Supporting Information

Design and investigation of a magnetic coupling piezoelectric inertial energy harvesting system for

low-power wireless sensors in intercity bus

Zhen Zhao a&, Xiaohui Zhang a&, Baifu Zhang b*, Haichuan Cui c, Xinjun Li a, Enyu He a

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A00A*-9 A0A*-9 AA*-9 Magnetic force (N) Magnetic force (N) Magnetic force (N) 400 600 Time (s) 200 400 600 1000 200 400 600 800 1000 200 Time (s) Time (s) A00A*-12 A0A*-12 AA*-12 Magnetic force (N) Magnetic force (N) Magnetic force (N) 400 400 1000 600 800 200 0 200 400 600 800 1000 200 600 0 1000 800 Time (s) Time (s) Time (s) A00A*-15 A0A*-15 AA*-15 Magnetic force (N) Magnetic force (N) Magnetic force (N) 200 200 600 400 800 1000 200 400 600 1000 0 400 800 1000 0 600 0 800 Time (s) Time (s) Time (s) A00A*-18 A0A*-18 AA*-18 Magnetic force (N) Magnetic force (N) Magnetic force (N) -3 -3 200 1000 1000 600 1000 800 200 600 0 400 800 200 400 600 0 400 800 Time (s) Time (s) Time (s)

Figures

Fig. S1 Magnetic force curve under condition three



Fig. S2 The voltage variation curves with condition 3



Fig. S3 The voltage variation curves with condition 4

Note. S1

Kinetic energy input model

External torque is primarily utilized in three components:

$$J \cdot \hat{\theta}(t) = \mathbf{m} \cdot l_0 \cdot \hat{\mathbf{x}}(t) \cdot \cos(\theta_0(t)) = T_1 + T_2 + T_3$$
(1)

Among these components, T_1 represents the equivalent torque of each system component, T_2 denotes the gear meshing damping torque, and T_3 refers to the magnetic torque resulting from the interaction between magnet A and magnet B.

$$T_1 = [J_0 + 3 \times n_0^2 \times (J_1 + J_2 + J_3 + J_4 + n_1^2 \times (J_5 + J_6)) + n_0^2 n_1^2 n_2^2 \times (J_7 + J_e)] \times \ddot{\theta}_0(t)$$
(2)

Among these parameters, J_0 represents the rotational inertia of the mass ball and the ring gear, while J_1 , J_2 , J_3 , J_4 , J_5 , J_6 , and J_7 correspond to the moments of inertia of gears 1 through 7. Additionally, J_e indicates the moment of inertia of the rotor.

$$J_{\rm s} = J_0 + 3 \times n_0^2 \cdot (J_1 + J_2 + J_3 + J_4 + n_1^2 \cdot (J_5 + J_6)) + n_0^2 n_1^2 n_2^2 \cdot (J_7 + J_e)$$
(3)

The gear meshing damping torque of the system is defined as:

$$T_2 = 3 \times (C_{\rm mr} + C_{\rm m1} + 2 \times C_{\rm m3} + C_{\rm m6}) \cdot \theta_0(t) \tag{4}$$

Among these parameters, $C_{\rm mr}$ represents the meshing damping coefficient between the ring gear and gear 1, $C_{\rm m1}$ denotes the meshing damping coefficient between gears 1 and 2, $C_{\rm m3}$ corresponds to the meshing damping coefficient between gears 3 and 5, and $C_{\rm m6}$ indicates the meshing damping coefficient between gears 6 and 7.

$$C_{\rm ms} = C_{\rm mr} + C_{\rm m1} + 2 \times C_{\rm m3} + C_{\rm m6} \tag{5}$$

The magnetic torque is:

$$T_3 = n_0 n_1 n_2 \cdot C_e \cdot \dot{\theta}_0(t) \tag{6}$$

$$n_0 = z_r / z_1, n_1 = z_3 / z_5, n_2 = z_6 / z_7 \tag{7}$$

Among these parameters, C_e indicates the system's magnet damping coefficient, while z_r , z_1 , z_3 , z_5 , z_6 , and z_7 denote the tooth counts of the ring gear, gear 1, 3, 5, 6, and 7, respectively.

Note. S2

Magnetic force model

$$\phi_x^N = -U_{mn}^N W_{pq}^N \ln(r^N - U_{mn}^N) - V_{ul}^N W_{pq}^N \ln(r^N - V_{ul}^N) + U_{ij}^N V_{ul}^N \tan^{-1}\left(\frac{U_{ij}^N V_{ul}^N}{r^N W_{pq}^N}\right) - r^N W_{pq}^N \tag{8}$$

where U_{mn}^N , V_{ul}^N , W_{pq}^N and r^N can be calculated as:

$$\begin{cases} U_{mn}^{N} = d_{x}^{N} + (-1)^{n} L - (-1)^{m} L^{N} \\ V_{ul}^{N} = d_{y}^{N} + (-1)^{l} W - (-1)^{u} W^{N} \\ W_{pq}^{N} = d_{z}^{N} + (-1)^{q} H - (-1)^{p} H^{N} \\ r^{N} = \sqrt{(U_{mn}^{N})^{2} + (V_{ul}^{N})^{2} + (W_{pq}^{N})^{2}} \end{cases}$$

$$\tag{9}$$

In this context, the parameters the L^{N} , W^{N} and H^{N} denote the extent, breadth, and depth of magnet A, respectively. Similarly, the terms L, W, and H correspond to the extent, breadth, and depth of magnet B. The orthogonal projection distances of magnets A and B along the x, y, and z

axes within the Cartesian coordinate system are represented by d_x^N , d_y^N , and d_z^N , respectively.

Magnets A and B are attached on the rotor and the PZT unit, respectively, and are situated within the x-y plane. Consequently, the perpendicular separation from magnet A to magnet B can be described as follows:

$$\begin{cases} d_x^N = r_m + d_{x0}^N - r_m \cos(\omega t - \varphi^N) - x(t) \\ d_y^N = r_m \sin(\omega t - \varphi^N) \\ d_z^N = 0 \end{cases}$$
(10)

In this context, r_m represents the radius of gyration of magnet A, which is fixed on the rotor; d_{x0}^N represents the original distance in the designated direction from magnet A to magnet B; x(t)

indicates the displacement of magnet B; φ^N refers to the angular change of magnet A at its initial position; and q signifies the number of magnet A units present.

$$\varphi^{i+1} = \varphi^i + 2\pi / q \tag{11}$$