

## Supplementary Information

### Highly efficient CO<sub>2</sub> hydrogenation to long-chain linear $\alpha$ -olefins via CO intermediate enrichment over Na/FeMn/ZrO<sub>2</sub> catalysts

Kangzhou Wang<sup>a,\*</sup>, Tong Liu<sup>b</sup>, Pengqi Hai<sup>a</sup>, Shunnosuke Fujii<sup>c</sup>, Chufeng Liu<sup>c</sup>, Hanyao Song<sup>c</sup>, Caixia Zhu<sup>d</sup>, Guangbo Liu<sup>d,e</sup>, Jianli Zhang<sup>b,\*</sup>, Zhou-jun Wang<sup>b,f,\*</sup>, Noritatsu Tsubaki<sup>c,\*</sup>

<sup>a</sup> School of Materials and New Energy, Ningxia University, Yinchuan 750021, Ningxia, China.

<sup>b</sup> State Key Laboratory of High-efficiency Utilization of Coal and Green Chemical Engineering, College of Chemistry & Chemical Engineering, Ningxia University, Yinchuan 750021, Ningxia, China.

<sup>c</sup> Department of Applied Chemistry, School of Engineering, University of Toyama, Gofuku 3190, Toyama 930-8555, Japan.

<sup>d</sup> Qingdao Institute of Bioenergy and Bioprocess Technology, Chinese Academy of Sciences, Qingdao 266101, China.

<sup>e</sup> College of Chemical Engineering, Qingdao University of Science and Technology, 53 Zhengzhou Road, Qingdao 266042, China.

<sup>f</sup> State Key Laboratory of Chemical Resource Engineering, Beijing Key Laboratory of Energy Environmental Catalysis, Beijing University of Chemical Technology, Beijing, 100029, China.

\*Corresponding author: kangzhou\_wang@nxu.edu.cn (K. Wang); zhangjl@nxu.edu.cn (J. Zhang); wangzj@mail.buct.edu.cn (Z.-j. Wang); tsubaki@eng.u-toyama.ac.jp (N. Tsubaki)

## 1. Catalyst preparation

The Na/FeMn/ZrO<sub>2</sub> catalyst was prepared via a pre-coordination anchoring strategy. Typically, 2.02 g Fe(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O (AR, Sinopharm Chemical Reagent Co., Ltd), 1.26 g Mn(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O (AR, Sinopharm Chemical Reagent Co., Ltd), and 11.69 g ethylene diamine tetraacetic acid (AR, Sigma Aldrich) was dissolved into 37.28 g of deionized water under stirring to form a solution, to which 6.52 g of ZrO<sub>2</sub> (AR, Sinopharm Chemical Reagent Co., Ltd) was added with continuous stirring for 5 h. Subsequently, the mixture was heated to 120 °C for evaporation and drying under stirring, and then calcined at 650 °C for 6 h to obtain the FeMn/ZrO<sub>2</sub> sample. The Na/FeMn/ZrO<sub>2</sub> catalyst was fabricated by an impregnation method. In brief, 0.05 g Na<sub>2</sub>CO<sub>3</sub> (AR, Sinopharm Chemical Reagent Co., Ltd) was dissolved into 2.0 g of deionized water. The resultant solution was added dropwise to 1.0 g of FeMn/ZrO<sub>2</sub> sample under ultrasonic condition. After drying in vacuum at 60 °C for 12 h, the Na/FeMn/ZrO<sub>2</sub> catalyst was obtained. Unless specified otherwise, Na and FeMn loading were fixed at 2 wt% and 30 wt%, respectively. The ZrO<sub>2</sub> used in the aforementioned catalysts is monoclinic ZrO<sub>2</sub>.

The reference of Na/FeMn/SiO<sub>2</sub> catalysts were prepared using pre-coordination anchoring strategy. The pre-coordination anchoring strategy primarily involved the formation of metal complexes through ligand-metal ion coordination. The carboxyl groups on the complex surface esterify with hydroxyl groups on the support surface, anchoring the metal ions to the support. Subsequently, reduction and carbonization treatments were applied to form the interfacial structure. In brief, a certain amount of Fe(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O (AR, Sinopharm Chemical Reagent Co., Ltd), Mn(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O (AR, Sinopharm Chemical Reagent Co., Ltd), ethylene diamine tetraacetic acid (AR, Sigma Aldrich) were dissolved into deionized water under stirring. Then,

$\text{SiO}_2$  (AR, Sigma Aldrich) was added to the above solution with continuous stirring for 5 h. Subsequently, the solution was heated to 120  $^{\circ}\text{C}$  for evaporation and drying, and then calcined at 650  $^{\circ}\text{C}$  for 6 h to obtain the  $\text{FeMn}/\text{SiO}_2$  sample.  $\text{Na}/\text{FeMn}/\text{ZrO}_2$  catalyst was prepared by impregnating method. Typically,  $\text{Na}_2\text{CO}_3$  (AR, Sinopharm Chemical Reagent Co., Ltd) was dissolved into deionized water, and then the above solution was added dropwise to  $\text{FeMn}/\text{SiO}_2$  sample under ultrasonic condition, followed by drying in vacuum at 60  $^{\circ}\text{C}$  for 12 h to obtain  $\text{Na}/\text{FeMn}/\text{SiO}_2$  catalyst. The weight percent of Na and  $\text{FeMn}$  are fixed at 2 wt% and 30 wt%, respectively.

The reference  $\text{Na}/\text{FeMn}$  catalyst were prepared by sol-gel method. Typically, a certain amount of  $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ ,  $\text{Mn}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ , and ethylene diamine tetraacetic acid were dissolved into deionized water to form uniform solution under stirring. After that, evaporation dried at 120  $^{\circ}\text{C}$  under stirring, and then calcined at 650  $^{\circ}\text{C}$  for 5 h to obtain  $\text{FeMn}$  samples.  $\text{Na}/\text{FeMn}$  catalyst was prepared by impregnating method.  $\text{Na}_2\text{CO}_3$  was dissolved into deionized water, and then was dropped in the  $\text{FeMn}$  sample, dried at 60  $^{\circ}\text{C}$  in vacuum for overnight. The final catalyst was denoted as  $\text{Na}/\text{FeMn}$ . The Fe and  $\text{Na}/\text{Fe}$  were prepared by the above-mentioned process.

## 2. Catalyst characterization

X-ray diffraction (XRD) spectra were performed on a Rigaku RINT 2400 X-ray diffract meter equipped using  $\text{Cu K}\alpha$  radiation at 40 kV and 20 mA with a scanning speed of  $2^{\circ}\cdot\text{min}^{-1}$  and step width of  $0.02^{\circ}$ . *In situ* XRD analysis was conducted on a Rigaku SmartLab equipped with  $\text{Cu K}\alpha$  radiation. Samples were reduced in flowing  $\text{H}_2$  ( $30\text{ mL}\cdot\text{min}^{-1}$ ) with programmed heating from room temperature to 600  $^{\circ}\text{C}$ . To monitor catalyst phase evolution during the

reaction process, the catalyst was first reduced at 400 °C for 1 h. After pretreatment, the sample was cooled down to 100 °C, followed by reaction gas introduction and data recording.

Scanning electron microscopy (SEM) images were taken on a JEOL JSM-6360LV microscope operated at an accelerating voltage of 1.5 kV. Transmission electron microscopy (TEM) and elemental mapping images were obtained on a JEOL JEM-2100F at an acceleration voltage of 200 kV.

$\text{N}_2$  sorption was conducted on a Micromeritics NOVA2200e analyzer. Prior to the measurement, the sample was degassed in vacuum at 200 °C for 5 h. The surface area was calculated by the Brunauer-Emmett-Teller (BET) method. The average pore size and pore volume were determined by the Barrett-Joyner-Halenda (BJH) method.

Hydrogen temperature-programmed reduction ( $\text{H}_2$ -TPR) measurements were performed on a BELCAT-II-T-SP with a thermal conductivity detector (TCD). Specifically, 50 mg catalyst was loaded into a U-shaped quartz tube reactor and pretreated at 150 °C for 2 h in flowing He. After that, the sample was cooled down to 100 °C, followed by reduction in flowing  $\text{H}_2$  (30  $\text{mL}\cdot\text{min}^{-1}$ ) at 10 °C·min<sup>-1</sup> up to 600 °C.

Temperature-programmed desorption (TPD) was performed on a BELCAT-II-T-SP instrument with a TCD. Specifically, 50 mg sample was loaded into a quartz tube reactor and reduced at 400 °C for 2 h in flowing  $\text{H}_2$  (30  $\text{mL}\cdot\text{min}^{-1}$ ). After that, the sample was cooled down to 50 °C and saturated with  $\text{CO}_2$  or CO. The sample was flushed in flowing He for 0.5 h to remove the gaseous  $\text{CO}_2$  or CO. Then, TPD was carried out in flowing He (30  $\text{mL}\cdot\text{min}^{-1}$ ) from 60 to 300 °C at 10 °C·min<sup>-1</sup>.

X-ray photoelectron spectroscopy (XPS) analysis was performed on a Thermo Fisher

Scientific ESCALAB 250Xi instrument using an Al Ka X-ray radiation source. The binding energy was calibrated by C 1s of adventitious carbon (284.6 eV).

The  $^{57}\text{Fe}$  Mössbauer spectra (MES) were carried out on a wissel spectrometer driving with a proportional counter at room temperature. The radioactive source was  $^{57}\text{Co}(\text{Pd})$  moving in a constant acceleration mode. The components of iron phases were identified based on their Mössbauer parameters including isomer shift, quadruple splitting and magnetic hyperfine field.

$\text{H}_2$ -temperature programmed surface reaction ( $\text{H}_2$ -TPSR) experiments were performed on a Micromeritics AutoChem II 2920 instrument. Specifically, the spent catalyst was purged with Ar at 320 °C for 1 h, followed by *in situ* reduction with  $\text{H}_2$  for 1 h. After cooling to 50 °C, the catalyst was exposed to a 5%CO/Ar mixture gas for 30 min. The sample was then purged with Ar at 50 °C for 30 min. Subsequently,  $\text{H}_2$  was introduced into the reactor with a programmed temperature ramp from 50 °C to 800 °C. Mass spectrometry (MS) signals for CO (m/z = 28) and  $\text{H}_2$  (m/z = 2) were recorded.

*In situ* diffuse reflectance infrared fourier transform spectroscopy (DRIFTS) was performed on a Nicolet Nexus 470 FTIR spectrometer equipped with a diffuse reflectance attachment and a mercury cadmium telluride (MCT) detector. Prior to the test, 20 mg sample was placed in a diffuse reflectance infrared cell with a ZnSe window. The sample was reduced at 400 °C for 1 h with a pure  $\text{H}_2$  flow of 30 mL/min, and then cooled down to 320 °C and the background spectrum was recorded. After the feedstock was introduced into the cell with flow of 30 mL/min, and the spectra were recorded by collecting 32 scans at  $4 \text{ cm}^{-1}$  resolution.

CO-DRIFTS was performed on a Nicolet 6700 spectrometer equipped with a diffuse reflectance cell and a liquid nitrogen-cooled high sensitivity MCT detector to detect the

adsorption and desorption of CO on the catalyst surface. The samples were first loaded into a reaction chamber and reduced by 10 % H<sub>2</sub>/Ar at a flow rate of 30 mL·min<sup>-1</sup> at 400 °C. Subsequently, 10 % CO/Ar was introduced into the reaction chamber and spectral data were collected.

### 3. DFT calculations

All calculations employed spin-polarized density functional theory (DFT) using the VASP software [1,2]. The exchange–correlation functional was treated within the generalized gradient approximation (GGA) using the Perdew-Burke-Ernzerhof (PBE) functional [3]. A plane-wave cutoff energy of 450 eV was applied. Valence electrons were described using the projector-augmented wave (PAW) method [4]. A Hubbard *U* correction of 5.0 eV was applied to the Ce 4f orbitals to accurately describe electron localization [5]. Ionic relaxation was performed until the maximum force on atom was below 0.05 eV/Å. van-der-Waals interactions were accounted for using the DFT-D3 method [6]. The bottom two atomic layers were fixed in position, while all other atoms were allowed to relax. Transition states were located using the climbing image nudge elastic band (CI-NEB) method. The results in Figure 7c and Figure 7d were obtained using this method.

### 4. Catalytic evaluation

CO<sub>2</sub> hydrogenation reactions were performed in a stainless steel fixed-bed reactor. In brief, 0.4 g catalyst was evenly mixed with 0.5 g quartz sand, which was then loaded in a reactor with internal diameter of 6 mm. Prior to reaction, the catalyst was *in situ* reduced at 400 °C for 8 h in flowing H<sub>2</sub> (60 mL·min<sup>-1</sup>) at atmospheric pressure. After reduction, the catalyst was cooled down to 320 °C, and then the reactant gas mixture (gas composition as 25.03 % CO<sub>2</sub>, 70.0 %

$\text{H}_2$ , Ar balance) was fed into the reactor. The reaction was carried out at 320 °C, 1.5 MPa, and 7500  $\text{mL}\cdot\text{g}_{\text{cat}}^{-1}\cdot\text{h}^{-1}$ . Reaction effluents were quantitatively analyzed using online gas chromatograph (GC-2014C, Shimadzu) equipped with TCD and active charcoal column (TDX-01) for Ar, CO,  $\text{CH}_4$ , and  $\text{CO}_2$  analysis together with flame ionization detector (FID) and Rtx-1 capillary column (60 m  $\times$  0.32 mm  $\times$  5  $\mu\text{m}$ ) for hydrocarbon analysis. The hydrocarbon distribution was calculated from total carbon moles.

$\text{CO}_2$  conversion and CO selectivity were calculated as follows:

$$\text{CO}_2 \text{ conversion} = \frac{\text{CO}_2 \text{ inlet} - \text{CO}_2 \text{ outlet}}{\text{CO}_2 \text{ inlet}} \times 100\% \quad (1)$$

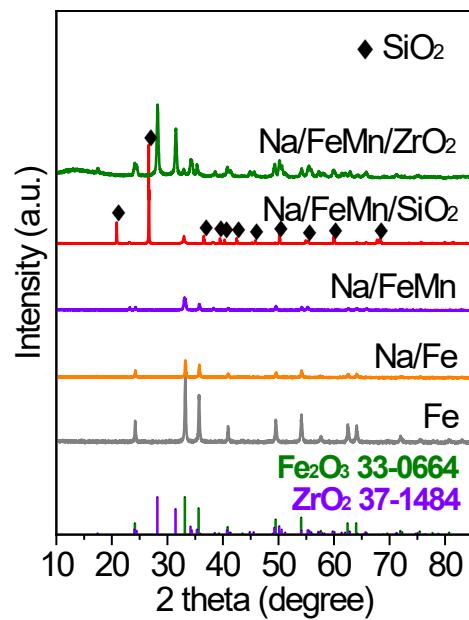
$$\text{CO selectivity} = \frac{\text{CO outlet}}{\text{CO}_2 \text{ inlet} - \text{CO}_2 \text{ outlet}} \times 100\% \quad (2)$$

where,  $\text{CO}_2$  inlet,  $\text{CO}_2$  outlet, and CO outlet represent the moles of  $\text{CO}_2$  at the inlet and outlet, and the moles of CO at the outlet, respectively.

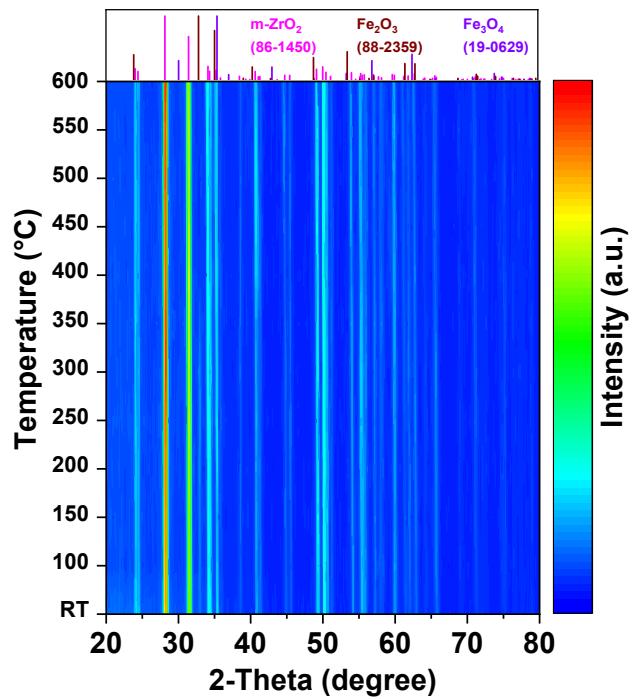
The selectivity of hydrocarbon in total hydrocarbons was calculated as follows:

$$\text{C}_i \text{ hydrocarbon selectivity} = \frac{\frac{\text{mole of } \text{C}_i \text{ hydrocarbon} \times i}{\sum_{i=1}^n \text{mole of } \text{C}_i \text{ hydrocarbon} \times i}}{\sum_{i=1}^n \text{mole of } \text{C}_i \text{ hydrocarbon} \times i} \times 100\% \quad (3)$$

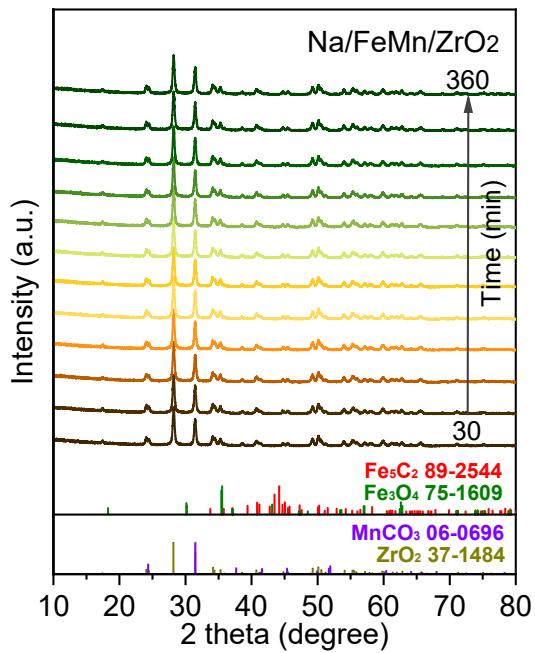
## 5. Results and discussion



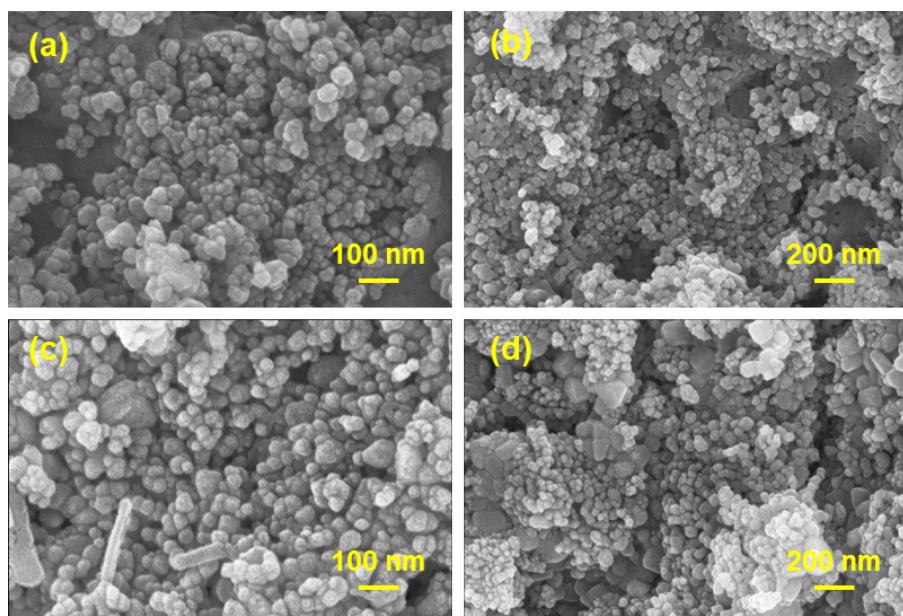
**Figure S1.** XRD patterns of the fresh catalysts



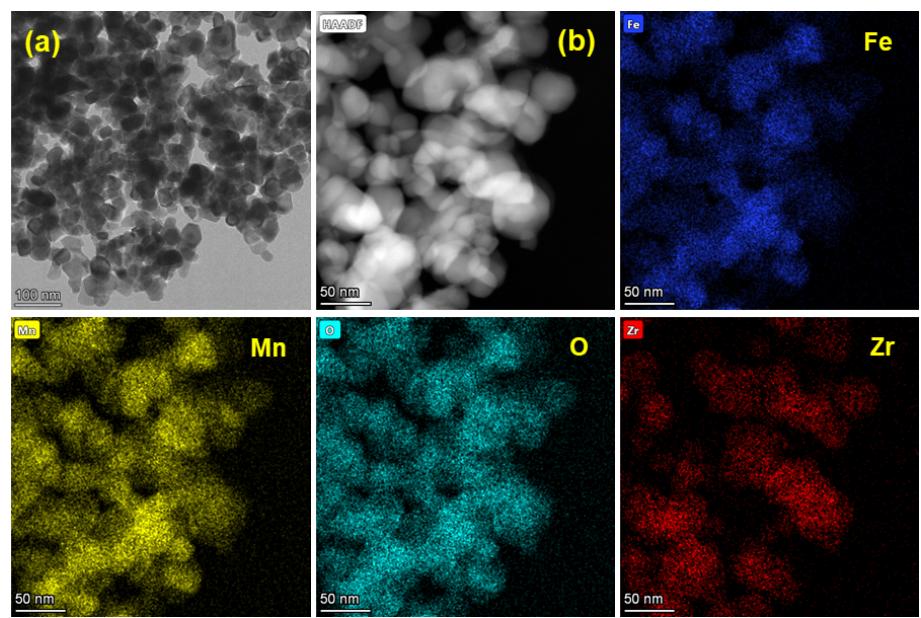
**Figure S2.** *In situ* XRD patterns of the Na/FeMn/ZrO<sub>2</sub> catalyst for H<sub>2</sub> reduction process.



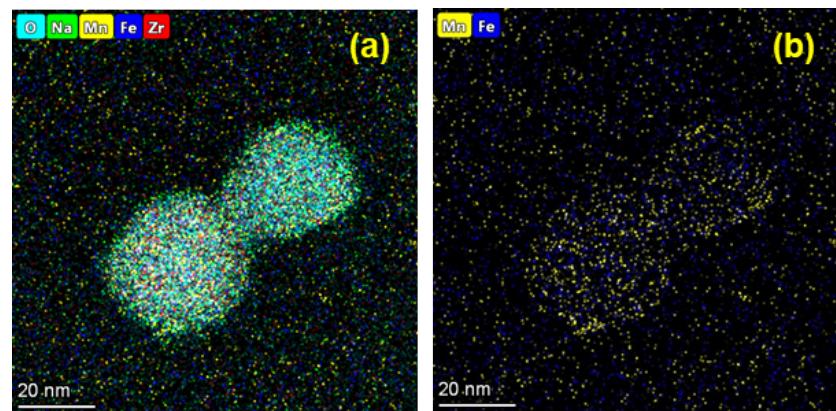
**Figure S3.** *In situ* XRD patterns of Na/FeMn/ZrO<sub>2</sub> for CO<sub>2</sub> hydrogenation.



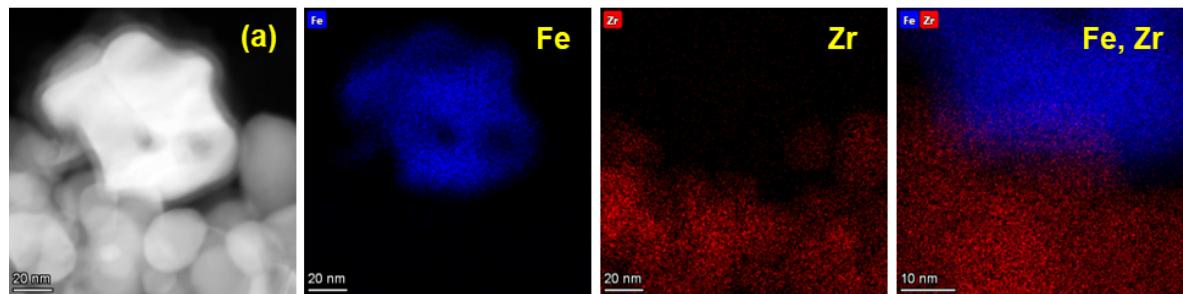
**Figure S4.** SEM images of the fresh Na/FeMn/ZrO<sub>2</sub> (a,b) and spent Na/FeMn/ZrO<sub>2</sub> (c,d) catalyst.



**Figure S5.** TEM image (a), STEM image (b) and EDS elemental mapping images of the fresh Na/FeMn/ZrO<sub>2</sub> catalyst.



**Figure S6.** The EDS mapping images of (a) all elemental, (b) Fe and Mn in the spent Na/FeMn/ZrO<sub>2</sub> catalyst



**Figure S7.** STEM image of spent Na/FeMn/ZrO<sub>2</sub> catalyst (a), EDS mapping images of all elemental (b), and the corresponding EDS elemental mapping images.

**Table S1.** The elemental composition of the as-prepared catalysts.

Catalysts	Element content (wt%) <sup>a</sup>				Dosage of raw materials (wt%) <sup>b</sup>			
	Na	Fe	Mn	Si or Zr	Na	Fe	Mn	Si or Zr
Na/FeMn	1.7	21.6	20.9	/	2.0	22.8	19.6	/
Na/FeMn/SiO <sub>2</sub>	1.7	4.7	3.5	37.4	2.0	3.6	3.1	39.1
Na/ FeMn/ZrO <sub>2</sub>	1.9	3.8	4.0	61.5	2.0	3.6	3.1	62.3

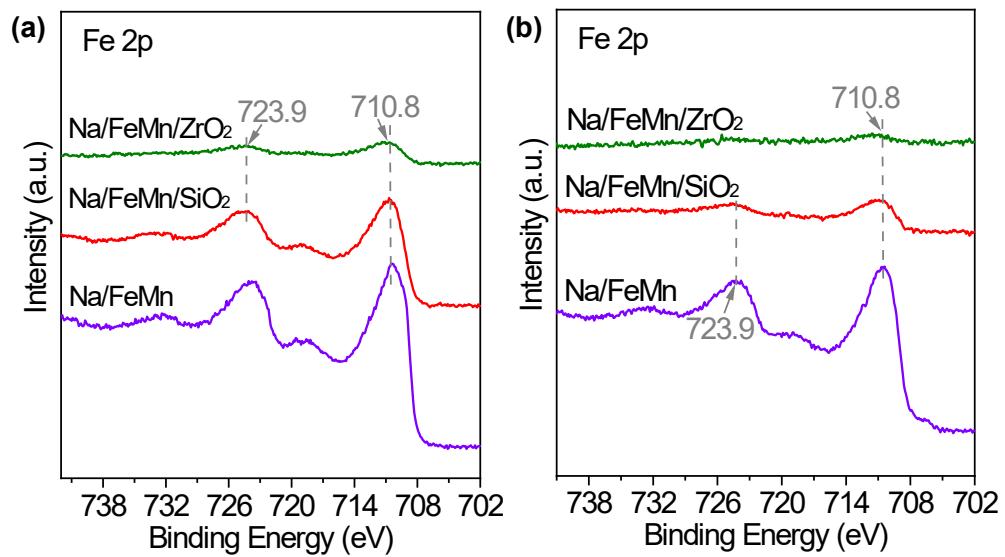
<sup>a</sup>The elemental composition of these catalysts was obtained by ICP analysis.

<sup>b</sup>The dosages of the elements were calculated according to the amounts of raw materials in the catalyst preparation.

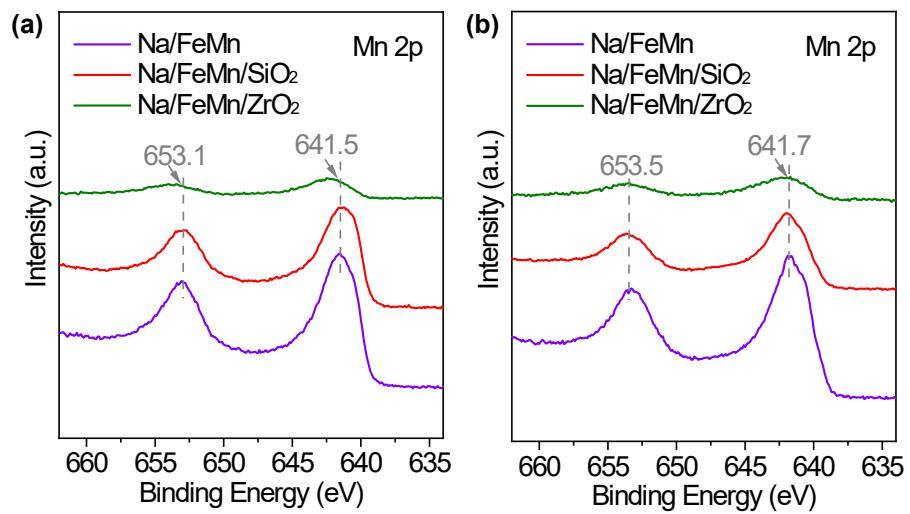
**Table S2.** Textural properties of the prepared catalysts.

Catalysts	BET surface area <sup>a</sup> (m <sup>2</sup> ·g <sup>-1</sup> )	Pore volume <sup>b</sup> (cm <sup>3</sup> ·g <sup>-1</sup> )	Average pore size <sup>c</sup> (nm)
Fe	23.7	0.14	11.5
Na/Fe	25.0	0.20	13.8
Na/FeMn	17.2	0.14	12.3
Na/FeMn/SiO <sub>2</sub>	14.7	0.04	1.7
Na/FeMn/ZrO <sub>2</sub>	31.5	0.26	8.7

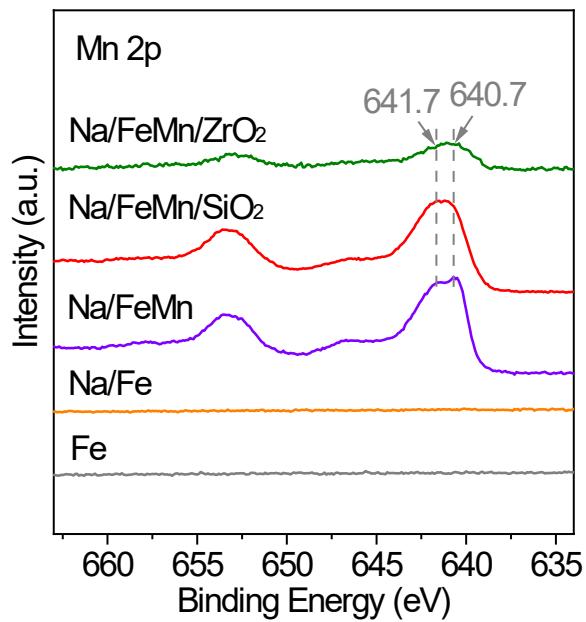
<sup>a</sup>BET specific surface area; <sup>b</sup>pore volume calculated by BJH method; <sup>c</sup>average diameter of mesopores evaluated by the BJH method.



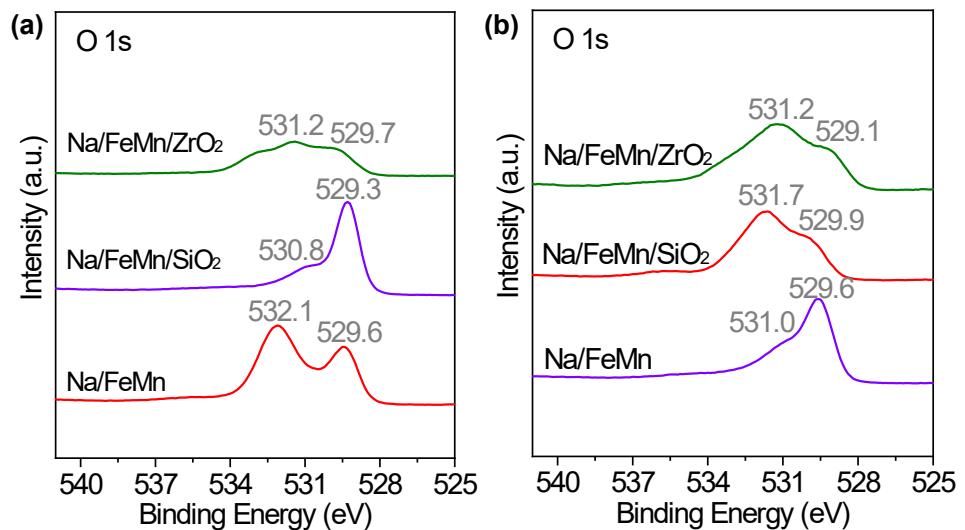
**Figure S8.** Fe 2p XPS spectra of fresh (a) and reduced (b) catalysts.



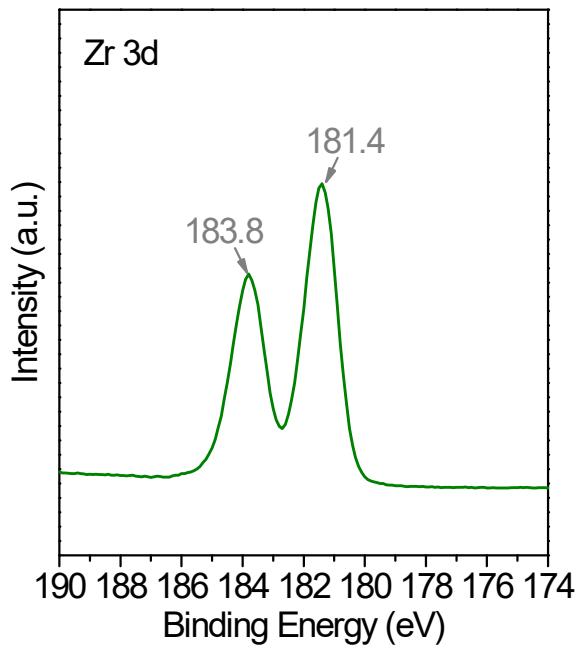
**Figure S9.** Mn 2p XPS spectra of fresh (a) and reduced (b) catalysts.



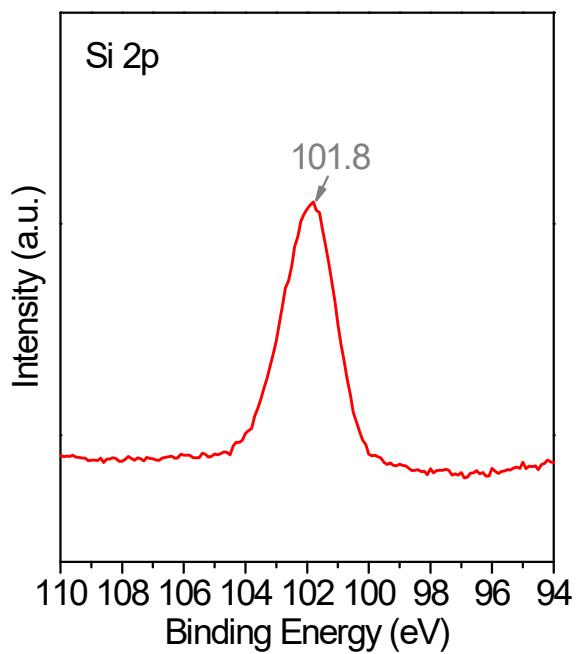
**Figure S10.** Mn 2p XPS spectra of the spent catalysts.



**Figure S11.** O 1s XPS spectra of fresh (a) and reduced (b) catalysts.



**Figure S12.** Zr 3d XPS spectra of the spent Na/FeMn/ZrO<sub>2</sub> catalyst.

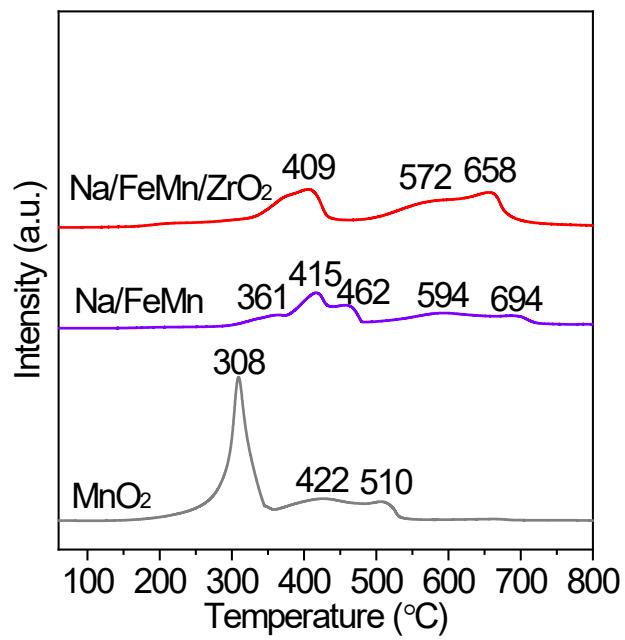


**Figure S13.** Si 2p XPS spectra of the spent Na/FeMn/SiO<sub>2</sub> catalyst.

**Table S3.** Surface element content of the spent catalysts obtained by XPS analysis.

Sample	Elements contents (%)					
	Fe	C	O	Na	Mn	Si or Zr
Fe	31.4	21.1	47.5	/	/	/
Na/Fe	21.7	36.5	34.1	7.7	/	/
Na/FeMn	7.1	31.7	39.7	8.4	13.1	/
Na/FeMn/SiO <sub>2</sub>	7.8	26.9	40.7	7.9	11.0	5.7
Na/FeMn/ZrO <sub>2</sub>	8.1	30.8	36.8	8.2	9.8	6.3

<sup>a</sup> Calculated in atomic %.



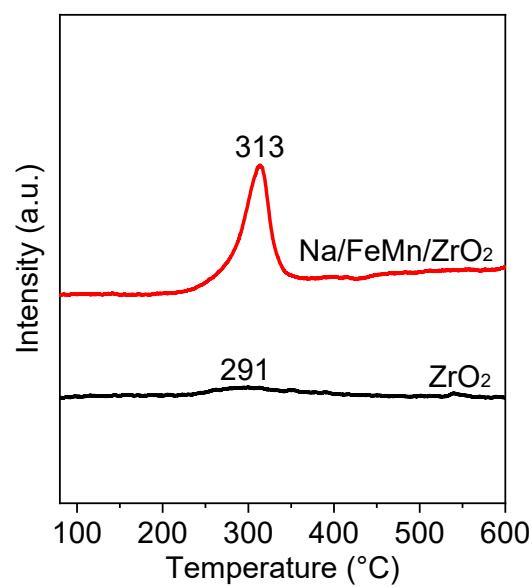
**Figure S14.**  $\text{H}_2$ -TPR profiles of the reference  $\text{MnO}_2$ ,  $\text{Na/FeMn}$ , and  $\text{Na/FeMn/ZrO}_2$  catalysts.

**Table S4.** The H<sub>2</sub> consumption of the prepared catalyst during the H<sub>2</sub> reduction process

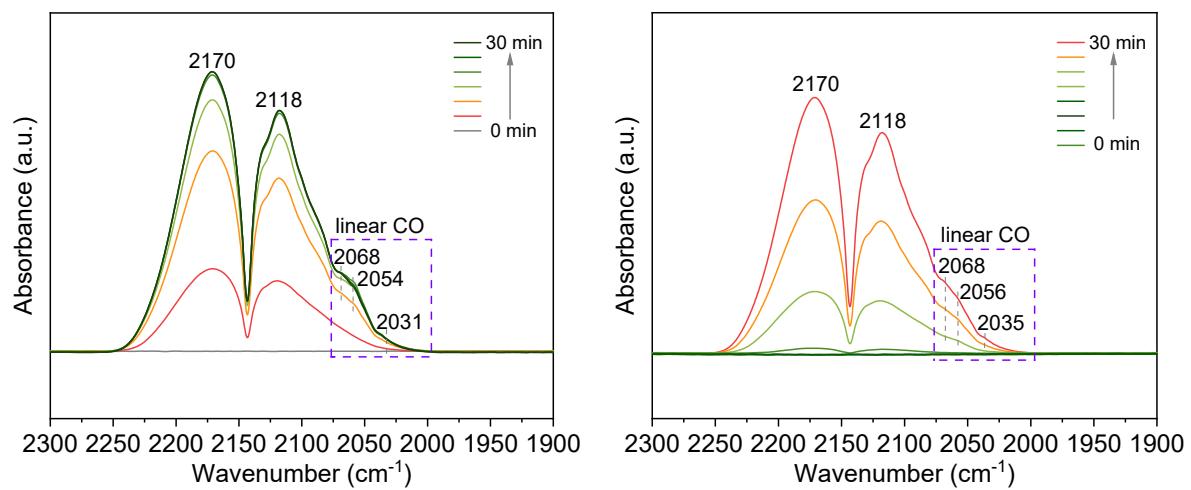
Catalysts	T <sub>m</sub> (°C) <sup>a</sup>			H <sub>2</sub> consumption (μmol·g <sup>-1</sup> ) <sup>b</sup>		
	α	β	γ	α	β	γ
Fe	50-380	380-600	600-800	3400.5	7280.1	0
Na/Fe	50-450	450-590	590-800	1899.2	8977.0	1237.4
Na/FeMn	50-480	480-660	660-800	3744.2	2360.7	1197.2
Na/FeMn/SiO <sub>2</sub>	50-480	480-600	600-800	374.1	653.2	523.4
Na/FeMn/ZrO <sub>2</sub>	50-460	460-610	610-800	514.0	347.2	359.1

<sup>a</sup> Temperature range of the reduction peak.

<sup>b</sup> The H<sub>2</sub> consumption of these catalysts was obtained by H<sub>2</sub>-TPR analysis.

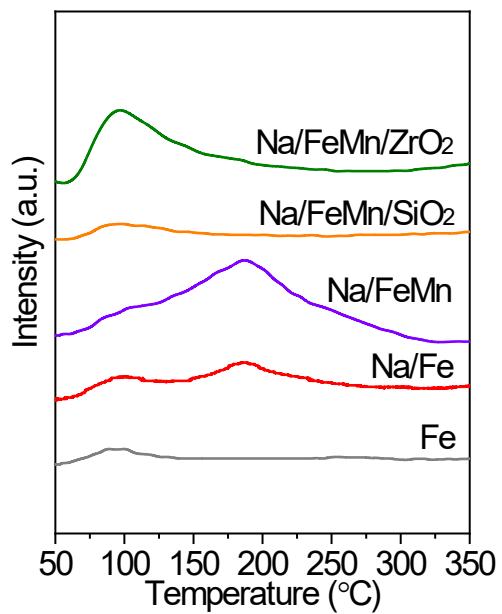


**Figure S15.** CO-TPD profiles of the reference ZrO<sub>2</sub> and Na/FeMn/ZrO<sub>2</sub> catalysts.



**Figure S16.** DRIFTS of CO adsorption (a) and CO desorption (b) spectra of Na/FeMn/ZrO<sub>2</sub>

catalyst.



**Figure S17.** CO<sub>2</sub>-TPD profiles of the catalysts.

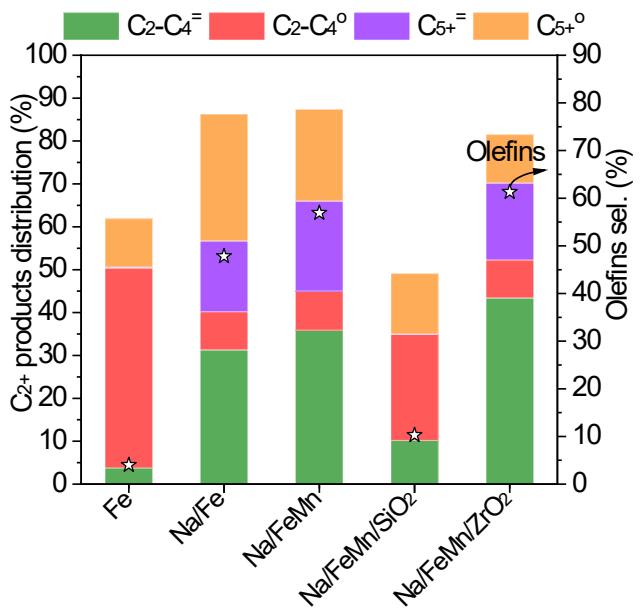
**Table S5.** Detailed Mössbauer parameters

Catalyst	Assignment	Mössbauer parameters				
		IS (mm·s <sup>-1</sup> )	QS (mm·s <sup>-1</sup> )	H (T)	Γ (mm·s <sup>-1</sup> )	Area (%)
Na/FeMn/ZrO <sub>2</sub> -spent	Fe <sub>3</sub> O <sub>4</sub> (B)	0.4	-0.05	48.56	0.19	1.3
	Fe <sub>3</sub> O <sub>4</sub> (A)	0.79	0.01	49.12	0.23	2.5
	χ-Fe <sub>5</sub> C <sub>2</sub> (II)	0.08	0.05	19.88	0.55	31.7
	χ-Fe <sub>5</sub> C <sub>2</sub> (I)	0.15	0.16	22.48	0.48	26.2
	χ-Fe <sub>5</sub> C <sub>2</sub> (III)	0.07	0.18	11.79	0.32	21.7
	Fe <sup>3+</sup>	0.24	0.85	—	0.88	16.6

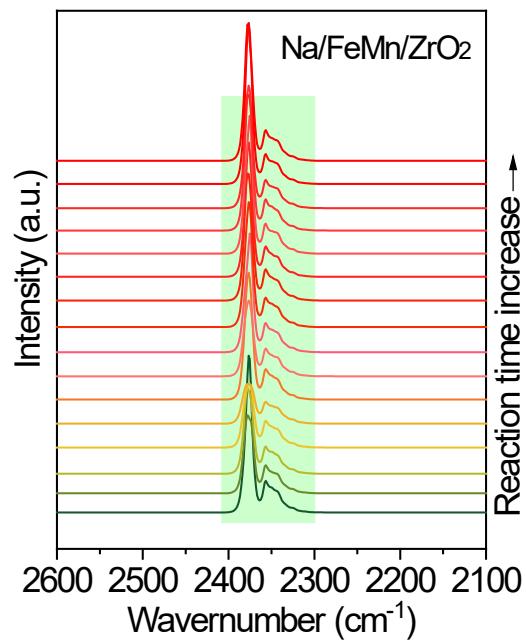
**Table S6.** Catalytic performance for the hydrogenation CO<sub>2</sub> to long chain linear  $\alpha$ -olefins.

Catalysts	CO <sub>2</sub>	CO	Hydrocarbon distribution (%)					LAOs sel. (%)	LAOs /C <sub>4+</sub> (%)	O/P	LAOs yield (%)
	conv. (%)	sel. (%)	CH <sub>4</sub>	C <sub>2-4</sub> <sup>0</sup>	C <sub>2-4</sub> <sup>=</sup>	C <sub>5+</sub> <sup>0</sup>	C <sub>5+</sub> <sup>=</sup>				
Fe	29.3	21.4	38.2	46.6	3.8	11.3	0.2	0.9	4.1	0.1	0.2
Na/Fe	33.6	22.0	13.7	8.9	31.3	29.6	16.5	25.0	42.5	3.5	6.5
Na/FeMn	30.2	31.9	12.7	9.1	35.9	21.4	21.0	31.0	54.8	4.0	6.3
Na/FeMn/SiO <sub>2</sub>	18.3	48.3	51.0	24.7	10.2	14.1	0.1	1.0	4.6	0.4	0.1
Na/FeMn/ZrO <sub>2</sub>	29.4	23.0	18.5	8.9	43.3	11.3	17.9	29.6	68.0	5.1	6.7

Reaction conditions: H<sub>2</sub>/CO<sub>2</sub> = 3, 1.5 MPa, 320 °C, WHSV=7500 mL·g<sub>cat</sub><sup>-1</sup>·h<sup>-1</sup>, TOS = 10 h



**Figure S18.**  $C_{2+}$  products distribution and olefins selectivity. Reaction conditions:  $H_2/CO_2 = 3$ , 1.5 MPa, 320 °C, 7500 mL·gcat<sup>-1</sup>·h<sup>-1</sup>, TOS = 10 h.



**Figure S19.** *In situ* DRIFTS of CO<sub>2</sub> hydrogenation to LAOs over the Na/FeMn/ZrO<sub>2</sub> catalyst.

Reduced conditions: 400 °C, H<sub>2</sub>, 30 mL·min<sup>-1</sup>; Reaction conditions: H<sub>2</sub>/CO<sub>2</sub> = 3, 320 °C, 30 mL·min<sup>-1</sup>.

**Figure S20.** Adsorption model of  $\text{CH}_2+\text{CH}_2$  over  $\text{Fe}_5\text{C}_2$  and the  $\text{Fe}_5\text{C}_2\text{-ZrO}_2$  interface.

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