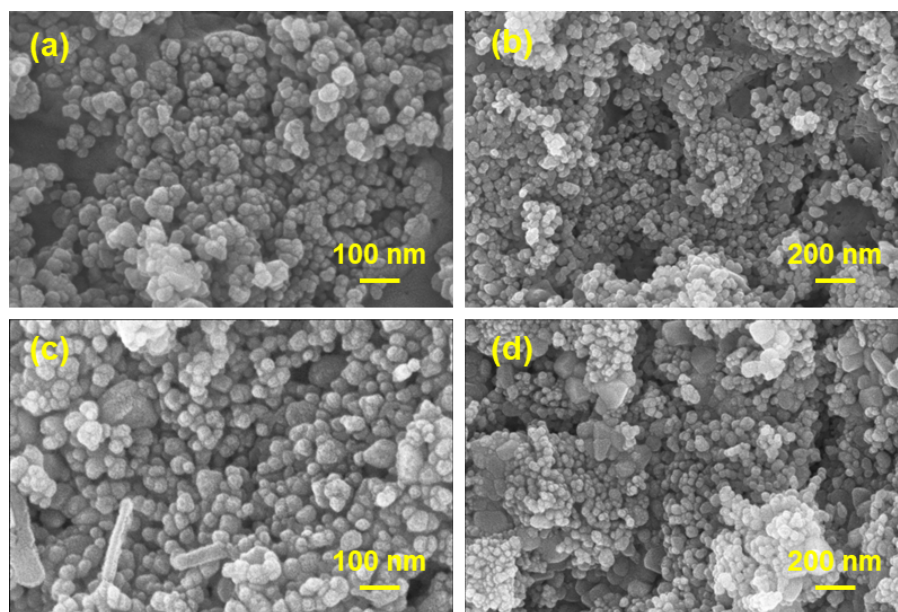


Figure S4. SEM images of the fresh Na/FeMn/ZrO₂ (a,b) and spent Na/FeMn/ZrO₂ (c,d) catalyst.

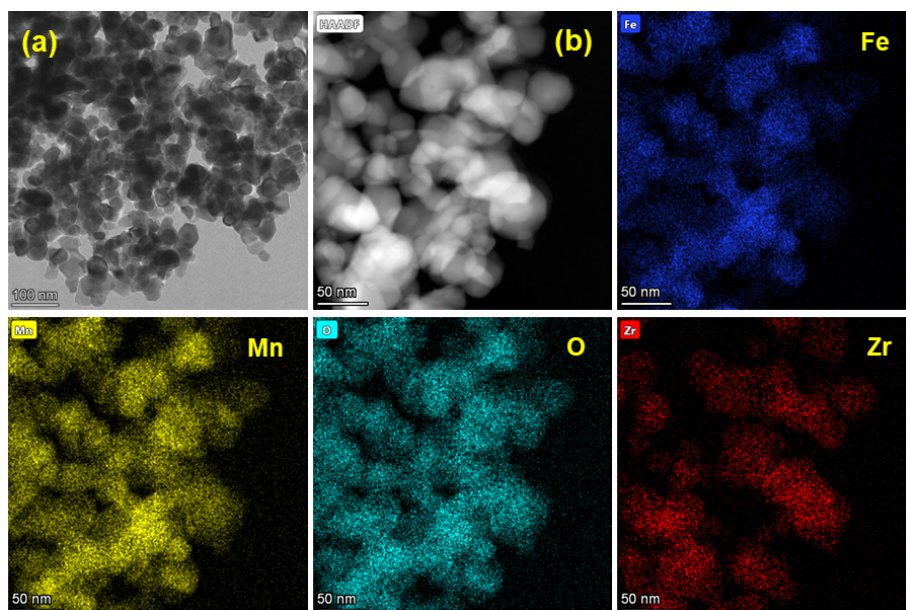


Figure S5. TEM image (a), STEM image (b) and EDS elemental mapping images of the fresh Na/FeMn/ZrO₂ catalyst.

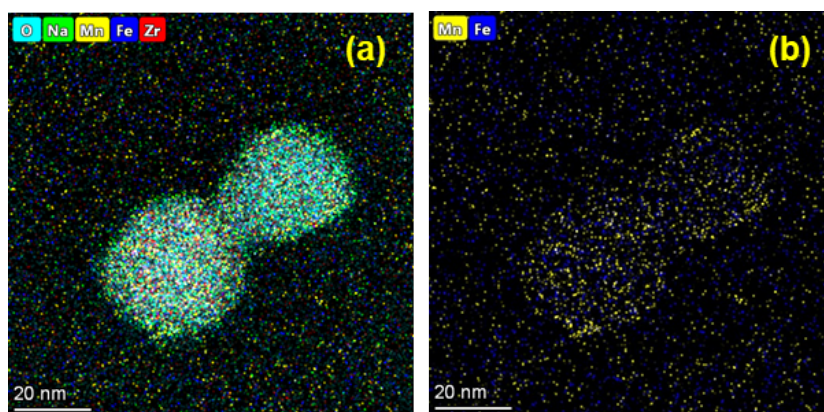


Figure S6. The EDS mapping images of (a) all elemental, (b) Fe and Mn in the spent Na/FeMn/ZrO₂ catalyst

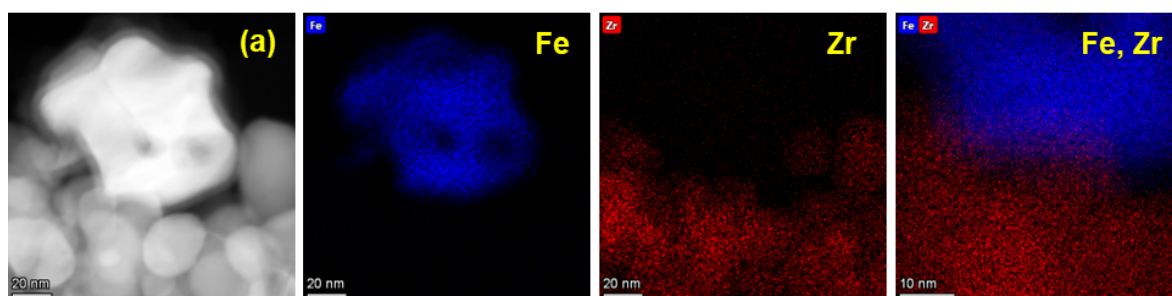


Figure S7. STEM image of spent Na/FeMn/ZrO₂ catalyst (a), EDS mapping images of all elemental (b), and the corresponding EDS elemental mapping images.

Table S1. The elemental composition of the as-prepared catalysts.

Catalysts	Element content (wt%) ^a				Dosage of raw materials (wt%) ^b			
	Na	Fe	Mn	Si or Zr	Na	Fe	Mn	Si or Zr
Na/FeMn	1.7	21.6	20.9	/	2.0	22.8	19.6	/
Na/FeMn/SiO ₂	1.7	4.7	3.5	37.4	2.0	3.6	3.1	39.1
Na/ FeMn/ZrO ₂	1.9	3.8	4.0	61.5	2.0	3.6	3.1	62.3

^aThe elemental composition of these catalysts was obtained by ICP analysis.

^bThe dosages of the elements were calculated according to the amounts of raw materials in the catalyst preparation.

Table S2. Textural properties of the prepared catalysts.

Catalysts	BET surface area ^a (m ² ·g ⁻¹)	Pore volume ^b (cm ³ ·g ⁻¹)	Average pore size ^c (nm)
Fe	23.7	0.14	11.5
Na/Fe	25.0	0.20	13.8
Na/FeMn	17.2	0.14	12.3
Na/FeMn/SiO ₂	14.7	0.04	1.7
Na/FeMn/ZrO ₂	31.5	0.26	8.7

^aBET specific surface area; ^bpore volume calculated by BJH method; ^caverage diameter of mesopores evaluated by the BJH method.

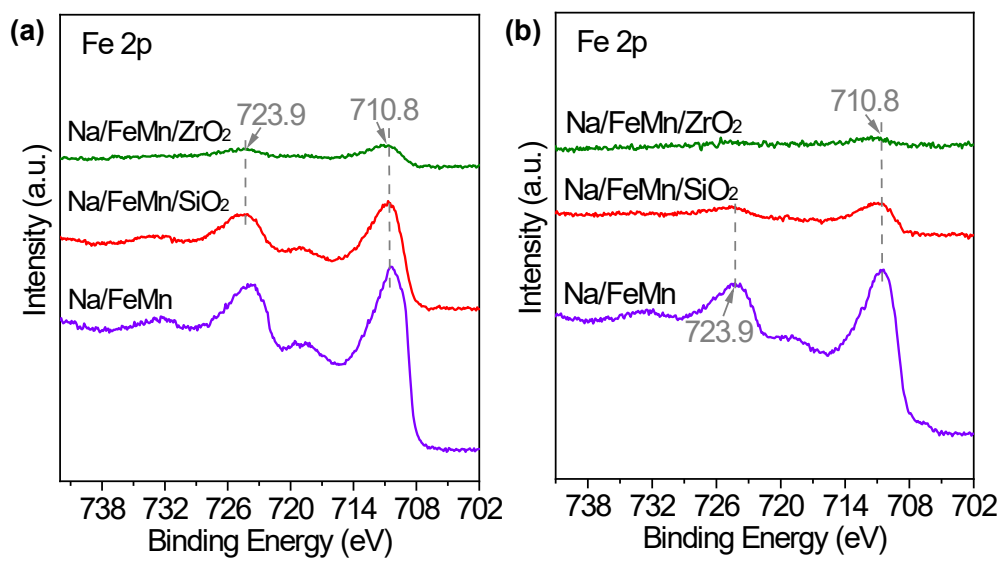


Figure S8. Fe 2p XPS spectra of fresh (a) and reduced (b) catalysts.

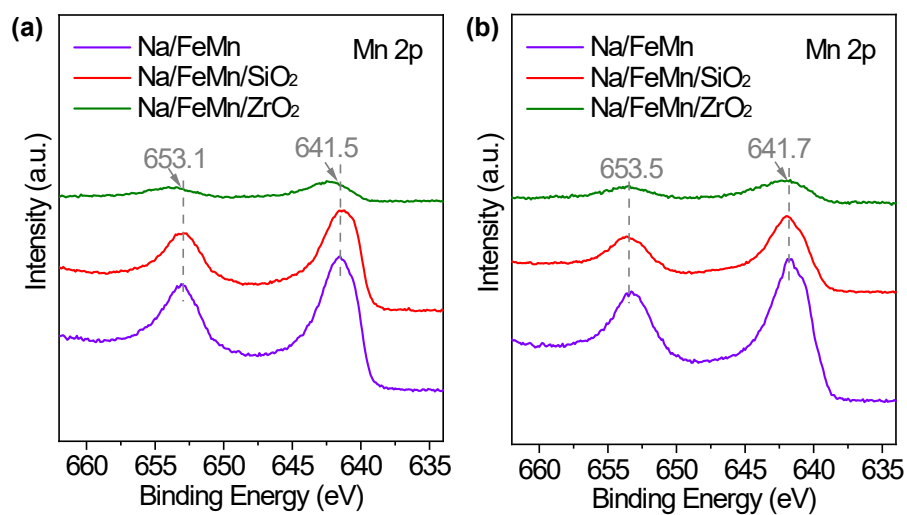


Figure S9. Mn 2p XPS spectra of fresh (a) and reduced (b) catalysts.

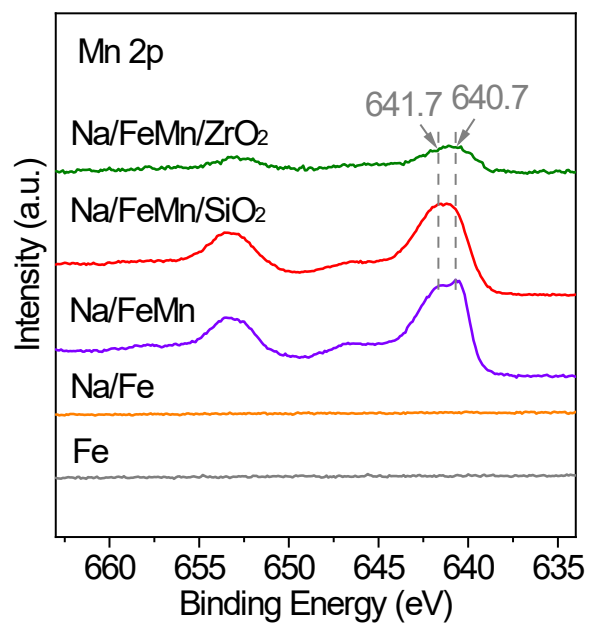


Figure S10. Mn 2p XPS spectra of the spent catalysts.

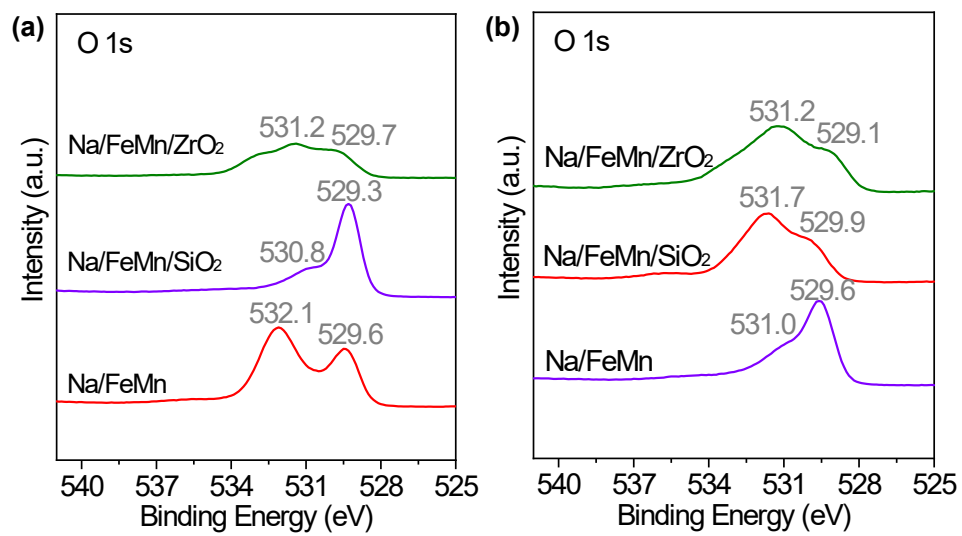


Figure S11. O 1s XPS spectra of fresh (a) and reduced (b) catalysts.

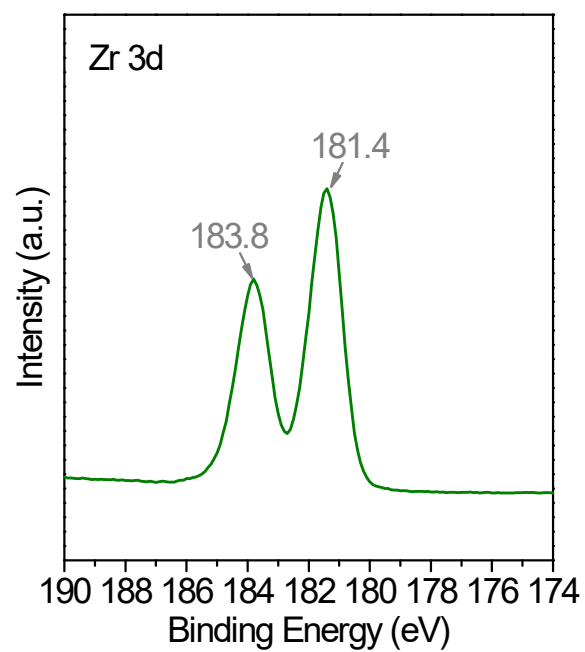


Figure S12. Zr 3d XPS spectra of the spent Na/FeMn/ZrO₂ catalyst.

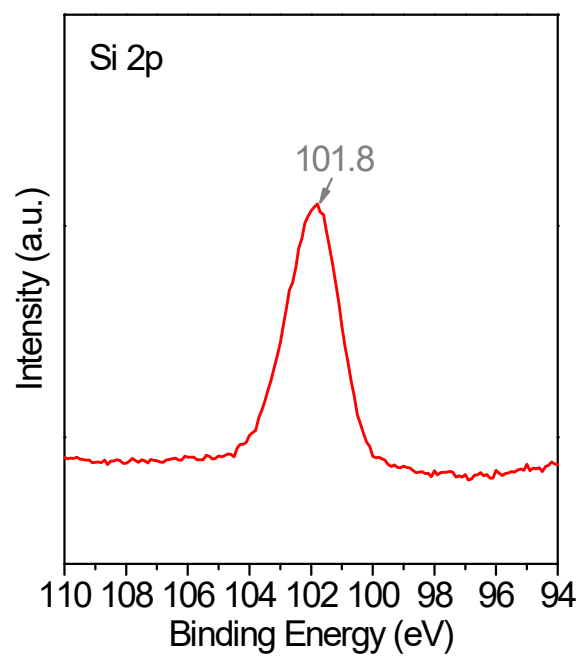


Figure S13. Si 2p XPS spectra of the spent Na/FeMn/SiO₂ catalyst.

Table S3. Surface element content of the spent catalysts obtained by XPS analysis.

Sample	Elements contents (%)					
	Fe	C	O	Na	Mn	Si or Zr
Fe	31.4	21.1	47.5	/	/	/
Na/Fe	21.7	36.5	34.1	7.7	/	/
Na/FeMn	7.1	31.7	39.7	8.4	13.1	/
Na/FeMn/SiO ₂	7.8	26.9	40.7	7.9	11.0	5.7
Na/FeMn/ZrO ₂	8.1	30.8	36.8	8.2	9.8	6.3

^a Calculated in atomic %.

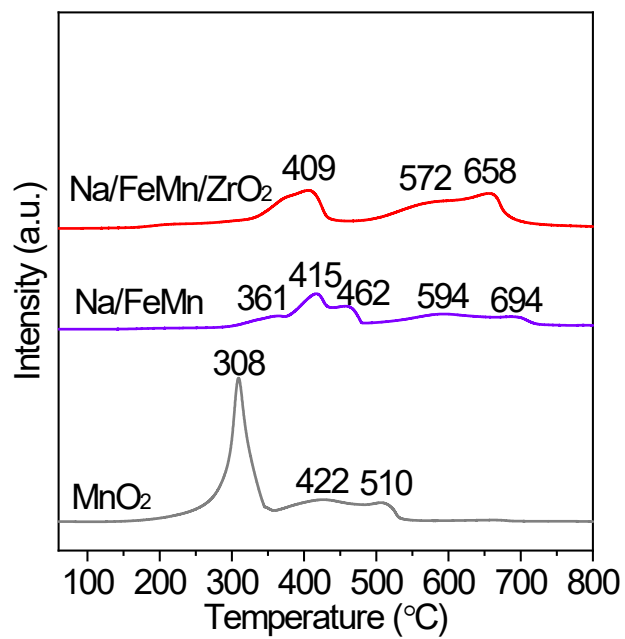


Figure S14. H₂-TPR profiles of the reference MnO₂, Na/FeMn, and Na/FeMn/ZrO₂ catalysts.

Table S4. The H₂ consumption of the prepared catalyst during the H₂ reduction process

Catalysts	T _m (°C) ^a			H ₂ consumption (μmol·g ⁻¹) ^b		
	α	β	γ	α	β	γ
Fe	50-380	380-600	600-800	3400.5	7280.1	0
Na/Fe	50-450	450-590	590-800	1899.2	8977.0	1237.4
Na/FeMn	50-480	480-660	660-800	3744.2	2360.7	1197.2
Na/FeMn/SiO ₂	50-480	480-600	600-800	374.1	653.2	523.4
Na/FeMn/ZrO ₂	50-460	460-610	610-800	514.0	347.2	359.1

^a Temperature range of the reduction peak.

^b The H₂ consumption of these catalysts was obtained by H₂-TPR analysis.

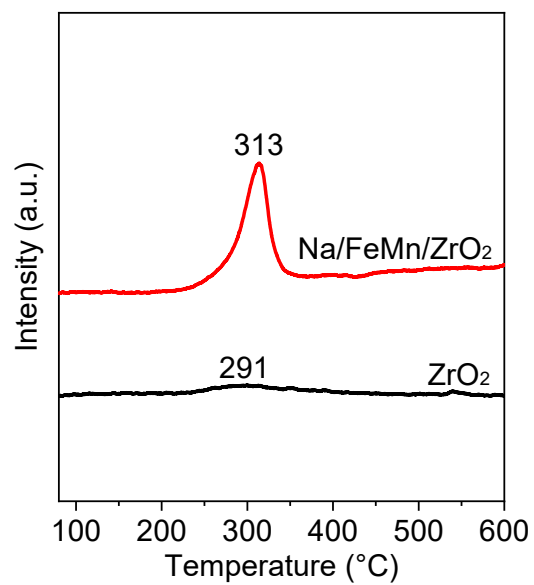


Figure S15. CO-TPD profiles of the reference ZrO₂ and Na/FeMn/ZrO₂ catalysts.

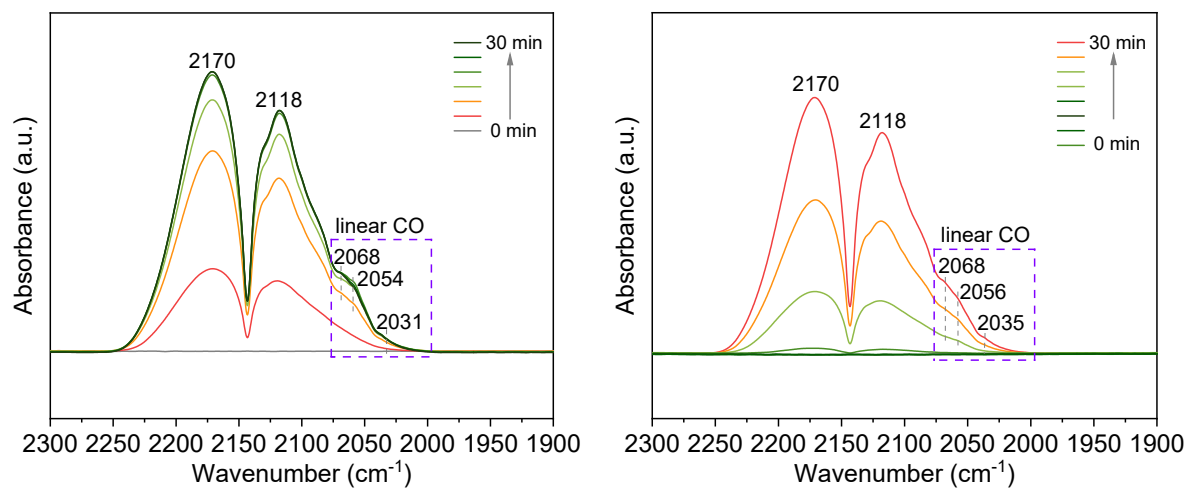


Figure S16. DRIFTS of CO adsorption (a) and CO desorption (b) spectra of Na/FeMn/ZrO₂ catalyst.

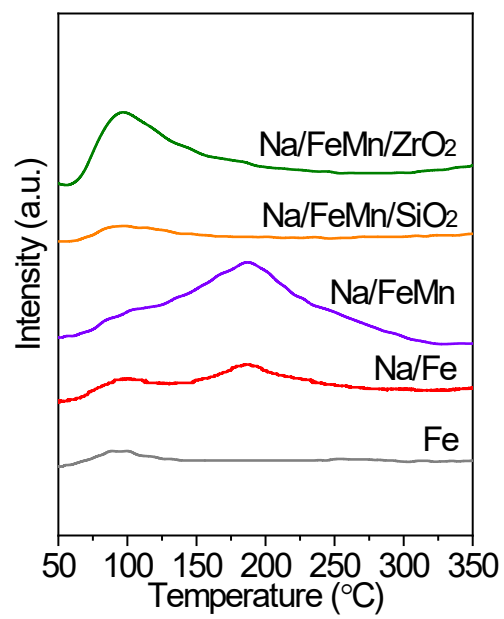


Figure S17. CO₂-TPD profiles of the catalysts.

Table S5. Detailed Mössbauer parameters

Catalyst	Assignment	Mössbauer parameters				
		IS (mm·s ⁻¹)	QS (mm·s ⁻¹)	H (T)	Γ (mm·s ⁻¹)	Area (%)
Na/FeMn/ZrO ₂ - spent	Fe ₃ O ₄ (B)	0.4	-0.05	48.56	0.19	1.3
	Fe ₃ O ₄ (A)	0.79	0.01	49.12	0.23	2.5
	χ-Fe ₅ C ₂ (II)	0.08	0.05	19.88	0.55	31.7
	χ-Fe ₅ C ₂ (I)	0.15	0.16	22.48	0.48	26.2
	χ-Fe ₅ C ₂ (III)	0.07	0.18	11.79	0.32	21.7
	Fe ³⁺	0.24	0.85	—	0.88	16.6

Table S6. Catalytic performance for the hydrogenation CO₂ to long chain linear α -olefins.

Catalysts	CO ₂ conv. (%)	CO sel. (%)	Hydrocarbon distribution (%)					LAOs sel. (%)	LAOs /C ₄₊ (%)	O/P	LAOs yield (%)
			CH ₄	C ₂₋₄ ⁰	C ₂₋₄ ⁼	C ₅₊ ⁰	C ₅₊ ⁼				
Fe	29.3	21.4	38.2	46.6	3.8	11.3	0.2	0.9	4.1	0.1	0.2
Na/Fe	33.6	22.0	13.7	8.9	31.3	29.6	16.5	25.0	42.5	3.5	6.5
Na/FeMn	30.2	31.9	12.7	9.1	35.9	21.4	21.0	31.0	54.8	4.0	6.3
Na/FeMn/SiO ₂	18.3	48.3	51.0	24.7	10.2	14.1	0.1	1.0	4.6	0.4	0.1
Na/FeMn/ZrO ₂	29.4	23.0	18.5	8.9	43.3	11.3	17.9	29.6	68.0	5.1	6.7

Reaction conditions: H₂/CO₂ = 3, 1.5 MPa, 320 °C, WHSV=7500 mL·g_{cat}⁻¹·h⁻¹, TOS = 10 h

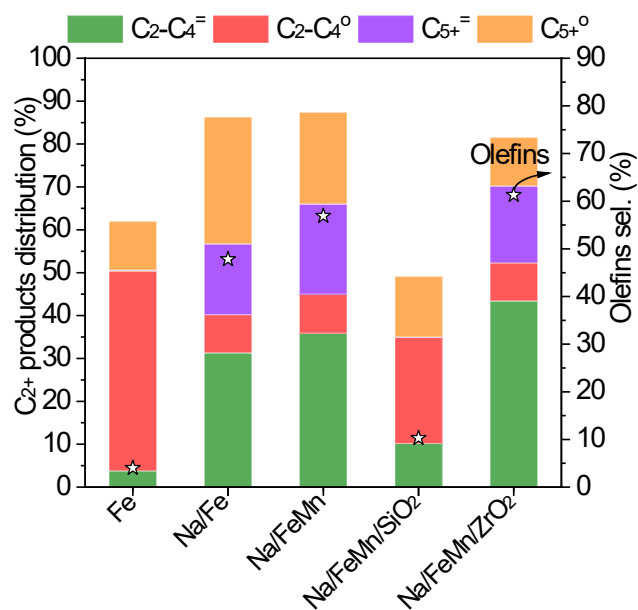


Figure S18. C₂+ products distribution and olefins selectivity. Reaction conditions: H₂/CO₂ = 3, 1.5 MPa, 320 °C, 7500 mL·gcat⁻¹·h⁻¹, TOS = 10 h.

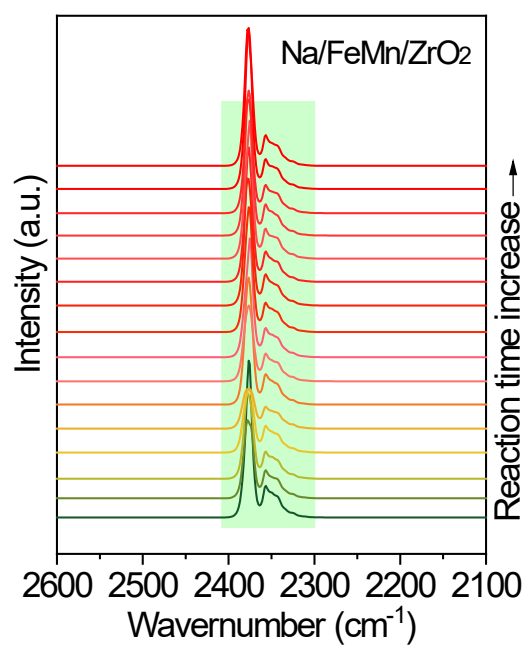


Figure S19. *In situ* DRIFTS of CO₂ hydrogenation to LAOs over the Na/FeMn/ZrO₂ catalyst.

Reduced conditions: 400 °C, H₂, 30 mL·min⁻¹; Reaction conditions: H₂/CO₂ = 3, 320 °C, 30 mL·min⁻¹.

Figure S20. Adsorption model of CH_2+CH_2 over Fe_5C_2 and the $\text{Fe}_5\text{C}_2\text{-ZrO}_2$ interface.

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