

Supporting Information

Efficient One-Step SO₂ Capture from Industrial Flue Gas via a Scalable Zr-Based Metal-Organic Framework

Si-Chao Liu^a, Li Xu^a, Li-Ping Zhang^a, Chen-Xu Li^b, You-Xiang Lu^{b*}, Yi-Tao Li^a, Jian Wang^{b*}, Shao-Min Wang^{a*}, Qing-Yuan Yang^{a*}

^aState Key Laboratory of Fluorine & Nitrogen Chemicals, School of Chemical Engineering and Technology, Xi'an Jiaotong University, Xi'an, Shaanxi 710049

^bAnhui Provincial Key Laboratory of Aerosol Analysis, Modulation and Biological Effect/China Tobacco Anhui Industrial Co., Ltd.

E-mail: 574567981@qq.com; wangj86@mail.ustc.edu.cn; shaominwang@xjtu.edu.cn; qingyuan.yang@xjtu.edu.cn

1. Supplemental Experiment Procedures

Breakthrough experiments:

The breakthrough experiments were conducted on a dynamic gas breakthrough setup. The sample packaging material is a U-shaped glass tube with an inner size of $\varphi = 4 \times 160$ mm, and quartz cotton is filled at both ends. Then the samples in U-shaped glass tube were activated by helium flow at 150°C (30 mL/min) for at least 2 h. The flow rate of the mixed gas is controlled by a mass flow controller (MFC). Outlet gas from the column was continuously monitored using gas chromatography (GC 9790 II) equipped with a thermal conductivity detector (TCD). The n-butane and iso-butane gas flows were both controlled at 0.2 mL/min. In cyclic breakthrough experiments, the sample regenerated by purged with helium gas at 30 mL/min for 3 h at 120°C between each breakthrough. The gas adsorption capacity in column can be determined by Eqn (1):

$$q_i = \frac{v \times V\%}{22.4} \times \int_{t_1}^{t_2} (c_0 - c_i) dt = \frac{v \times V\%}{22.4} \times S \quad (1)$$

In equation (1), q_i (mmol/g) is the adsorption capacity of component i , v is the flow rate of the gas mixture, $V\%$ is the molar fraction of SO₂, CO₂, or N₂. c_0 and c_i are the outlet and inlet fraction of gas component i , respectively.

Calculation of isosteric enthalpy of adsorption (Q_{st}):

The Q_{st} for SO₂ and CO₂ were fitted by the virial equation (Eqn (2)) according to the isotherms at different temperatures. The fitting parameters were then used to calculate the Q_{st} using Eqn (3)¹.

$$y = \ln(x) + \frac{1}{T} (a_0 + a_1x + a_2x^2 + a_3x^3 + a_4x^4 + a_5x^5) + (b_0 + b_1x + b_2x^2 + b_3x^3) \quad (2)$$

$$Q_{st} = -8.314 \times (a_0 + a_1q + a_2q^2 + a_3q^3 + a_4q^4 + a_5q^5) \quad (3)$$

Where a_i and b_i are virial coefficients required to describe the isotherms in detail. q represents the adsorption capacity (mmol/g) at different times at a constant temperature.

Calculation of selectivity via IAST:

Single-component gas equilibrium adsorption isotherms were fitted with the dual-site

Langmuir-Freundlich model, given by the following equation:

$$y = \frac{a_1 \times b_1 \times x^{c_1}}{1 + b_1 \times x^{c_1}} + \frac{a_2 \times b_2 \times x^{c_2}}{1 + b_2 \times x^{c_2}}$$

(5)

Where y is the gas adsorption capacity (mmol/g), a is the saturated adsorption capacity of the gas (mmol/g), and b is the Langmuir parameter in kPa^{-1} , x is the gas pressure in kPa , c is the dimensionless Freundlich parameter, and subscripts 1 and 2 correspond to two different identities. The fitting parameters of the Langmuir-Freundlich model were determined using a least-squares.

The adsorption selectivity of the binary mixture was predicted by using the Ideal Adsorption Solution Theory (IAST)². The adsorption selectivity can be determined by

Eqn (6):

$$S_{ads} = \frac{X_1/X_2}{Y_1/Y_2} \quad (6)$$

Where S is the selectivity of component 1 relative to 2. X_1 and X_2 are the molar fractions of components A and B in the adsorption phase, respectively. Y_A and Y_B are molar fractions of components A and B in the gas phase, respectively.

Computational details:

DFT calculations were carried out using Material Studio package. For the Grand canonical Monte Carlo (GCMC) simulations³, the guest molecules SO_2 , CO_2 and N_2

were geometrically optimized using Forcite code⁴ and the electrostatic potential (ESP) charges were applied to the guest molecules. The crystal structure of the MOF-801(Zr) was optimized with Forcite code, and the optimization results matched well with the crystal structures. The gas molecules and MOF skeleton were both treated as rigid bodies. The gas-framework interactions were described by the standard universal force field (UFF)⁵. The density distribution of SO₂, CO₂ and N₂ were calculated by using the fix pressure task in Sorption module and Metropolis method. For each state point, the system was equilibrated for 1×10⁶ steps, and then the ultimate data were collected for another 1×10⁷ steps. The locate task simulated the beneficial adsorption sites with a single guest molecule. All CIF files were processed to remove solvents and guest molecules before computation.

Supplemental Figures and Tables

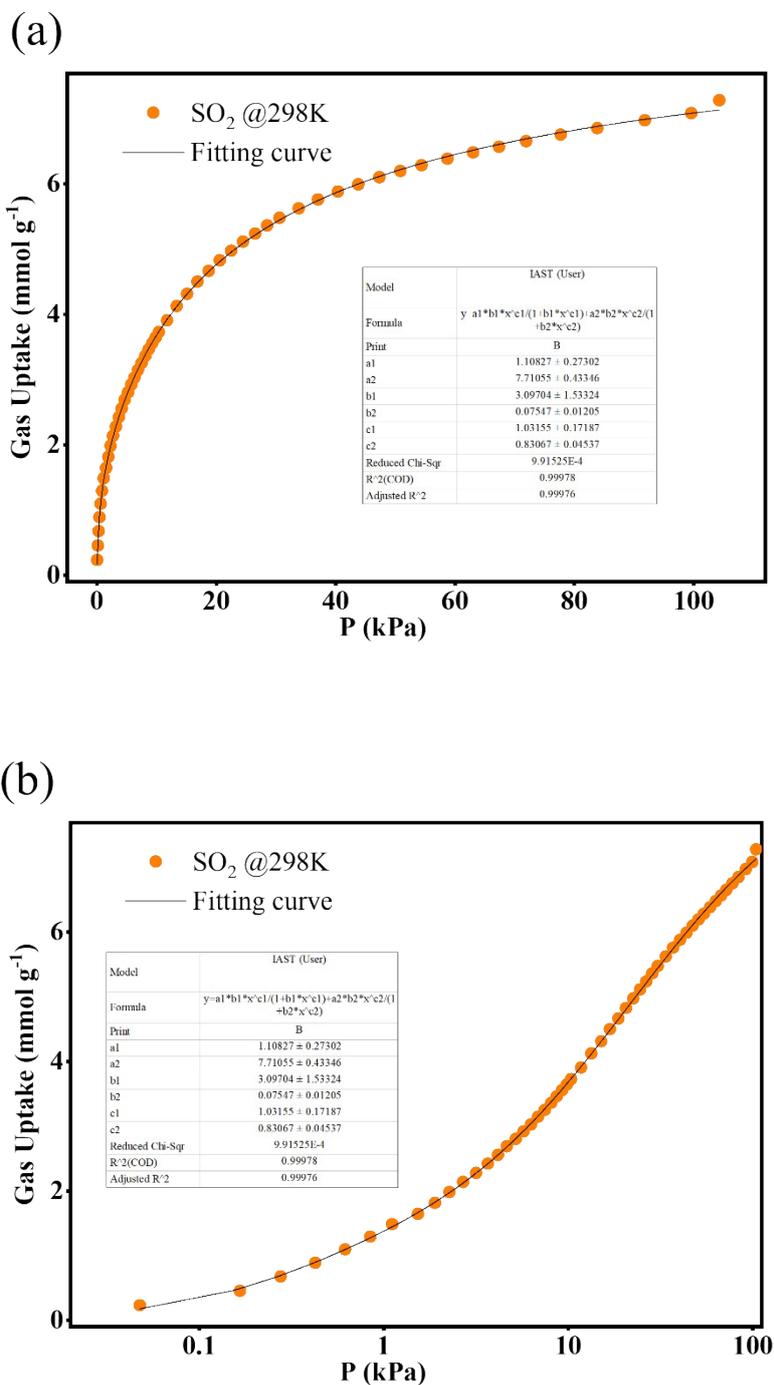
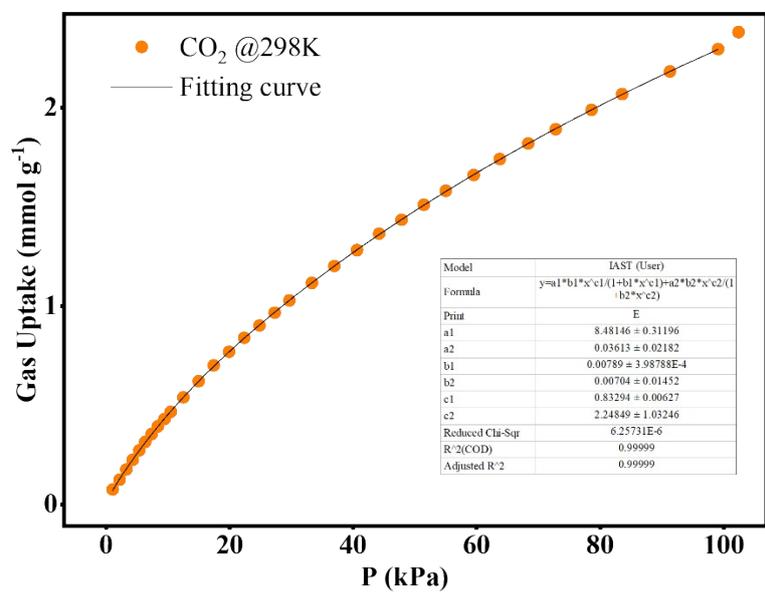


Figure S1. Dual-site Langmuir-Freundlich model for SO₂ adsorption isotherm on MOF-801(Zr) at 298 K. (a) Linear-scale plot (b) Log plot.

(a)



(b)

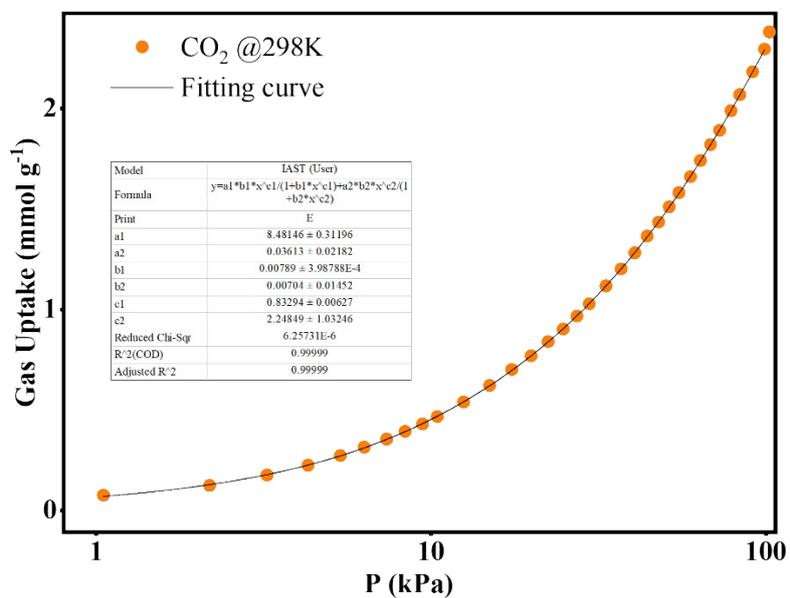


Figure S2. Dual-site Langmuir-Freundlich model for CO₂ adsorption isotherm on MOF-801(Zr) at 298 K. (a) Linear-scale plot (b) Log plot.

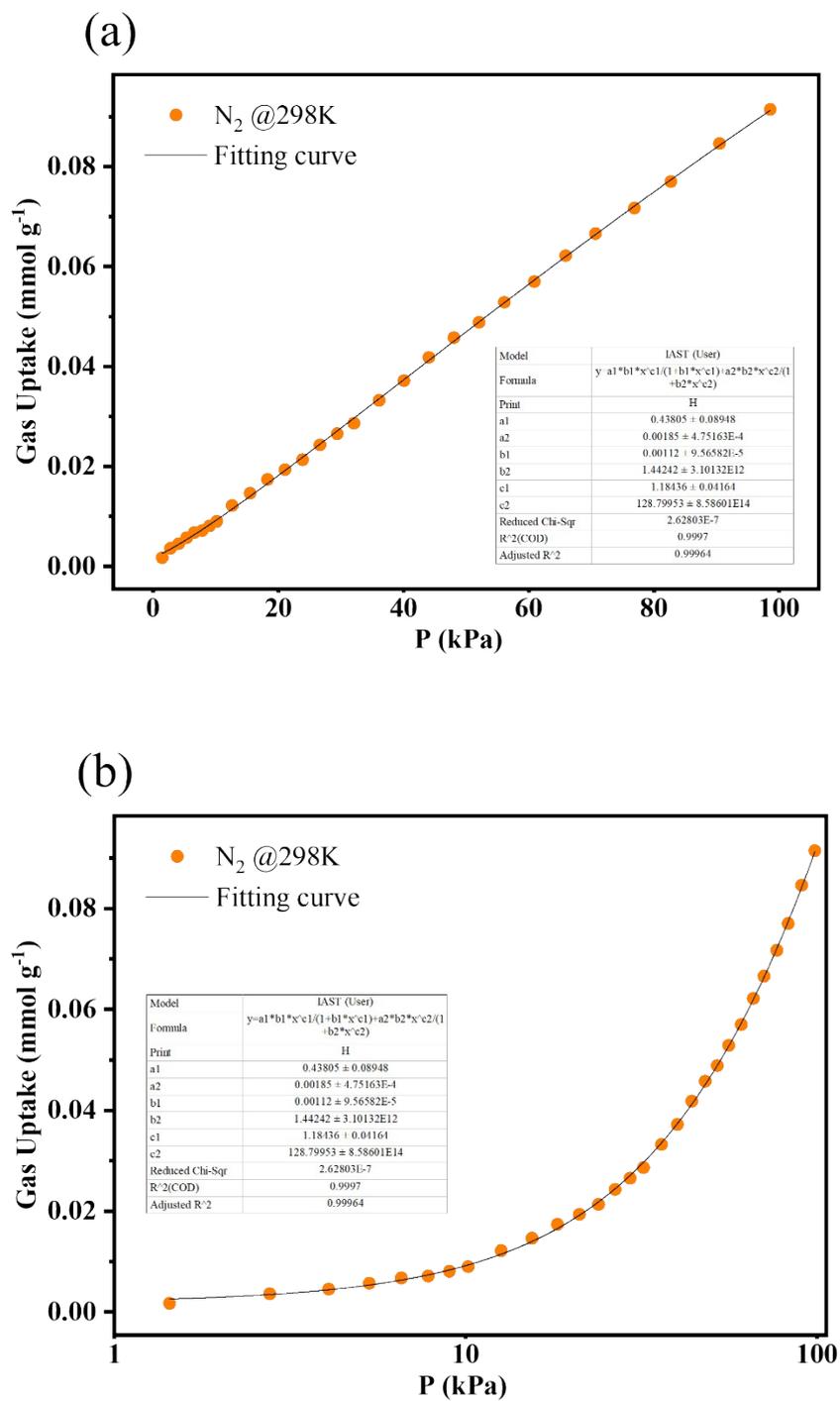


Figure S3. Dual-site Langmuir-Freundlich model for N₂ adsorption isotherm on MOF-801(Zr) at 298 K. (a) Linear-scale plot (b) Log plot.

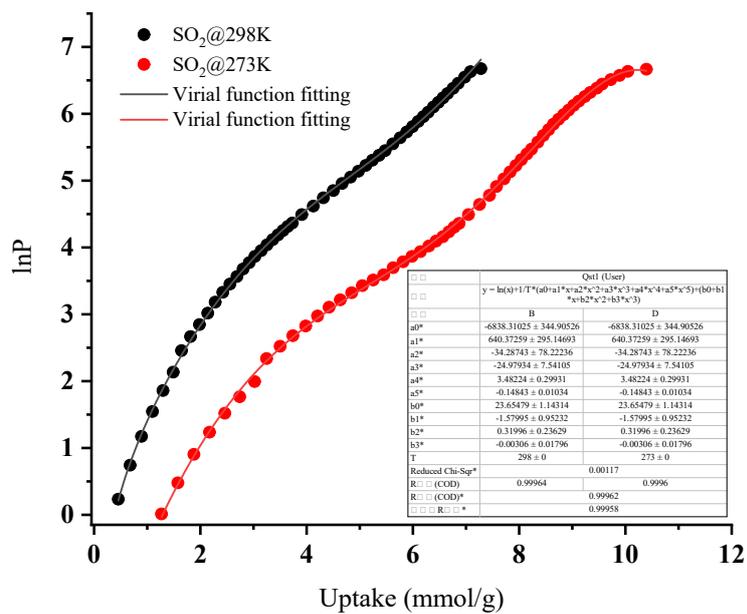


Figure S4. Virial fits for SO₂ on different temperature adsorption isotherms of MOF-801(Zr).

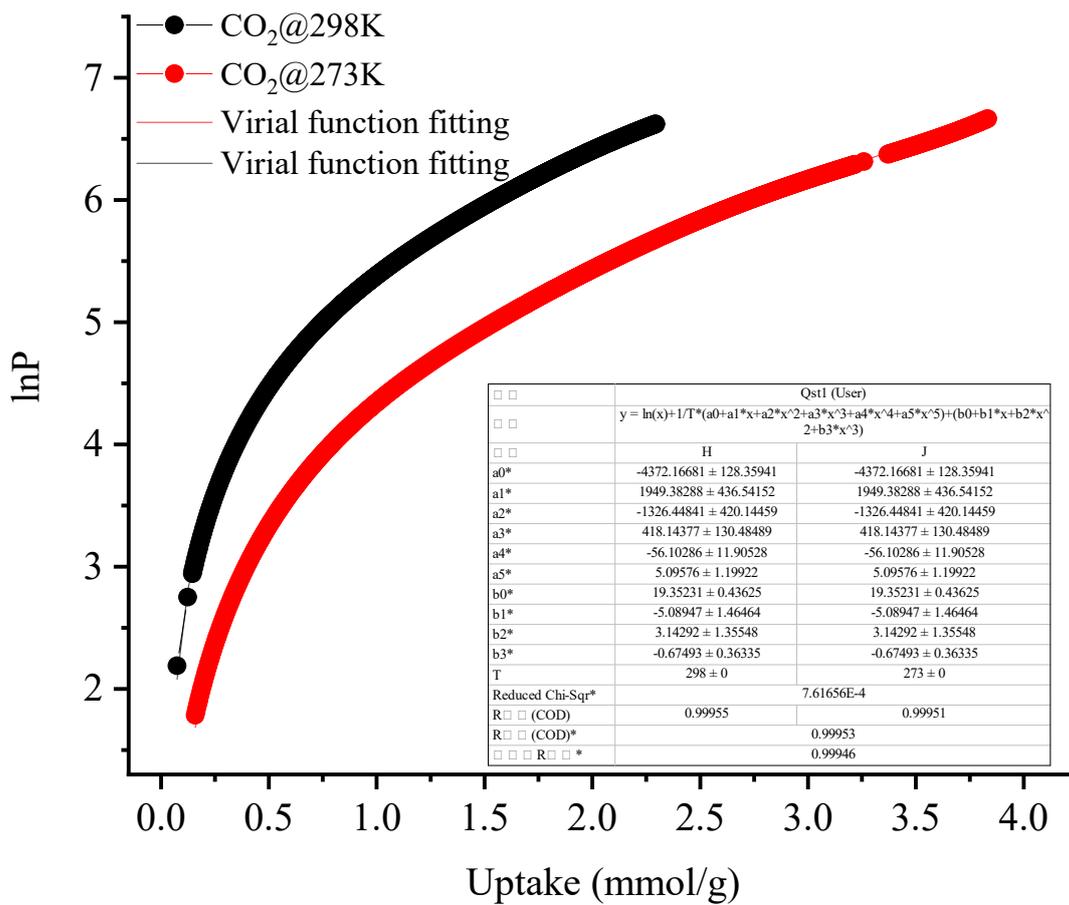


Figure S5. Virial fits for CO₂ on different temperature adsorption isotherms of MOF-801(Zr).

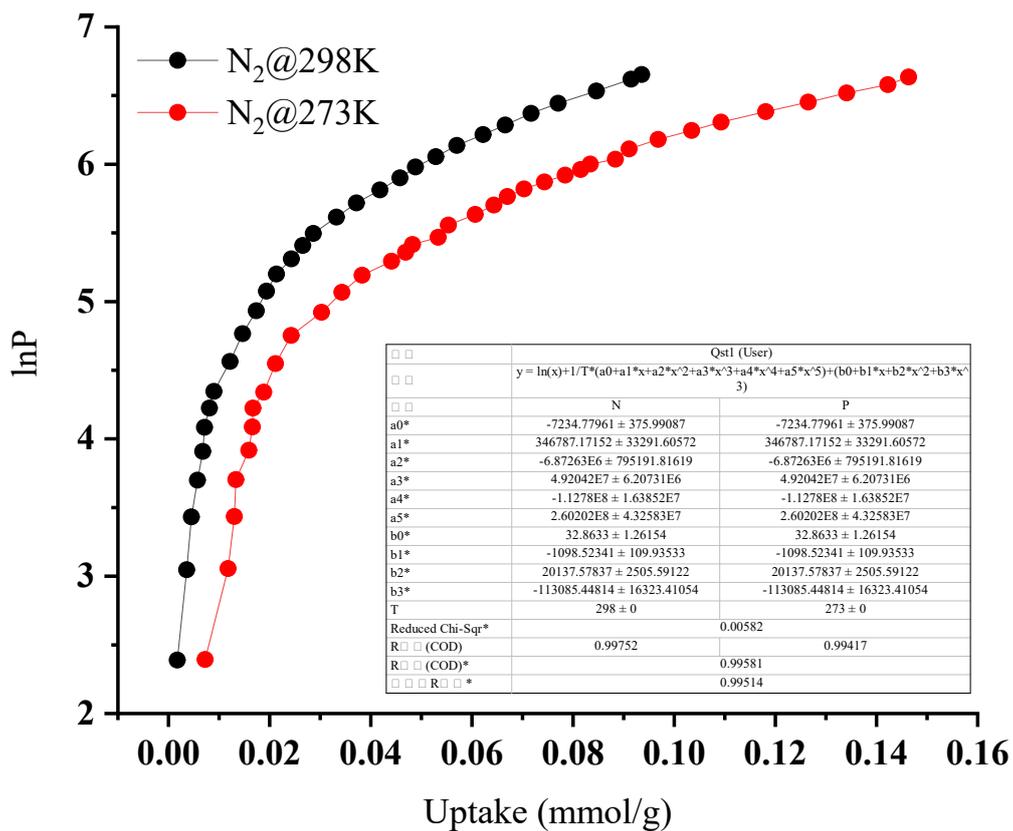


Figure S6. Virial fits for N₂ on different temperature adsorption isotherms of MOF-801(Zr).

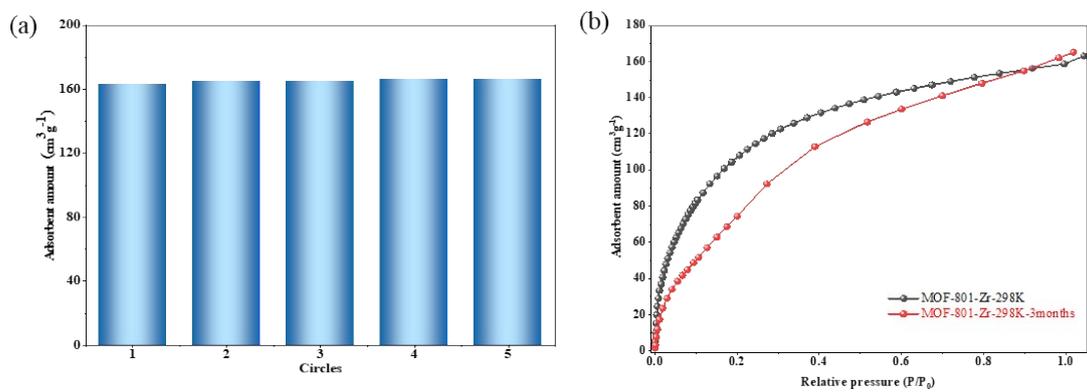


Figure S7. (a) The SO₂ adsorption performance in five-cycle testing (298 K). (b) Performance comparison of MOF-801(Zr) before and after three months of storage.

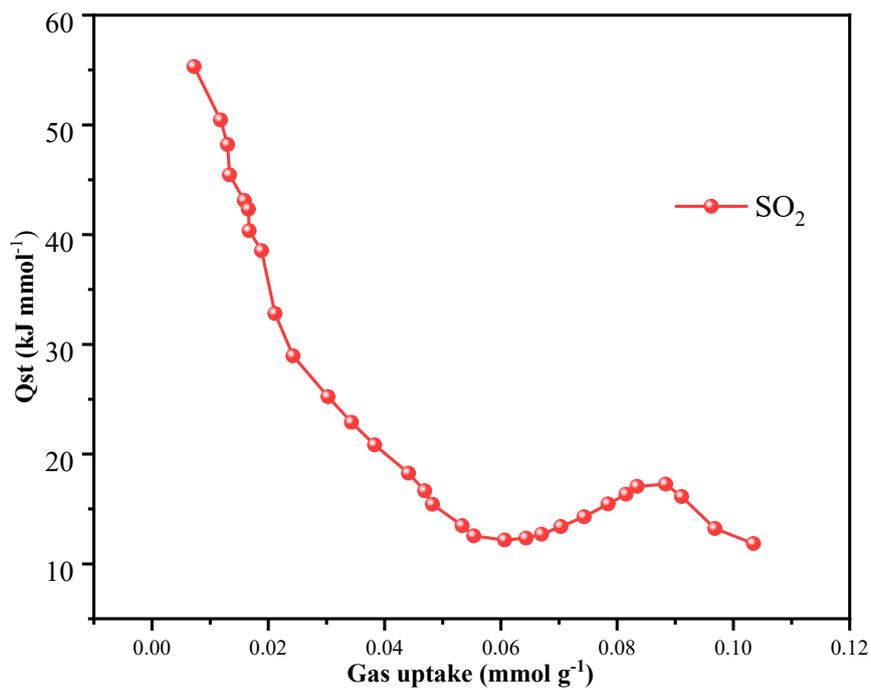


Figure S8. The Q_{st} of adsorption for N_2 for MOF-801(Zr).

For N_2 , the Q_{st} value reported in the main text refers to the heat of adsorption at 1 bar.

Given the linear nature and low uptake of the N_2 isotherms, the full Q_{st} curve for N_2 is omitted to maintain focus on the SO_2 capture performance.

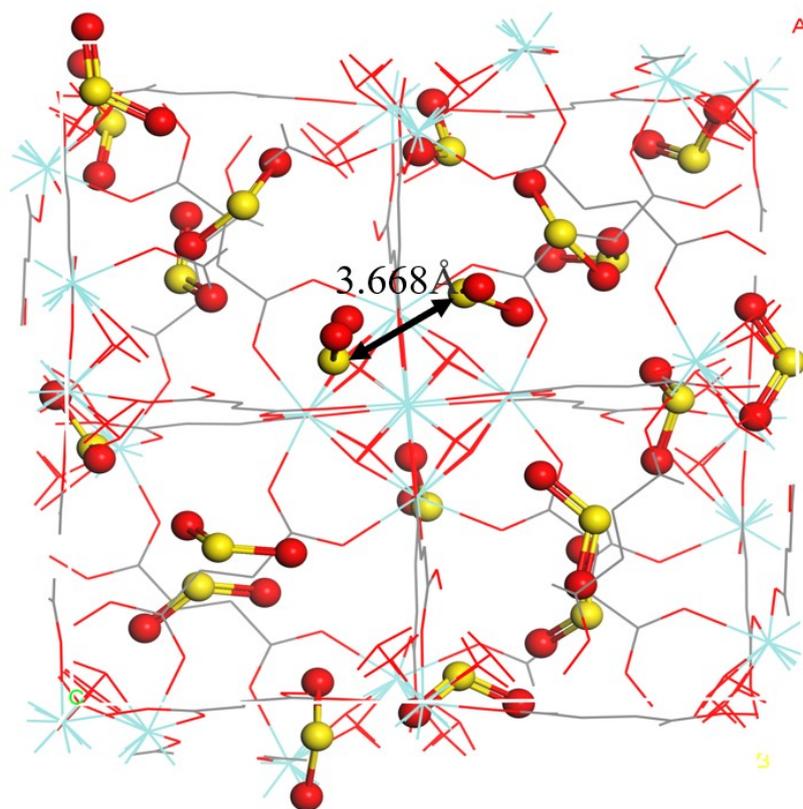


Figure S9. The GCMC simulation snapshots and the analysis of the intermolecular distances.

Table S1. Comparison of the uptake capacity of various adsorbents for SO₂ separation at 298 K.

Adsorbent	SO ₂ uptake (mmol/g)	IAST Selectivity (SO ₂ /CO ₂ , 10/90)	IAST Selectivity (SO ₂ /N ₂ , 1/99)	Ref.
MOF-801(Zr)	7.28	35.8	86368	This work
MFM-300(In)	8.28	50	2700	6
NOTT-300	8.1	—	6522	7
Zr-bptc	7.8	600	18000	8
UIO-66-Cu	8.2	54	3100	9
SIFSIX-1-Cu	9.51	70.7	3145.7	10
Mg-gallate	7.61	321	>1 × 10 ⁴	11
HBU-23	4.57	58.9	2333.5	12
CPL-1	2.29	8.7	368	13
ZU-801	3.48	145	>1 × 10 ⁴	14
G808-N-10	15.7	83	2915	15
FJI-H14	9.91	47	6857 (10/90)	16
DMOF-ADC	6.51	75	—	17
NiNi-PYZ-NH ₂	8.39	54.8(15/85)	—	18
DUT-67	9.3	37	20437	19
PCN-250(Fe ₂ Zn)	11.6	50	>1 × 10 ⁴	20
NanoCB ₆ -H	7.17	120	1720	21
ELM-12	3.3	30	871	22

Table S2. Crystallographic data and structure refinements for MOF-801(Zr).

MOF-801(Zr)	
Formula	C ₂₄ H ₁₂ O ₃₂ Zr ₆
F.w.	1359.66
T (K)	363.15
Space group	<i>Pn-3</i>
<i>a</i> (Å)	17.8348(17)
<i>b</i> (Å)	17.8348(17)
<i>c</i> (Å)	17.8348(17)
α (°)	90
β (°)	90
γ (°)	90
V (Å ³)	5672.9(16)
Z	4
$\rho_{\text{calc}}/\text{mg mm}^{-3}$	1.592
<i>m</i> (mm ⁻¹)	1.450
R1 (>2 σ /all date)	0.0619/0.1002
wR2 (>2 σ /all date)	0.1553/0.1733
Largest diff. peak/hole / e Å ⁻³	1.45/-0.77

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