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# **Supporting Information**

# The Experimental Phase Equilibria Studies of the Fe-Sb-As System

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#### S1 The industrial applications of the Fe-Sb-As system

Peterson and Twidwell <sup>1</sup> reported the removal of arsenic by roasting with pyrite from Sb-As containing lead bullion was reported. Filippou et al. <sup>2</sup> reported 6 wt.% Sb in enargite (Cu<sub>3</sub>As<sub>0.8</sub>Sb<sub>0.2</sub>S<sub>4</sub>), a key mineral in coppergold deposits. They also reported high As-containing minerals can be separated into two types of feed (As-rich and As-lean but rich in precious metals) by adjusting pulp-potential <sup>2</sup>.

In new pyrometallurgical technology, As- and Sb-rich feeds are treated to sulfidization roasting under reducing conditions, halogenation, and carbothermic reduction to form copper arsenide <sup>2</sup>. Nazari et al. <sup>3</sup> identified the presence of As with Sb in minerals like arsenopyrite, oliverite, which are undesirable during copper extraction. These are removed via volatilization to improve crude Cu and sulfuric acid production from released SO<sub>2</sub>. They also reported that arsenic can be removed as ferric arsenate <sup>3</sup>.

Nshimiyimana et al. <sup>4</sup> identified Fe-Sb-As-containing arsenopyrite ( $Fe_{0.95}Co_{0.05}$ )( $As_{0.97}Sb_{0.01}$ )S and freibergite ( $Ag_{5.7}Cu_{4.6}Fe_{1.8}$ )( $Sb_{3.9}As_{0.2}$ )S<sub>13</sub> minerals. Majzlan et al. <sup>5</sup> reported As-Sb and Fe-Sb-As components in trombolite and tetrahedrite (Cu,Fe,Zn)<sub>12</sub>(Sb,As)<sub>4</sub>S<sub>13</sub>, respectively. Jurkovic <sup>6</sup> observed Fe-Sb-As metals in different minerals, including As-Sb bearing goethite ( $\alpha$ -FeOOH), As-bearing tripuhyite (FeSbO<sub>4</sub>), senarmontite ( $Sb_2O_3$ ), and cervantite ( $Sb_2O_4$ ) in soils.

Zhang et al.<sup>7</sup> noted that Fe-Sb-As metals in acid mine drainage, caused by minerals exploration and utilization, rigorously contaminate ecological environments. They also reported that As-containing slag poses ecological risks, which can be mitigated by forming stable As phases during pyrometallurgical operations <sup>8</sup>. During Sn smelting, the slag contained around 10-15 wt.% Sb and 1-3 wt.% As. As-Sb dust contains 0.5–1% As and 2–4% Sb.

## S2. The Fe-As system

Friedrich <sup>9</sup> used thermal analysis and microscopy and determine the phase diagram from the compositions of 6-49 at. % As. Oberhoffer and Gallaschik <sup>10</sup> used thermal analysis, microscopy, and magnetic content analysis to determination the phase diagram from 0-32 at. % As and magnetic transition. Jones <sup>11</sup> measured diffusion of arsenic in iron and determine the saturation composition of iron (FCC) at 1423 K. Svechnikov and Gridnev <sup>12</sup> used a dilatometry, microscopy, and XRD to determine limits of the iron (FCC) saturation loop. Sawamura and Mori <sup>13</sup> used thermal analysis and microscopy and reported the solubility of arsenic in iron (FCC) based on extrapolations from measurements made on alloys of iron and arsenic containing low concentrations of carbon. Sawamura et al.<sup>14</sup> used a DTA to determine the phase diagram between 40 to 57 at. % As. Svechnikov and Shurin <sup>15</sup> used thermal analysis, microscopy, and XRD to determine the limits of the solubility of arsenic in iron (FCC). Svechnikov et al. <sup>16</sup> used microhardness, microscopy and XRD to determine the solid solubility of arsenic in iron (FCC). Clark <sup>17</sup> used DTA, optical microscopy and XRD to study the Fe-As system. Clark <sup>18</sup> used optical microscopy and XRD to study the Fe-As system. Clark <sup>18</sup> used optical microscopy and XRD to study the Fe-As system. Predel and Frebel <sup>19</sup> used DTA to determine the solid solubility of arsenic in iron (BCC). Bozic <sup>20</sup> used thermal analysis to determine the maximum solid solubility of arsenic in iron (BCC) at the eutectic temperature. Pei et al. <sup>21</sup> and Kidari and Chartrand <sup>22</sup> thermodynamically assessed the

Fe-As system. Ugai et al. <sup>23</sup> used DTA and XRD and reported the pressure-temperature-composition diagram for the Fe-As system for 0.50-1.0 at. % As.











(c) Fe(As, Sb) liquidus (Sample 30-61)





















(i) Boundary between Fe(As, Sb) and Fe(As, Sb)<sub>2</sub> primary phase fields (Sample 88-92)











Figure S1 Microstructures for the Fe-Sb-As systems in the same chronological order with phases given in Table S1.











![](_page_28_Figure_0.jpeg)

Figure S2 Microstructures for the Fe-As systems in the same chronological order given in Table S2.

![](_page_29_Figure_0.jpeg)

![](_page_30_Figure_0.jpeg)

![](_page_31_Figure_0.jpeg)

![](_page_32_Figure_0.jpeg)

Figure S3 Microstructures for the Fe-Sb systems in the same chronological order given in Table S3.

Table S1 Measured composition of the phases (average values and standard deviation) in the Fe-Sb-As system, expressed in mol.% with  $SiO_2$  substrate of each phase equilibrated at fixed temperature and fixed first preheating at 600 °C for 1 h to all arsenic containing samples with or without second preheating.

S.	Preheat 2	Equilib	ration	Phase	Nor	malized mo	I. %	Unnormalized
no.	(°C/h)	T (°C)	t (h)		Fe	Sb	As	(wt.%)
(a) B0	CC-Fe liqui	dus		•				
1	-	1000	7	Liquid metal	$68.4 \pm 0.2$	$28.3 \pm 0.2$	$3.4 \pm 0.0$	100.33
				BCC-Fe	$94.1\pm0.1$	$4.0\pm0.0$	$1.9 \pm 0.1$	100.20
2	-	1000	4.75	Liquid metal	$69.7 \pm 0.1$	$24.4 \pm 0.1$	$5.9 \pm 0.1$	100.33
				BCC-Fe	$93.6 \pm 0.0$	$3.1 \pm 0.0$	$3.3\pm0.0$	100.32
3	-	950	4	Liquid metal	$71.0 \pm 0.2$	$16.5 \pm 0.2$	$12.5 \pm 0.2$	100.33
				BCC-Fe	$92.5 \pm 0.0$	$1.9\pm0.0$	$5.6 \pm 0.0$	100.36
(b) M	$eX = Fe_{1+x}($	Sb, As) li	quidus	1				
4	-	1000	6	Liquid metal	$65.2 \pm 0.7$	$30.9\pm0.9$	$4.0 \pm 0.2$	100.38
				MeX	$59.1 \pm 0.2$	$39.3 \pm 0.2$	$1.6 \pm 0.1$	99.72
5	-	950	5.5	Liquid metal	$39.7 \pm 2.3$	$55.6 \pm 2.5$	$4.7 \pm 0.3$	100.12
				MeX	$54.4 \pm 0.2$	$41.2 \pm 0.2$	$4.4 \pm 0.1$	99.92
6	-	950	5.5	Liquid metal	$43.0 \pm 0.9$	$26.4 \pm 1.5$	$30.6 \pm 0.7$	100.06
				MeX	$53.8 \pm 0.1$	$6.2 \pm 0.1$	$40.0 \pm 0.2$	100.21
7	-	950	6	Liquid metal	$68.5 \pm 0.5$	$18.2 \pm 0.7$	$13.3 \pm 0.7$	100.26
				MeX	$57.9 \pm 0.1$	$35.4 \pm 0.1$	$6.7 \pm 0.0$	100.07
8	-	950	4.25	Liquid metal	$48.7 \pm 1.2$	$38.1 \pm 1.4$	$13.1 \pm 0.3$	100.09
				MeX	$55.4 \pm 0.2$	$31.0 \pm 0.2$	$13.6 \pm 0.1$	100.29
9	-	950	4.25	Liquid metal	$43.9 \pm 0.9$	$47.1 \pm 1.1$	$9.0 \pm 0.2$	100.17
			_	MeX	$55.0 \pm 0.2$	$34.7 \pm 0.1$	$10.3 \pm 0.1$	99.65
10	_	950	12.25	Liquid metal	$48.8 \pm 0.7$	$20.8 \pm 1.0$	$30.4 \pm 0.4$	100.31
				MeX	$55.0 \pm 0.1$	$10.2 \pm 0.1$	$34.8 \pm 0.1$	100.18
11	1000/0.5	925	19.75	Liquid metal	$38.7 \pm 0.4$	$48.4 \pm 0.6$	$12.9 \pm 0.3$	100.29
				MeX	$55.1 \pm 0.2$	$24.1 \pm 0.1$	$20.8 \pm 0.1$	100.17
12	1000/0.5	925	20	Liquid metal	$39.1 \pm 0.6$	$37.6 \pm 1.0$	$23.4 \pm 0.4$	100.16
				MeX	$54.8 \pm 0.1$	$11.9 \pm 0.1$	$33.3 \pm 0.1$	100.26
13	1000/0.5	925	20.75	Liquid metal	$28.1 \pm 1.0$	$47.5 \pm 1.5$	$24.4 \pm 0.6$	100.28
				MeX	$52.9 \pm 0.1$	$7.3 \pm 0.0$	$39.8 \pm 0.1$	100.32
14	-	925	25.5	Liquid metal	$42.1 \pm 0.4$	$40.0 \pm 0.5$	$18.0 \pm 0.4$	100.13
				MeX	$55.3 \pm 0.1$	$20.7 \pm 0.1$	$24.0 \pm 0.1$	100.30
15	1000/0.5	900	4	Liquid metal	$27.0 \pm 0.8$	$64.5 \pm 1.4$	$8.5 \pm 0.8$	100.16
				MeX	$55.0 \pm 0.5$	$24.0 \pm 0.3$	$21.0 \pm 0.2$	100.11
16	1000/0.5	900	15	Liquid metal	$20.1 \pm 0.9$	$65.8 \pm 1.4$	$14.2 \pm 0.6$	100.13
				MeX	$53.8 \pm 0.1$	$10.7 \pm 0.1$	$35.5 \pm 0.1$	100.22
17	1000/0.5	900	6	Liquid metal	$29.5 \pm 1.0$	$67.6 \pm 1.0$	$2.9 \pm 0.1$	100.23
				MeX	$53.6 \pm 0.2$	$41.9 \pm 0.2$	$4.5 \pm 0.1$	100.38
18	1000/0.5	900	20	Liquid metal	$66.0 \pm 0.2$	$8.8 \pm 0.2$	$25.2 \pm 0.1$	100.35
				MeX	$59.0 \pm 0.1$	$19.0 \pm 0.1$	$22.1 \pm 0.1$	100.20
19	1000/0.5	850	12	Liquid metal	$21.6 \pm 2.3$	$71.9 \pm 3.3$	$6.5 \pm 1.0$	100.21
				MeX	$53.8 \pm 0.1$	$25.7 \pm 0.3$	$20.5 \pm 0.3$	100.09
20	950/0.5	850	15	Liquid metal	$14.5 \pm 0.7$	$76.6 \pm 1.2$	$8.9 \pm 0.6$	100.29
				MeX	$53.0 \pm 0.1$	$14.8 \pm 0.2$	$32.2 \pm 0.1$	100.19
21	1000/0.5	850	8	Liquid metal	$12.8 \pm 0.7$	$77.4 \pm 1.0$	$9.7 \pm 0.9$	100.39
			_	MeX	$52.5 \pm 0.1$	9.8 ± 1.2	$37.7 \pm 1.2$	100.12
22	1000/0.5	850	6.5	Liquid metal	$13.1 \pm 0.7$	$77.3 \pm 1.1$	$9.6 \pm 0.5$	100.29
				MeX	$53.0 \pm 0.1$	$11.7 \pm 0.1$	$35.3 \pm 0.0$	100.34

23	1000/0.5	850	13.5	Liquid metal	$22.6\pm0.7$	$74.9\pm0.7$	$2.5\pm0.1$	99.84
				MeX	$53.7 \pm 0.1$	$39.4 \pm 0.1$	$6.9\pm0.1$	100.09
24	1000/0.5	850	21	Liquid metal	$22.2 \pm 0.8$	$74.6 \pm 0.8$	$3.2 \pm 0.1$	99.77
				MeX	$53.7 \pm 0.1$	$39.7 \pm 0.1$	$6.6 \pm 0.0$	100.26
25	900/0.5	800	13	Liquid metal	$13.8\pm0.7$	$82.7 \pm 1.0$	$3.5\pm0.3$	100.26
				MeX	$53.1 \pm 0.1$	$26.6 \pm 0.6$	$20.2\pm0.5$	100.24
26	-	800	11	Liquid metal	$9.3 \pm 2.1$	$84.9\pm2.5$	$5.8\pm1.7$	100.15
				MeX	$52.2\pm0.4$	$21.1 \pm 0.7$	$26.7\pm1.1$	100.34
27	1000/0.5	800	6	Liquid metal	$16.9\pm1.2$	$81.2\pm1.3$	$1.9\pm0.1$	100.20
				MeX	$53.2\pm0.2$	$42.4 \pm 0.1$	$4.5\pm0.1$	100.24
28	1000/0.5	750	43	Liquid metal	$9.7 \pm 0.2$	$88.2 \pm 0.2$	$2.1\pm0.1$	100.22
				MeX	$52.4 \pm 0.1$	$31.3 \pm 0.2$	$16.3\pm0.3$	100.26
29	1000/0	750	6	Liquid metal	$8.0 \pm 0.6$	$89.2 \pm 0.8$	$2.8\pm0.3$	100.43
				MeX	$52.4 \pm 0.1$	$22.2 \pm 0.5$	$25.4\pm0.5$	100.33
(c) Fe	(As, Sb) liq	uidus				1		
30	-	1000	5	Liquid metal	$39.4 \pm 0.7$	$13.3 \pm 1.2$	$47.3\pm1.2$	100.42
				FeAs	$49.4 \pm 0.1$	$0.43 \pm 0.01$	$50.2 \pm 0.1$	100.98
31	-	975	7	Liquid metal	$27.5 \pm 1.0$	$28.3 \pm 1.4$	$44.2 \pm 0.6$	100.17
				FeAs	$50.2 \pm 0.1$	$0.06 \pm 0.01$	$49.7\pm0.1$	100.72
32	-	975	4.5	Liquid metal	$42.5 \pm 0.7$	$20.3 \pm 1.0$	$37.2 \pm 0.5$	100.30
				FeAs	$50.5 \pm 0.1$	$0.94 \pm 0.11$	$48.6 \pm 0.1$	100.84
33	-	975	6.5	Liquid metal	$27.5 \pm 0.8$	$31.9 \pm 1.2$	$40.6\pm0.9$	100.09
				FeAs	$50.1 \pm 0.2$	$0.15 \pm 0.01$	$49.8\pm0.2$	100.04
34	-	975	5	Liquid metal	$30.5 \pm 0.6$	$32.8 \pm 0.9$	$36.7\pm0.5$	100.31
				FeAs	$49.6 \pm 0.1$	$0.90 \pm 0.02$	$49.6 \pm 0.1$	100.86
35	-	975	5	Liquid metal	$28.7 \pm 2.8$	$22.9 \pm 3.7$	$48.3 \pm 1.4$	100.32
				FeAs	$49.5 \pm 0.1$	$0.39 \pm 0.02$	$50.1 \pm 0.1$	100.79
36	1000/0.5	950	20.5	Liquid metal	$34.1 \pm 0.7$	$35.7 \pm 1.1$	$30.3 \pm 0.6$	100.18
	1000/0 5	0.50		FeAs	$49.0 \pm 0.2$	$1.5 \pm 0.0$	$49.5 \pm 0.2$	100.09
37	1000/0.5	950	21.5	Liquid metal	$19.0 \pm 1.3$	$42.6 \pm 2.2$	$38.4 \pm 1.0$	100.31
20	1000/0.5	0.50	- 21	FeAs	$49.5 \pm 0.2$	$0.55 \pm 0.01$	$50.0 \pm 0.2$	100.68
38	1000/0.5	950	21	Liquid metal	$20.3 \pm 1.4$	$45.7 \pm 2.2$	$34.1 \pm 0.8$	100.34
20		050	5	FeAs	$49.5 \pm 0.1$	$0.73 \pm 0.01$	$49.8 \pm 0.1$	100.38
39	-	950	5	Liquid metal	$21.4 \pm 0.7$	$46.4 \pm 1.1$	$32.2 \pm 0.4$	100.42
40	1000/0 5	050	22	FeAs	$49.7 \pm 0.1$	$0.83 \pm 0.02$	$49.3 \pm 0.1$	100.84
40	1000/0.5	950	22	Liquid metal	$21.8 \pm 2.1$	$46.4 \pm 3.8$	$31.8 \pm 1.8$	100.22
41		050	5 75	FeAs	$49.8 \pm 0.2$	$0.87 \pm 0.02$	$49.3 \pm 0.2$	100.30
41	-	930	5.75	Equid metal	$28.3 \pm 1.8$	$42.4 \pm 3.4$	$29.3 \pm 1.8$	100.13
12		050	5 75	FeAs	$30.1 \pm 0.1$	$0.80 \pm 0.03$	$49.1 \pm 0.1$	100.20
42	-	930	5.75	Equid metal	$10.0 \pm 1.7$	$37.7 \pm 1.3$	$43.3 \pm 3.0$ $50.0 \pm 0.1$	100.37
12		050	5 25	Liquid motal	$49.7 \pm 0.1$ 10.8 $\pm$ 1.1	$0.33 \pm 0.02$	$30.0 \pm 0.1$ $48.1 \pm 2.1$	100.93
43	-	950	5.25	Equila metai	$19.0 \pm 1.1$ $40.2 \pm 0.1$	$32.1 \pm 2.0$	$40.1 \pm 2.1$ 50 2 $\pm$ 0 1	100.44
11		025	5.5	Liquid metal	$\frac{49.3 \pm 0.1}{26.6 \pm 0.8}$	$10.38 \pm 0.03$	$30.3 \pm 0.1$ 23.6 ± 0.6	100.33
	-	125	5.5	Elquid metal FeAs	$20.0 \pm 0.0$ $49.8 \pm 0.4$	13+00	$23.0 \pm 0.0$ $49.0 \pm 0.4$	100.32
45		925	6	I jouid metal	$10.8 \pm 0.9$	$1.5 \pm 0.0$ 53 7 + 0.8	$\frac{47.0 \pm 0.4}{35.5 \pm 0.7}$	100.47
	-	125	0	Fede	$10.0 \pm 0.9$ 50 0 + 0 1	0.00 + 0.00	$50.0 \pm 0.7$	100.31
46		925	5	Liquid metal	$13.6 \pm 0.1$	$643 \pm 0.00$	$22.0 \pm 0.1$	100.09
	-	125	5	Fede	$502 \pm 0.3$	$0.56 \pm 0.9$	$49.2 \pm 0.3$	100.22
47	1000/0 5	925	20.75	Liquid metal	$18.3 \pm 0.2$	$62.5 \pm 0.05$	$19.2 \pm 0.2$ $19.2 \pm 0.9$	100.23
.,	1000/010	/	20.70	FeAs	$50.0 \pm 0.1$	$1.7 \pm 0.3$	$48.3 \pm 0.3$	100.22
48	1000/0.5	925	20	Liquid metal	$12.3 \pm 0.8$	$62.5 \pm 1.1$	$25.3 \pm 0.6$	100.40
				FeAs	$49.6 \pm 0.1$	$0.79\pm0.02$	$49.6 \pm 0.1$	100.82

49	1000/0.5	925	19.75	Liquid metal	$10.8\pm0.6$	$50.7 \pm 1.1$	$38.5 \pm 0.8$	100.30
				FeAs	$49.8\pm0.1$	$0.37\pm0.01$	$49.9\pm0.1$	100.21
50	1000/0.5	900	14	Liquid metal	$17.2\pm0.5$	$67.3 \pm 0.9$	$15.5 \pm 0.5$	100.10
				FeAs	$49.7\pm0.1$	$1.9 \pm 0.1$	$48.4 \pm 0.1$	100.33
51	950/0.5	900	58	Liquid metal	$7.7\pm0.6$	$72.0 \pm 1.2$	$20.3\pm0.7$	100.05
				FeAs	$49.8\pm0.1$	$0.80\pm0.04$	$49.4\pm0.1$	99.97
52	1000/0.5	900	21	Liquid metal	$9.0\pm0.7$	$73.0\pm1.4$	$18.0\pm0.7$	100.09
				FeAs	$49.7\pm0.2$	$0.89\pm0.02$	$49.5\pm0.2$	100.76
53	-	850	36	Liquid metal	$5.3\pm0.3$	$79.8\pm0.7$	$14.9\pm0.4$	100.18
				FeAs	$49.8\pm0.1$	$0.61\pm0.03$	$49.6\pm0.1$	100.34
54	1000/0.5	850	8	Liquid metal	$6.5\pm0.9$	$80.6\pm1.8$	$12.9\pm0.9$	100.23
				FeAs	$49.8\pm0.1$	$1.1 \pm 0.1$	$49.1\pm0.1$	100.67
55	-	800	10	Liquid metal	$2.8\pm0.4$	$82.8\pm0.9$	$14.5\pm0.6$	100.26
				FeAs	$49.4\pm0.2$	$0.36\pm0.04$	$50.3\pm0.2$	100.74
56	1000/0.5	800	4.5	Liquid metal	$2.4\pm0.3$	$82.1\pm0.5$	$15.5\pm0.3$	100.32
				FeAs	$49.0\pm0.1$	$0.61\pm0.06$	$50.4\pm0.2$	100.30
57	1000/0.5	800	11.5	Liquid metal	$5.5\pm0.6$	$86.3 \pm 1.4$	$8.2\pm0.8$	100.32
				FeAs	$49.9\pm0.1$	$1.4 \pm 0.3$	$48.7\pm0.2$	100.62
58	850/0.5	750	56	Liquid metal	$1.2 \pm 0.2$	$86.4\pm0.7$	$12.4\pm0.7$	99.66
				FeAs	$49.7\pm0.1$	$0.35\pm0.08$	$49.9\pm0.1$	100.48
59	1000/0.5	750	12.5	Liquid metal	$3.8\pm0.2$	$91.6\pm0.3$	$4.6\pm0.2$	100.43
				FeAs	$49.8\pm0.1$	$1.1 \pm 0.1$	$49.1\pm0.2$	101.00
60	1000/0.5	700	13.5	Liquid metal	$1.4 \pm 0.1$	$92.4 \pm 0.2$	$6.2\pm0.1$	100.28
				FeAs	$49.5\pm0.2$	$0.60 \pm 0.30$	$49.9\pm0.3$	100.65
61	1000/0.5	650	10.25	Liquid metal	$1.3\pm0.1$	$95.2\pm0.1$	$3.5\pm0.1$	100.15
				FeAs	$50.1\pm0.2$	$0.66\pm0.23$	$49.3\pm0.2$	100.36
(d) Fe	(As, Sb) <sub>2</sub> li	quidus						
62	-	900	5.5	Liquid metal	$6.7 \pm 0.5$	$58.8\pm0.9$	$34.4\pm0.9$	100.29
				FeAs <sub>2</sub>	$33.3 \pm 0.1$	$1.2 \pm 0.1$	$65.5\pm0.2$	101.00
63	1000/0.5	850	19	Liquid metal	$3.9\pm0.6$	$72.0 \pm 1.3$	$24.1 \pm 0.9$	100.36
				FeAs <sub>2</sub>	$32.9\pm0.1$	$1.3 \pm 0.2$	$65.8\pm0.2$	100.13
64	1000/0.5	850	36.5	Liquid metal	$2.7 \pm 0.3$	$65.3 \pm 0.8$	$32.1 \pm 0.5$	100.29
				FeAs <sub>2</sub>	$33.2 \pm 0.2$	$0.92 \pm 0.22$	$65.9 \pm 0.2$	100.91
65	1000/0.5	850	18.5	Liquid metal	$3.4 \pm 0.3$	$70.8 \pm 0.7$	$25.8 \pm 0.4$	100.12
				FeAs <sub>2</sub>	$33.2 \pm 0.1$	$0.85 \pm 0.13$	$65.9 \pm 0.2$	100.91
66	-	850	42	Liquid metal	$2.8 \pm 0.1$	$66.5 \pm 0.4$	$30.7 \pm 0.3$	100.42
				FeAs <sub>2</sub>	$33.6 \pm 0.1$	$0.77 \pm 0.05$	$65.7 \pm 0.2$	100.05
67	1000/0.5	800	14	Liquid metal	$2.0 \pm 0.2$	$79.7 \pm 0.5$	$18.2 \pm 0.4$	100.17
				FeAs <sub>2</sub>	$32.8 \pm 0.1$	$1.3 \pm 0.2$	$65.9 \pm 0.1$	100.25
68	1000/0.5	800	36.5	Liquid metal	$1.1 \pm 0.1$	$68.9 \pm 0.4$	$30.1 \pm 0.4$	99.83
				FeAs <sub>2</sub>	$33.5 \pm 0.1$	$0.80 \pm 0.23$	$65.7 \pm 0.3$	100.53
69	1000/0.5	800	13.5	Liquid metal	$1.8 \pm 0.5$	$76.5 \pm 0.6$	$21.7 \pm 0.3$	100.42
				FeAs <sub>2</sub>	$32.8 \pm 0.2$	$1.0 \pm 0.2$	$66.1 \pm 0.3$	101.02
70	-	800	16	Liquid metal	$1.0 \pm 0.8$	$66.6 \pm 0.8$	$32.5 \pm 0.6$	99.87
				FeAs <sub>2</sub>	$33.1 \pm 0.1$	$0.44 \pm 0.02$	$66.4 \pm 0.1$	100.99
71	1000/0.5	800	6.5	Liquid metal	$1.1 \pm 0.1$	$70.5 \pm 0.3$	$28.3 \pm 0.2$	100.25
	1005/5		• -	FeAs <sub>2</sub>	$33.4 \pm 0.4$	$0.99 \pm 0.82$	$65.6 \pm 0.4$	100.38
72	1000/0.5	750	39	Liquid metal	$1.1 \pm 0.2$	$85.3 \pm 0.6$	$13.6 \pm 0.4$	100.16
	0.50/0.5			FeAs <sub>2</sub>	$33.3 \pm 0.1$	$1.4 \pm 0.1$	$65.3 \pm 0.1$	100.51
73	⊢ <u>850/0 5</u>	750	13	Liquid metal	$10.60 \pm$	$+78.0\pm0.3$	$ 21.4 \pm 0.2 $	99.62
	050/0.5	750	15		0.11			
	850/0.5	750	15	FeAs <sub>2</sub>	0.11 33.6 ± 0.2	0.26 ± 0.19	66.1 ± 0.2	100.67

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		n.				0.07			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					FeAs <sub>2</sub>	$33.4 \pm 0.1$	$0.62 \pm 0.39$	$66.0 \pm 0.4$	100.86
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	75	1000/5mi	700	14.5	Liquid metal	0.94 ±	$90.7 \pm 0.1$	$8.3\pm0.1$	100.33
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		n.				0.11			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					FeAs <sub>2</sub>	$33.5\pm0.1$	$1.8 \pm 0.3$	$64.7\pm0.3$	99.99
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	76	1000/0.5	700	11.5	Liquid metal	0.36 ±	$78.9\pm0.3$	$20.7\pm0.2$	100.14
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$						0.08			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					FeAs <sub>2</sub>	$33.2\pm0.0$	$1.1 \pm 0.5$	$65.7\pm0.5$	100.41
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	77	800/0.5	700	14.25	Liquid metal	$0.50 \pm$	$80.0 \pm 0.5$	$19.5 \pm 0.4$	99.71
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$						0.11			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					FeAs <sub>2</sub>	$33.2 \pm 0.5$	$1.04 \pm 0.37$	$65.7 \pm 0.4$	100.61
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	78	950/0.5	650	12	Liquid metal	$0.52 \pm$	$89.9 \pm 0.3$	$9.6 \pm 0.3$	99.67
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$						$0.0^{7}$	0.26 + 0.25	C(1 + 0.4)	100.50
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	70	050/0.5	(50	1.5	$FeAs_2$	$33.6 \pm 0.0$	$0.36 \pm 0.35$	$66.1 \pm 0.4$	100.59
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	/9	830/0.5	650	15	Liquid metal	$0.2/\pm$	$/9.2 \pm 0.5$	$20.5 \pm 0.3$	99.71
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					Fals	0.14	$0.40 \pm 0.55$	$66.0 \pm 0.6$	100 50
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	80	800/0.5	650	10.5	Liquid motal	$0.25 \pm 0.1$	$0.49 \pm 0.33$	$00.0 \pm 0.0$	00.70
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	00	800/0.5	030	10.5		$0.25 \pm$	$79.3 \pm 0.1$	$20.4 \pm 0.1$	99.19
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					Fedse	333 + 01	$0.34 \pm 0.42$	$664 \pm 04$	100 39
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	(e) M	$eX_{a}$ (Me = 1	Fe and X	= Sh and	$\frac{1}{4}$ As) liquidus	$55.5 \pm 0.1$	0.54 ± 0.42	00.7 ± 0.7	100.57
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	81	1000/0.5	650	36.5	Liquid metal	$2.2 \pm 0.2$	$96.1 \pm 0.3$	$1.7 \pm 0.1$	100.00
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		1000,010	000	2012	MeX <sub>2</sub>	$33.6 \pm 0.1$	$60.5 \pm 0.1$	$5.9 \pm 0.1$	100.36
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	(f) Bo	undary bety	ween BCC	C-Fe and	$MeX = Fe_{1+x}$	(Sb. As) pri	mary phase f	ields	100.00
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	82	-	975	6.5	Liquid metal	$68.9 \pm 0.4$	$24.2 \pm 0.6$	$7.0 \pm 0.4$	100.34
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					BCC-Fe	$93.6 \pm 0.1$	$3.0 \pm 0.0$	$3.4 \pm 0.0$	100.40
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					MeX	$59.7 \pm 0.1$	$37.8 \pm 0.1$	$2.4 \pm 0.0$	100.31
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	83	1000/0.5	900	4	Liquid metal	$71.7 \pm 0.2$	$11.4 \pm 0.1$	$16.9\pm0.2$	100.08
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					BCC-Fe	$91.5\pm0.0$	$1.3 \pm 0.0$	$7.1 \pm 0.0$	99.96
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					MeX	$59.0\pm0.0$	$32.8 \pm 0.1$	$8.1 \pm 0.1$	99.69
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	84	950/0.5	900	10.75	Liquid metal	$72.3\pm0.5$	$10.2\pm0.3$	$17.5\pm0.6$	100.33
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					BCC-Fe	$91.4\pm0.2$	$1.3 \pm 0.1$	$7.3\pm0.1$	100.26
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					MeX	$59.8\pm0.2$	$31.6 \pm 0.1$	$8.6\pm0.1$	100.19
$ \begin{array}{ c c c c c c c c } \hline BCC-Fe & 91.0 \pm 0.1 & 0.86 \pm 0.02 & 8.1 \pm 0.1 & 100.28 \\ \hline MeX & 60.0 \pm 0.1 & 27.5 \pm 0.1 & 12.5 \pm 0.0 & 100.40 \\ \hline (g) Boundary between MeX = Fe_{1+x}(Sb, As) and Fe(As, Sb) primary phase fields \\ \hline 86 & 1000/0.5 & 750 & 36 & Liquid metal & 6.2 \pm 0.6 & 90.6 \pm 0.9 & 3.2 \pm 0.3 & 100.32 \\ \hline MeX & 51.9 \pm 0.1 & 18.8 \pm 0.4 & 29.3 \pm 0.4 & 100.29 \\ \hline FeAs & 49.5 \pm 0.3 & 2.6 \pm 0.1 & 47.9 \pm 0.3 & 101.01 \\ \hline (h) Boundary between MeX = Fe_{1+x}(Sb, As) and Fe_2(As, Sb) \\ \hline 87 & 950/0.5 & 850 & 13.5 & Liquid metal & 69.3 \pm 0.5 & 6.0 \pm 0.1 & 24.7 \pm 0.5 & 100.16 \\ \hline MeX & 59.8 \pm 0.2 & 19.5 \pm 0.1 & 20.7 \pm 0.1 & 99.76 \\ \hline Fe_2As & 65.8 \pm 0.1 & 2.6 \pm 0.1 & 31.6 \pm 0.1 & 100.12 \\ \hline (i) Boundary between Fe(As, Sb) and Fe(As, Sb)_2 primary phase fields \\ \hline 88 & - & 950 & 6 & Liquid metal & 20.3 \pm 0.9 & 30.7 \pm 1.4 & 49.0 \pm 0.8 & 100.44 \\ \hline FeAs & 49.7 \pm 0.1 & 0 & 50.3 \pm 0.1 & 100.20 \\ \hline FeAs_2 & 33.6 \pm 0.1 & 0.15 \pm 0.06 & 66.3 \pm 0.2 & 100.91 \\ \hline 89 & - & 925 & 5.5 & Liquid metal & 10.6 \pm 0.4 & 50.2 \pm 1.0 & 39.2 \pm 1.0 & 100.43 \\ \hline FeAs_2 & 34.0 \pm 0.1 & 0.33 \pm 0.07 & 65.6 \pm 0.1 & 100.90 \\ \hline 90 & 1000/0.5 & 925 & 14.25 & Liquid metal & 11.0 \pm 0.5 & 48.5 \pm 1.2 & 40.5 \pm 0.9 & 100.45 \\ \hline FeAs & 49.8 \pm 0.2 & 0.36 \pm 0.02 & 49.8 \pm 0.2 & 100.13 \\ \hline \end{array}$	85	1000/0.5	850	10.25	Liquid metal	$72.0\pm0.1$	$7.8 \pm 0.1$	$20.3\pm0.1$	100.18
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					BCC-Fe	$91.0\pm0.1$	$0.86 \pm 0.02$	$8.1\pm0.1$	100.28
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					MeX	$60.0\pm0.1$	$27.5 \pm 0.1$	$12.5\pm0.0$	100.40
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	(g) Bo	oundary bet	ween Me	$X = Fe_{1+}$	x(Sb, As) and	Fe(As, Sb)	primary phas	e fields	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	86	1000/0.5	750	36	Liquid metal	$6.2 \pm 0.6$	$90.6 \pm 0.9$	$3.2\pm0.3$	100.32
Image: heat of the formula is the formula in the formula is the					MeX	$51.9 \pm 0.1$	$18.8 \pm 0.4$	$29.3 \pm 0.4$	100.29
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					FeAs	$49.5 \pm 0.3$	$2.6 \pm 0.1$	$47.9 \pm 0.3$	101.01
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	(h) Bo	bundary bet	ween Me.	$X = Fe_{1+}$	x(Sb, As) and	$Fe_2(As, Sb)$			100.16
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	87	950/0.5	850	13.5	Liquid metal	$69.3 \pm 0.5$	$6.0 \pm 0.1$	$24.7 \pm 0.5$	100.16
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					MeX	$59.8 \pm 0.2$	$19.5 \pm 0.1$	$20.7 \pm 0.1$	99.76
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	() <b>D</b>	1 1	E-(/		$  Fe_2As$	$ 65.8 \pm 0.1 $	$2.6 \pm 0.1$	$31.6 \pm 0.1$	100.12
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	(1) BO	undary betw	veen Fe(A	AS, SD) a	I intervention (As, Sb)	$_2$ primary p	$\frac{1}{20.7 \pm 1.4}$	40.0 + 0.0	100 44
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	88	-	930	0	Equid metal	$20.3 \pm 0.9$	$30./\pm 1.4$	$49.0 \pm 0.8$	100.44
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					FeAs	$49.7 \pm 0.1$		$30.3 \pm 0.1$	100.20
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	00		025	55	reAs <sub>2</sub>	$33.0 \pm 0.1$	$0.13 \pm 0.00$	$00.3 \pm 0.2$	100.91
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	09	-	923	5.5	Equid metal	$10.0 \pm 0.4$	$50.2 \pm 1.0$	$37.2 \pm 1.0$	100.43
90 1000/0.5 925 14.25 Liquid metal 11.0 $\pm$ 0.5 48.5 $\pm$ 1.2 40.5 $\pm$ 0.9 100.45   FeAs 49.8 $\pm$ 0.2 0.36 $\pm$ 0.02 49.8 $\pm$ 0.2 100 13					Fels	$34.0 \pm 0.1$	$0.33 \pm 0.07$	$+7.7 \pm 0.0$	100.30
FeAs 49.8 $\pm$ 0.2 0.3 $\pm$ 1.2 40.3 $\pm$ 0.3 100.43   FeAs 49.8 $\pm$ 0.2 0.36 $\pm$ 0.02 49.8 $\pm$ 0.2 100 13	90	1000/0.5	925	14 25	Liquid metal	$110 \pm 0.1$	$485 \pm 0.07$	$40.5 \pm 0.1$	100.90
		1000/0.5	220	11.23	FeAs	$49.8 \pm 0.2$	$0.36 \pm 0.02$	$49.8 \pm 0.7$	100.13

				FeAs <sub>2</sub>	$33.4 \pm 0.2$	$1.0 \pm 0.2$	$65.5\pm0.1$	100.67
91	1000/0.5	900	14	Liquid metal	$6.8 \pm 0.3$	$60.8 \pm 0.9$	$32.4 \pm 0.9$	100.35
				FeAs	$49.6 \pm 0.2$	$0.48\pm0.09$	$50.0 \pm 0.2$	99.85
				FeAs <sub>2</sub>	$32.3 \pm 0.7$	$2.1 \pm 0.8$	$65.6 \pm 0.2$	100.51
92	1000/0.5	700	12	Liquid metal	$1.0 \pm 0.2$	$90.8 \pm 0.2$	$8.1 \pm 0.1$	100.23
				FeAs	$49.3 \pm 0.1$	$0.44 \pm 0.17$	$50.3 \pm 0.2$	100.74
				FeAs <sub>2</sub>	$32.8 \pm 0.1$	$1.7 \pm 0.2$	$65.6 \pm 0.1$	100.87
(i) Bo	undary bety	veen Fe(A	As, Sb) a	and MeX <sub>2</sub> (Me	= Fe and X	= Sb and As	) primary pl	hase fields
93	1000/0.5	700	20	Liquid metal	$4.8 \pm 0.5$	$93.3 \pm 0.5$	$1.9 \pm 0.1$	100.28
				FeAs	$50.4 \pm 0.1$	$2.9 \pm 0.2$	$46.8 \pm 0.3$	100.71
				MeX <sub>2</sub>	$33.7 \pm 0.1$	$61.6 \pm 0.1$	$4.7 \pm 0.1$	99.78
94	1000/0.5	700	6	Liquid metal	$4.7 \pm 0.5$	$93.4 \pm 0.5$	$1.9 \pm 0.1$	100.15
				FeAs	$49.2 \pm 1.2$	$2.5 \pm 0.2$	$48.3 \pm 1.3$	100.30
				MeX <sub>2</sub>	$33.7 \pm 0.2$	$59.5 \pm 0.7$	$6.7 \pm 0.6$	100.35
(k) Su	b-solidus		1				<u> </u>	
95	1000/0.5	950	21	MeX	$53.5 \pm 0.1$	$5.1 \pm 0.1$	$41.4 \pm 0.1$	100.32
				FeAs	$49.8 \pm 0.2$	$0.84\pm0.07$	$49.3 \pm 0.2$	100.78
96	1000/0.5	900	24	Fe <sub>2</sub> As	$65.5 \pm 0.2$	$0.88 \pm 0.02$	$33.6 \pm 0.2$	100.14
				MeX	$59.4 \pm 0.8$	$4.6 \pm 0.5$	$36.0 \pm 0.3$	100.43
97	900/0.5	850	12	BCC-Fe	$91.0 \pm 0.0$	$0.76 \pm 0.01$	$8.3 \pm 0.0$	99.80
				MeX	$59.6 \pm 0.1$	$28.0 \pm 0.0$	$12.4 \pm 0.1$	100.26
98	1000/0.5	850	12	MeX	$60.9 \pm 0.8$	$6.1 \pm 0.9$	$33.0 \pm 0.0$	100.22
				Fe <sub>2</sub> As	$65.1 \pm 0.1$	$1.4 \pm 0.0$	$33.5 \pm 0.1$	100.17
99	1000/0.5	850	15	MeX	$60.2 \pm 0.3$	$19.2 \pm 0.2$	$20.5 \pm 0.2$	100.31
				Fe <sub>2</sub> As	$65.9 \pm 0.1$	$1.4 \pm 0.5$	$32.7 \pm 0.4$	100.06
100	900/0.5	800	5	BCC-Fe	$91.3 \pm 0.1$	$0.58 \pm 0.02$	$8.1 \pm 0.1$	100.06
				MeX	$59.3 \pm 0.1$	$28.3 \pm 0.1$	$12.4 \pm 0.0$	100.32
101	900/0.5	800	14	MeX	$57.4 \pm 0.3$	$10.2 \pm 0.1$	$32.4 \pm 0.3$	100.33
				Fe <sub>2</sub> As	$65.7 \pm 0.1$	$1.3 \pm 0.1$	$32.9 \pm 0.2$	100.20
102	900/0.5	800	17	MeX	$54.9 \pm 0.4$	$11.2 \pm 0.1$	$33.8 \pm 0.4$	99.95
				FeAs	$49.9\pm0.2$	$1.8 \pm 0.2$	$48.3\pm0.4$	100.82
103	1000/0.5	800	5	BCC-Fe	$90.5 \pm 0.5$	$0.93\pm0.39$	$8.6 \pm 0.1$	100.42
				MeX	$60.1 \pm 0.2$	$25.1 \pm 0.6$	$14.8\pm0.4$	100.23
				Fe <sub>2</sub> As	$68.7\pm0.5$	$3.0\pm0.1$	$28.3\pm0.4$	100.32
104	950/0.5	800	15	BCC-Fe	$90.6\pm0.3$	$0.70\pm0.12$	$8.6 \pm 0.2$	99.66
				MeX	$59.5 \pm 0.1$	$26.2\pm0.0$	$14.3\pm0.1$	99.67
				Fe <sub>2</sub> As	$65.8 \pm 0.1$	$2.8 \pm 0.1$	$31.5 \pm 0.1$	100.08
105	950/0.5	750	15	BCC-Fe	$91.5 \pm 0.1$	$0.49\pm0.02$	$8.0 \pm 0.1$	99.78
				MeX	$58.7 \pm 0.2$	$29.5\pm0.2$	$11.9\pm0.1$	100.12
				Fe <sub>2</sub> As	$65.9 \pm 0.1$	$3.2 \pm 0.1$	$30.9\pm0.1$	100.09
106	950/0.5	700	12	BCC-Fe	$92.0 \pm 0.1$	$0.45\pm0.04$	$7.5 \pm 0.0$	100.13
				MeX	$58.0\pm0.2$	$31.9\pm0.5$	$10.1\pm0.5$	100.28
				Fe <sub>2</sub> As	$66.5\pm0.8$	$2.8\pm0.2$	$30.7\pm0.7$	100.27
107	950/0.5	600	11.5	FeAs	$50.4\pm0.2$	$0.06\pm0.01$	$49.6\pm0.2$	100.33
				FeAs <sub>2</sub>	$33.6 \pm 0.2$	$0.88\pm0.24$	$65.5 \pm 0.3$	100.19
				As-Sb	$0.0 \pm 0.1$	$90.2 \pm 1.1$	$9.8 \pm 1.1$	99.67
				solution				
108	1000/0.5	600	10.5	FeAs	$50.1 \pm 0.1$	$0.60\pm0.52$	$49.3\pm0.6$	100.48
				As-Sb	$0.3\pm0.2$	$\overline{95.9\pm0.8}$	$3.8 \pm 0.7$	99.83
				solution				
109	900/0.5	600	38	FeAs	$49.2\pm0.4$	$1.7\pm0.7$	$49.1 \pm 0.4$	100.70
				MeX <sub>2</sub>	$33.6 \pm 0.2$	$60.2 \pm 0.7$	$6.3\pm0.7$	100.39
				As-Sb	$1.1 \pm 0.6$	$97.8 \pm 0.9$	$1.1 \pm 0.3$	99.86

				solution				
110	800/0.5	600	12	FeAs <sub>2</sub>	$33.5 \pm 0.3$	$0.21 \pm 0.26$	$66.3 \pm 0.5$	100.52
				As-Sb	$0.0 \pm 0.1$	$78.1 \pm 0.3$	$21.9\pm0.3$	99.77
				solution				
111	1000/0.5	550	37	FeAs	$50.6\pm0.2$	$1.1 \pm 0.2$	$48.3\pm0.3$	100.46
				As-Sb	$0.4 \pm 0.2$	$97.4 \pm 0.5$	$2.2 \pm 0.3$	99.90
				solution				
112	900/0.5	550	37	MeX <sub>2</sub>	$33.8\pm0.2$	$60.0\pm0.7$	$6.2\pm0.6$	100.33
				As-Sb	$0.9 \pm 0.4$	$98.0 \pm 0.7$	$1.1 \pm 0.3$	99.71
				solution				

Table S2 Measured composition of the phases (average values and standard deviation) in the Fe-As syster	n,
expressed in mol.% with SiO2 substrate of each phase equilibrated at fixed temperature and fixed first preheatin	ıg
at 600 °C for 1 h to all arsenic containing samples with or without second preheating.	

S	Preheat	Equili	bratio	Phasa	Normalize	ed mol. %	Unnormalized
no.	(°C/h)	T	t (h)	1 Hast	Fe	As	(₩1.70)
	C Faliquid	(°C)					
(I) BC		1500	3	Liquid metal	$97.2 \pm 0.2$	$28 \pm 0.2$	100.02
115	-	1500	5	BCC-Fe	$99.10 \pm$	$2.0 \pm 0.2$	99.75
				Bee-re	0.02	0.01 ± 0.02	99.15
114	-	1450	5.25	Liquid metal	$93.9\pm0.1$	$6.1 \pm 0.1$	100.48
				BCC-Fe	$98.1\pm0.0$	$1.9 \pm 0.0$	99.71
115	-	1400	4.75	Liquid metal	$91.1 \pm 0.1$	$8.9 \pm 0.1$	100.24
				BCC-Fe	$97.2 \pm 0.1$	$2.8 \pm 0.1$	99.76
116	-	1350	13.5	Liquid metal	$88.8\pm0.2$	$11.2 \pm 0.2$	100.33
				BCC-Fe	$96.4\pm0.0$	$3.6 \pm 0.0$	99.87
117	-	1300	11.5	Liquid metal	$86.5\pm0.4$	$13.5 \pm 0.4$	100.34
				BCC-Fe	$95.5\pm0.0$	$4.5\pm0.0$	99.93
118	-	1250	25.5	Liquid metal	$84.1\pm0.6$	$15.9\pm0.6$	100.50
				BCC-Fe	$94.8\pm0.2$	$5.2 \pm 0.2$	99.79
119	-	1200	26.5	Liquid metal	$81.7\pm0.4$	$18.3\pm0.4$	100.31
				BCC-Fe	$93.9\pm0.2$	$6.1 \pm 0.2$	99.92
120	-	1150	18.7	Liquid metal	$80.8\pm0.6$	$19.2 \pm 0.6$	100.13
			5	BCC-Fe	$93.3\pm0.1$	$6.7 \pm 0.1$	99.84
121	-	1100	5.75	Liquid metal	$79.1\pm0.3$	$20.9\pm0.3$	100.01
				BCC-Fe	$92.8\pm0.1$	$7.2 \pm 0.1$	100.05
122	-	1050	5.75	Liquid metal	$77.7 \pm 0.4$	$22.3 \pm 0.4$	100.32
				BCC-Fe	$92.3 \pm 0.1$	$7.7 \pm 0.1$	100.12
123	-	1000	25.5	Liquid metal	$76.7\pm0.5$	$23.3\pm0.5$	100.11
				BCC-Fe	$91.6 \pm 0.1$	$8.4 \pm 0.1$	100.03
124	1000/0.5	950	17	Liquid metal	$75.8\pm0.3$	$24.2 \pm 0.3$	100.26
				BCC-Fe	$91.1 \pm 0.1$	$8.9 \pm 0.1$	99.90
125	1000/0.5	900	15.7	Liquid metal	$75.1 \pm 0.2$	$24.9\pm0.2$	100.24
			5	BCC-Fe	$90.7 \pm 0.1$	$9.3 \pm 0.1$	100.07
126	1000/0.5	850	47.2	Liquid metal	$74.3 \pm 0.2$	$25.7 \pm 0.2$	100.34
			5	BCC-Fe	$90.3 \pm 0.1$	$9.7 \pm 0.1$	100.13
(m) Fe	e <sub>2</sub> As liquidu	S		[ ]		1	
127	1000/0.5	900	24.5	Liquid metal	$69.5 \pm 0.3$	$30.5 \pm 0.2$	100.20
				Fe <sub>2</sub> As	$66.2 \pm 0.2$	$33.8 \pm 0.2$	100.41
128	1000/0.5	850	40	Liquid metal	$74.0 \pm 0.2$	$26.0 \pm 0.0$	99.90
				Fe <sub>2</sub> As	$66.4 \pm 0.0$	$33.6 \pm 0.0$	100.13
129	1000/0.5	850	7.25	Liquid metal	$74.0 \pm 0.2$	$26.0 \pm 0.0$	99.90
()~~				Fe <sub>2</sub> As	$66.3 \pm 0.2$	$33.7 \pm 0.0$	99.98
(n) Su	b-solidus	1000		<b></b>	40.0.0.4		100.10
130	-	1000	72.7	FeAs	$49.8 \pm 0.1$	$50.2 \pm 0.1$	100.19
101	1050/0.2	0.000	5	MeX "Fe <sub>3</sub> As <sub>2</sub> "	$55.3 \pm 0.1$	$44./\pm0.1$	100.45
131	1050/0.2	980	/1.7	FeAs	$49.9 \pm 0.1$	$50.1 \pm 0.0$	100.66
100	5	0.00	5	MeX "Fe <sub>3</sub> As <sub>2</sub> "	$55.8 \pm 0.2$	$44.2 \pm 0.1$	100.49
132	1050/0.2	960	84.7	FeAs	$50.0 \pm 0.1$	$50.0 \pm 0.1$	100.48
	5		5	MeX "Fe <sub>3</sub> As <sub>2</sub> "	$56.7 \pm 0.1$	$43.3 \pm 0.1$	100.12
133	1050/0.2	940	70.7	FeAs	$50.1 \pm 0.0$	$49.9 \pm 0.2$	100.66

	5		5	MeX "Fe <sub>3</sub> As <sub>2</sub> "	$57.1 \pm 0.1$	$42.9 \pm 0.1$	100.07
134	1050/0.2	920	72	FeAs	$49.8\pm0.1$	$50.2 \pm 0.2$	100.84
	5			MeX "Fe <sub>3</sub> As <sub>2</sub> "	$57.1 \pm 0.1$	$42.9 \pm 0.1$	100.10
135	1000/0.5	900	75	Fe <sub>2</sub> As	$66.4\pm0.2$	$33.6 \pm 0.2$	100.26
				MeX "Fe <sub>3</sub> As <sub>2</sub> "	$59.7\pm0.1$	$40.3 \pm 0.1$	100.54
136	1050/0.2	900	71.5	FeAs	$49.8\pm0.2$	$50.2 \pm 0.1$	100.86
	5			MeX "Fe <sub>3</sub> As <sub>2</sub> "	$57.5\pm0.1$	$42.5 \pm 0.1$	100.19
137	1000/0.5	880	71.5	Fe <sub>2</sub> As	$66.6\pm0.2$	$33.4 \pm 0.1$	100.14
				MeX "Fe <sub>3</sub> As <sub>2</sub> "	$59.3\pm0.1$	$40.7 \pm 0.1$	100.12
138	1050/0.2	880	71	FeAs	$50.3\pm0.1$	$49.7\pm0.1$	100.07
	5			MeX "Fe <sub>3</sub> As <sub>2</sub> "	$58.1\pm0.1$	$41.9\pm0.1$	100.04
139	1000/0.5	860	85.5	Fe <sub>2</sub> As	$66.4\pm0.1$	$33.6 \pm 0.1$	100.28
				MeX "Fe <sub>3</sub> As <sub>2</sub> "	$59.2\pm0.1$	$40.8\pm0.1$	100.37
140	1050/0.2	860	84	FeAs	$49.9\pm0.1$	$50.1 \pm 0.1$	100.20
	5			MeX "Fe <sub>3</sub> As <sub>2</sub> "	$58.4\pm0.1$	$41.6 \pm 0.1$	100.50
141	1000/0.5	840	94.5	Fe <sub>2</sub> As	$66.3\pm0.1$	$33.7 \pm 0.1$	100.38
				FeAs	$49.9\pm0.1$	$50.1\pm0.0$	100.75
142	1050/0.2	840	70.5	Fe <sub>2</sub> As	$66.4\pm0.1$	$33.6 \pm 0.1$	100.03
	5			FeAs	$49.9\pm0.1$	$50.1\pm0.0$	101.00
143	1000/0.5	820	72.7	Fe <sub>2</sub> As	$66.3\pm0.1$	$33.7\pm0.0$	100.12
			5	FeAs	$50.2\pm0.0$	$49.8\pm0.0$	100.12
144	1050/0.2	820	74.5	Fe <sub>2</sub> As	$66.6\pm0.1$	$33.4\pm0.0$	100.16
	5			FeAs	$50.0\pm0.0$	$50.0\pm0.0$	100.15
145	1000/0.5	700	86	BCC-Fe	$9\overline{1.8\pm0.1}$	$8.2 \pm 0.0$	100.19
				Fe <sub>2</sub> As	$66.2 \pm 0.1$	$33.8\pm0.0$	100.30
146	1000/0.5	600	85	BCC-Fe	$9\overline{2.3 \pm 0.4}$	$7.7 \pm 0.0$	99.62
				Fe <sub>2</sub> As	$66.1 \pm 0.2$	$33.9\pm0.0$	100.27

Table S3 Measured composition of the p	bhases (average values	and standard deviatio	n) in the Fe-Sb system,
expressed in mol.% with SiO <sub>2</sub> substrate of	each phase equilibrated	at fixed temperature wi	th or without preheating.

	Preheat	eheat Equilibratio		Phase	Normal	ized mol.	Unnormalized	
<b>S.</b>	2	n	1			<b>%</b>	(wt.%)	
no.	(°C/h)	T	t (h)		Fe	Sb		
		(°C)						
(0) BC	C-Fe liquid	us	_	T · · 1		10.0	100.47	
147	-	1400	5	Liquid	89.8 ±	$10.2 \pm$	100.47	
				metal	0.4	0.4	00 <b>50</b>	
				BCC-Fe	98.3 ±	$1.7 \pm 0.0$	99.72	
					0.0			
148	-	1350	5.25	Liquid	86.0 ±	$14.0 \pm$	100.40	
				metal	0.6	0.6		
				BCC-Fe	97.8 ±	$2.2 \pm 0.0$	99.98	
					0.0			
149	-	1300	3.5	Liquid	82.1 ±	17.9 ±	100.50	
				metal	1.2	1.2		
				BCC-Fe	97.3 ±	$2.7 \pm 0.0$	99.98	
					0.0			
150	-	1250	6.25	Liquid	$78.7 \pm$	21.3 ±	100.31	
				metal	0.8	0.8		
				BCC-Fe	96.9±	$3.1 \pm 0.1$	100.11	
					0.1			
151	-	1200	5.5	Liquid	74.8 ±	25.2 ±	100.26	
				metal	0.8	0.8		
				BCC-Fe	96.4 ±	$3.6 \pm 0.0$	100.17	
					0.0			
152	_	1150	6.75	Liquid	72.1 ±	27.9 ±	100.36	
_				metal	1.0	1.0		
				BCC-Fe	96.1±	$3.9 \pm 0.0$	99.77	
					0.0			
153	_	1100	3	Liquid	70.3 ±	29.7 ±	100.28	
				metal	0.8	0.8		
				BCC-Fe	95.6 ±	$4.4 \pm 0.0$	100.21	
				20010	0.0		1000-1	
154	_	1050	6	Liquid	68.3 +	31.7+	100.32	
10.		1000	Ũ	metal	0.5	0.5	100002	
				BCC-Fe	95.1+	49+00	99 70	
				Decire	0.0	1.9 ± 0.0	<i>уу</i> .то	
(p) Me	• eX-Fe1Sh	iquidus	1			1		
155	-	1020	28.7	Liquid	64.0 ±	36.0±	100.33	
			5	metal	0.4	0.4	100.00	
				MeX	59.2 +	40.8+	100.16	
				1.10/1	0.2	0.2	100110	
156	-	1000	4.75	Liquid	43.8+	56.2 +	100.18	
	1	1000		2.14.4			100.10	

				metal	0.7	0.7	
				MeX	55.1 ±	44.9 ±	100.30
					0.1	0.1	
157	_	975	7.5	Liquid	38.9+	61.1+	100 44
107		10	/.5	metal	1.3	1.3	100.11
				MeX	54.8 +	$45.2 \pm$	100.21
				IVIC/X	0.2	$13.2 \pm 0.2$	100.21
158	_	950	26	Liquid	34.1 +	65.9 +	99.88
150	-	950	20	metal	1 2	12	99.00
				MaX	542	1.2	00.02
				IVIEA	$54.5 \pm$	$43.7 \pm$	99.95
150	1000/0.5	025	145	т :: 1		0.1	00.04
159	1000/0.5	925	14.5	Liquid	30.9 ±	69.1±	99.94
				metal	1.0	1.0	100.00
				MeX	53.7±	$46.3 \pm$	100.29
					0.1	0.1	
160	1000/0.5	900	20	Liquid	$27.2 \pm$	$72.8 \pm$	100.42
				metal	1.4	1.4	
				MeX	53.6 ±	$46.4 \pm$	100.11
					0.1	0.1	
161	1000/0.5	850	14.5	Liquid	21.6 ±	$78.4 \pm$	99.83
				metal	1.6	1.6	
				MeX	52.9 ±	47.1 ±	100.06
					0.2	0.2	
162	1000/0.5	800	15	Liquid	16.2 ±	83.8 ±	99.83
				metal	0.8	0.8	
				MeX	52.7 ±	47.3 ±	99.72
					0.2	0.2	
163	1000/0.5	750	19.7	Liquid	11.7+	88.3 +	99.67
100	1000,000	, 0 0	5	metal	1.3	1.3	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
			Ū	MeX	52.0+	48.0 +	100.26
				1,1011	0.2	0.2	100.20
(a) Me	$X_{a}$ (Me = F	e and X	= Sb) li	auidus	0.2	0.2	
164	1000/0.5		24.7	Liquid	$53 \pm 0.7$	047+	00 77
104	1000/0.5	700	24.7	metal	$5.5 \pm 0.7$	0.0	<i>уу</i> .//
			5	M-X	227		100.42
				Mex <sub>2</sub>	$33.7 \pm$	$00.3 \pm$	100.42
1.65	1000/0.5	(50	25	T · · 1	0.2	0.0	00.00
165	1000/0.5	650	25	Liquid	$2.5 \pm 0.2$	97.5 ±	99.90
				metal	22.0.1	0.0	100.07
				$MeX_2$	33.8±	$66.2 \pm$	100.36
					0.1	0.0	
(r) Sub	o-solidus			L	1		
166	1050/0.2	900	52	BCC-Fe	95.4 ±	$4.6 \pm 0.0$	99.97
	5				0.0		
				MeX	58.4 ±	41.6 ±	99.52
					0.1	0.0	
167	1050/0.2	800	51	BCC-Fe	96.1 ±	$3.9\pm0.0$	99.96
	5				0.0		
				MeX	56.9 ±	43.1 ±	99.85
					0.2	0.0	

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