

Supporting Information

Disorder by Design: High-Entropy Oxide as Next Generation Thermoelectric Materials

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S1. Mole fractions of precursor oxides and high entropy oxides:

Following Banerjee et al.'s¹ thermodynamic feasibility calculations, several authors²⁻⁵ have used the same approach for their respective high entropy oxides. Table S1 presents the calculated coefficients (a-f and a_1 - f_1) for Equation 16, governing the thermodynamic transition from precursor oxides to high entropy oxides.

Table S1: Mole fractions of precursor oxides ($a_1, b_1, \dots, f_1$) and high entropy oxides (a, b, ..., f) as described in equation 16.

Final Product	Precursors											
HEO	$A_{a_1}O_x$	a/a_1	$B_{b_1}O_x$	b/b_1	$C_{c_1}O_x$	c/c_1	$D_{d_1}O_x$	d/d_1	$E_{e_1}O_x$	e/e_1	$F_{f_1}O_x$	f/f_1
$\text{Sr}(\text{Ti}_{0.2}\text{Mo}_{0.2}\text{Fe}_{0.2}\text{Nb}_{0.2}\text{Cr}_{0.2})\text{O}_3^1$	SrCO_3	$0.2/1$	TiO_2	$0.2/1$	MoO_3	$0.2/1$	Fe_2O_3	$0.2/2$	Nb_2O_5	$0.2/2$	Cr_2O_3	$0.2/2$
$(\text{Sr}_{0.2}\text{Ba}_{0.2}\text{La}_{0.2}\text{Eu}_{0.2}\text{Pb}_{0.2})\text{Nb}_2\text{O}_6^3$	SrCO_3	$0.2/1$	BaCO_3	$0.2/1$	La_2O_3	$0.2/2$	Eu_2O_3	$0.2/2$	PbO	$0.2/1$	Nb_2O_5	$2/2$
$\text{Sr}(\text{Ce}_{0.05}\text{Sn}_{0.08}\text{Zr}_{0.2}\text{Ti}_{0.16}\text{Y}_{0.3}\text{Nb}_{0.11}\text{Al}_{0.1})\text{O}_{2.9}^4$	SrCO_3	$0.2/1$	CeO_2	$.05/1$	SnO_2	$.08/1$	ZrO_2	$0.2/1$	TiO_2	$.16/1$	Y_2O_3	$0.3/2$

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									Nb ₂ O ₅	.11/2	Al ₂ O ₃	0.1/2
(Sr _{0.2} Ba _{0.2} Li _{0.2} K _{0.2} Na _{0.2})Nb ₂ O ₆ ⁵	SrCO ₃	0.2/1	BaC O ₃	0.2/1	Li ₂ C O ₃	0.2/2	K ₂ CO ₃	0.2/2	Na ₂ CO ₃	0.2/2	Nb ₂ O ₅	2/2
(Sr _{1/3} Ba _{1/3} Ca _{1/3})TiO ₃ ²	SrCO ₃	.33/1	BaC O ₃	.33/1	CaCO ₃	.33/1	TiO ₂	1/1	Na ₂ CO ₃	0.2/2	Nb ₂ O ₅	0.2/2

S2. Mathematical proof of the fact that the possible high entropy alloys will be much more than lower component alloys (such as- binary, ternary alloys etc.):

Let's consider two alloys with the number of elements **r** and **r+1**. The elements will be selected from **n** number of chemical elements.

The formula to calculate the number of ways to choose **r** elements from a set of **n** elements will be, $N_1 = C(n, r) = \frac{n!}{r!(n-r)!} \dots (S1)$

Similarly, when we select **r+1** elements from a possible set of **n** species, the number of selection will be, $N_2 = C(n, r+1) = \frac{n!}{(r+1)!(n-(r+1))!} \dots (S2)$

Let's take the ratio of these two numbers and we obtain:

$$R = \frac{N_1}{N_2} = \frac{C(n, r)}{C(n, r+1)} = \frac{\frac{n!}{r!(n-r)!}}{\frac{n!}{(r+1)!(n-(r+1))!}} = \frac{(r+1)!(n-(r+1))!}{r!(n-r)!} \dots (S3)$$

Now, applying the relations $(r+1)! = (r+1) \times r!$ and $(n-r)! = (n-r) \times (n-r-1)!$, we obtain,

$$R = \frac{(r+1)}{(n-r)} \dots (S4)$$

If $r \leq n/2$, then $(n-r) > (r+1)$, or in other words, $R = \frac{(r+1)}{(n-r)} < 1 \dots (S5)$

This result indicates that for two alloys — one with **r** elements and another with **r+1** elements — the number of possible alloys will always be greater for the alloy containing **r+1** elements, provided that $r \leq n/2$.

Since at least 40 to 50 metallic elements can potentially form high-entropy alloys (HEAs) with 5, 6 or 7 components, the condition $r \ll n/2$ holds true in the case of HEAs. Consequently, the number of possible HEAs far exceeds that of lower-component alloys, highlighting the vast compositional space available for HEAs compared to traditional binary, ternary, or quaternary alloys.

References:

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