

## Breaking the Performance Trade-offs in Ammonia Synthesis via Spontaneous Proton Supply

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## Methods

### Density functional theory (DFT) calculations

Spin-polarized DFT calculations are performed with the Vienna ab initio simulation package (VASP) to evaluate Gibbs free energies.<sup>1</sup> Ion-electron interactions are treated with the projector-augmented plane-wave<sup>2</sup> and exchange-correlation interactions are described by the Perdew-Burke-Ernzerhof functional within the generalized gradient approximation.<sup>3</sup> Following previous reports, we consider  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  (110) surface with four transition metal atomic layers (bottom two layers fixed) as the calculated model, and  $\text{Co}_{0.8}\text{Fe}_{0.2}(\text{OH})_2$  (001) and (100) surfaces with four and two transition metal atomic layers (bottom two and one layers fixed, respectively) as the calculated model, respectively.<sup>4</sup> The slabs are separated by a vacuum space of at least 15 Å along the z axis and a  $(3 \times 3 \times 1)$  Monkhorst–Pack k-point grids are used. Grimme's D3 method is adopted to account for van der Waals (vdW) interactions.<sup>5</sup> The cut-off energy is set as 550 eV, and all systems are optimized until energy and force are less than  $10^{-5}$  eV and 0.01 eV/Å. The computational results are carried out with VASPKIT.<sup>6</sup>

The Gibbs free energy of each elemental step ( $\Delta G$ ) of the  $\text{NO}_3\text{RR}$  is adopted following the works of Nørskov et al.<sup>7,8</sup>

$$\Delta G = \Delta E + \Delta E_{\text{ZPE}} - T\Delta S - eU + 0.059 \times \text{pH}$$

where  $\Delta E$  is the changed energy,  $\Delta E_{\text{ZPE}}$  and  $\Delta S$  are the change of zero-point vibrational energy and the change of entropy, respectively, which can be obtained by the vibrational frequency of the optimized structures. T is the temperature and set to 298.15 K, e and U are the transferred charge and the electrode potential, respectively. The pH is set as 14 in accordance with the experimental environments.

**Constant Potential Method.** Constant potential method is employed to simulate the applied potential effect on the  $\text{NO}_3\text{RR}$  potential-determining step on A- $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$ .<sup>9</sup> The aqueous environment is modeled as a continuum dielectric by the VASPsol code.<sup>10</sup> Charges ranging from  $-1.5$  e to  $+1.5$  e is added in steps of 0.5 e for each system to clarify the applied potential function. The potential-dependent energy can be calculated as<sup>11</sup>

$$U_q = -4.6 - \varphi_q / eV$$

where 4.6 V is the absolute potential relative to the SHE benchmarked in the VASPsol.<sup>12</sup>

The energy varies with the electrode potential as a quadratic function,

$$E(U_q) = -\frac{1}{2}C(U_q - U_0)^2 + E_0$$

where C is the capacitance of the system,  $U_0$  is the potential of zero charges (PZC), and  $E_0$  is the energy at the zero charges.

### Material synthesis

$\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  spinel oxide powders are synthesized by traditional sol-gel methods. Taking the preparation of 10 mmol  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  as an example, 10 mmol  $\text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  (Nickel(II) nitrate hexahydrate, crystals or chunks, Sigma Aldrich), 2.5 mmol  $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$  (Iron(III) nitrate nonahydrate, ACS reagent,  $\geq 98\%$ , Sigma-Aldrich) and 17.5 mmol  $\text{Cr}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$  (Chromium(III) nitrate nonahydrate, 99%, Sigma-Aldrich) are dissolved using minimum deionized water (DI water) with magnetic stirring in a 1-liter glassy beaker. Then, both 30 mmol EDTA (Ethylenediaminetetraacetic acid, BioUltra, anhydrous,  $\geq 99\%$  (titration), Sigma-Aldrich) and 60 mmol  $\text{C}_6\text{H}_8\text{O}_7 \cdot \text{H}_2\text{O}$  (Citric acid monohydrate, ACS reagent,  $\geq 99.0\%$ ) are added into solutions subsequently.

The pH is adjusted with  $\text{NH}_4\text{OH}$  (Ammonium hydroxide solution, Ammonium hydroxide solution, puriss., 25–30%  $\text{NH}_3$  basis, Sigma-Aldrich) under stirring until a clear solution is obtained. The solution is heated at 200 °C until a gel is formed, followed by drying at 250 °C overnight. The dried precursor is ground to a powder and calcined in air at 1000 °C for 10 h (ramp rate of 5 °C  $\text{min}^{-1}$ ). After furnace cooling, the product is ground to yield the final powder.

### Materials characterization

Phase identification of  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  is performed using X-ray powder diffraction (Bruker D8 Advance,  $\text{Cu K}\alpha$ ,  $\lambda = 1.5418 \text{ \AA}$ ) with a scan rate of  $2^\circ \text{ min}^{-1}$ . High-resolution transmission electron microscopy (HRTEM) images are acquired on a JEOL JEM-2100F operated at 200 kV. X-ray photoelectron spectroscopy (XPS) measurements are conducted on a PHI-5400 system using an  $\text{Al K}\alpha$  source (250 W) with a position-sensitive detector. Co K-edge X-ray absorption near-edge structure (XANES) and extended X-ray absorption fine structure (EXAFS) spectra are collected in transmission mode at the X-ray Absorption Fine-structure for Catalysis (XAFCA) beamline of the Singapore Synchrotron Light Source. Data reduction and analysis are performed with the Athena package.

### Electrochemical measurement

Electrocatalyst pre-activation is conducted in a single-cell setup; all other electrochemical tests use a custom H-cell separated by a Nafion 117 membrane (DuPont) at ambient conditions. Before using the membrane, it is soaked in 5 wt%  $\text{H}_2\text{O}_2$  solution at 80 °C for 1 hour first, then it is soaked in 5 wt%  $\text{H}_2\text{SO}_4$  solution at 80 °C for 1 hour, later it is soaked in deionized water for an hour at 80 °C. A Biologic-SP150 potentiostat is used to record the electrochemical response. In the typical three-electrode system, a glassy carbon electrode (the glassy carbon electrode is a disk electrode with a diameter of  $\Phi=5 \text{ mm}$ . The exposed geometric electrode area is calculated from the disk area,  $A=\pi d^2/4$ , giving an area of  $0.196 \text{ cm}^2$ ), a Hg/HgO electrode and a platinum plate electrode are used as the working electrode, reference and counter electrode, respectively. The Hg/HgO reference is calibrated in 1 M KOH following literature procedures. Solution resistance is determined by potentiostatic electrochemical impedance spectroscopy (200 kHz to 0.1 Hz).

Catalyst inks are prepared by dispersing 25 mg catalyst, 12.5 mg acetylene black, 3.875 mL deionized water, 1.0 mL isopropyl alcohol, and 125  $\mu\text{L}$  Nafion solution (5 wt%) by sonication for  $\geq 2$  h. An 8  $\mu\text{L}$  aliquot is drop-cast onto the glassy carbon electrode, yielding a loading of  $204.1 \mu\text{g cm}^{-2}$ . Pre-activation of  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  is performed by chronoamperometry at 1.6 V vs. RHE for 2 h in 1 M KOH. For nitrate reduction ( $\text{NO}_3\text{RR}$ ), 40 mL of 1 M KOH + 0.1 M  $\text{KNO}_3$  is used in each H-cell compartment. The electrolyte is purged with Ar for 30 min prior to testing. Cyclic voltammetry (CV) is recorded at  $10 \text{ mV s}^{-1}$ . The  $\text{NO}_3\text{RR}$  is measured at a stirring rate of 600 rpm in the cathodic chamber. FE and  $\text{NH}_3$  yield rate are evaluated at potentials from  $-0.2$  to  $-0.6 \text{ V vs. RHE}$  in 0.1 V increments using 30-min potentiostatic holds. Potentials are converted to the RHE scale according to  $E (\text{V vs. RHE}) = E (\text{vs. Hg/HgO}) + 0.098 + 0.0591 \times \text{pH} (25 \text{ }^\circ\text{C})$ , unless otherwise specified. All electrochemical measurements are repeated independently three times. The data are reported as mean  $\pm$  standard deviation, and the error bars represent the standard deviation derived from three independent measurements.

### Product analysis

**Ammonia detection**  $\text{NH}_3$  concentrations are determined by the indophenol blue method. Electrolyte samples are withdrawn and diluted to the calibration range. A 2 mL aliquot of the diluted solution is mixed with 2 mL of 1 M KOH containing 5 wt% salicylic acid and 5 wt% potassium citrates. Next, 1 mL of 0.05 M  $\text{KClO}$  and 0.2 mL of 1.0 wt%  $\text{C}_5\text{FeN}_6\text{K}_2\text{O}$  (potassium nitroferricyanide) solution are added. After 2 h at room temperature, absorbance at 655 nm was measured on a UV-2600 spectrophotometer and converted to  $\text{NH}_3$  concentration using a calibration curve.<sup>13</sup>

**Nitrite detection** A color reagent is prepared by dissolving 0.2 g N-(1-naphthyl)ethylenediamine dihydrochloride, 4 g p-aminobenzenesulfonamide, and 10 mL phosphoric acid ( $\rho = 1.685 \text{ g mL}^{-1}$ ) in 50 mL deionized water with thorough stirring. Electrolyte samples are diluted to the calibration range, and 5 mL of the diluted sample is combined with 0.1 mL color reagent. After 20 min at room temperature, the absorbance at 540 nm is recorded.<sup>13</sup> Nitrite concentrations are obtained from calibration with standard  $\text{KNO}_2$  solutions.

### FE and yield rate

Faradaic efficiency (FE) is calculated as:

$$FE = \frac{ncV_{\text{catholyte}}F}{Q} \times 100\%$$

where  $n$  is the electron-transfer number (8 for  $\text{NH}_3$ , 2 for  $\text{NO}_2^-$ ),  $c$  is the concentration of  $\text{NH}_3$  or  $\text{NO}_2^-$ ,  $V_{\text{catholyte}}$  is the catholyte volume (40 mL),  $F$  is the Faradaic constant ( $96485 \text{ C mol}^{-1}$ ), and  $Q$  is the total charge passed.

Yield rate is calculated as:

$$\text{Yield} = \frac{cV_{\text{catholyte}}}{St}$$

where  $S$  is the geometric area of the cathode, and  $t$  is the electrolysis time (30 min).

### Electrochemical in-situ ATR-FTIR

In situ ATR-FTIR spectra are acquired following our previous procedure<sup>14</sup> using a Bruker Vertex 80 coupled to a PIKE VeeMAX III electrochemical accessory. A liquid-nitrogen-cooled mercury cadmium telluride (MCT) detector is employed. The internal reflection element is a Si prism coated by e-beam evaporation with Ti (5 nm) and Au (25 nm), used at an incidence angle of  $60^\circ$ . Catalysts are drop-cast on the prism to a loading of  $0.2 \text{ mg cm}^{-2}$  and served as the working electrode. An Ag/AgCl (sat. KCl) reference and a graphite rod counter electrode are used. The electrolyte is 1 M KOH + 0.1 M  $\text{KNO}_3$ . Spectra are collected during chronoamperometry at the indicated potentials.

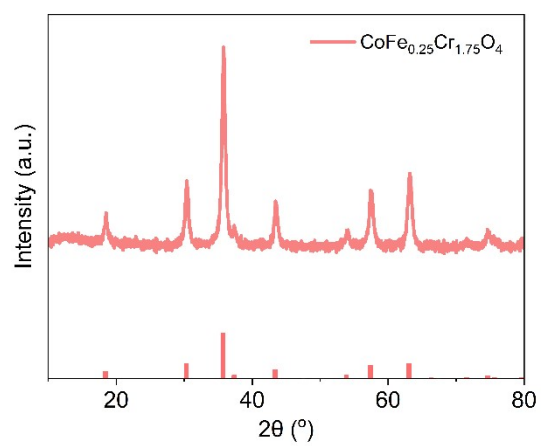
### Electrochemical impedance spectroscopy

Electrochemical impedance spectroscopy is performed to evaluate the interfacial charge-transfer behavior of  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$ , A- $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$ , and  $\text{Co}_{0.8}\text{Fe}_{0.2}(\text{OH})_2$  during nitrate reduction. The Nyquist plots are fitted using a modified Randles circuit,  $R_s - (R_{ct} \parallel \text{CPE}_{dl})$ , where  $R_s$  represents the solution resistance,  $R_{ct}$  denotes the charge-transfer resistance associated with the faradaic  $\text{NO}_3^-$  reduction process, and  $\text{CPE}_{dl}$  describes the non-ideal double-layer capacitance at the electrode/electrolyte interface,  $n$  is the CPE exponent. The fitted  $R_s$  values are similar for the three samples, ranging from 5.02 to 5.60  $\Omega$ , indicating comparable ohmic resistance under the same electrolyte and cell configuration. In contrast, the  $R_{ct}$  value decreases markedly from 61.79  $\Omega$  for  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  to 10.21  $\Omega$  for A- $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  and 9.43  $\Omega$  for  $\text{Co}_{0.8}\text{Fe}_{0.2}(\text{OH})_2$ , revealing substantially improved interfacial charge-transfer kinetics after activation/reconstruction and for the  $\text{Co}_{0.8}\text{Fe}_{0.2}(\text{OH})_2$  reference. The much smaller  $R_{ct}$  of A- $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  compared with  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  suggests that the activated surface provides a more favorable interface for electron transfer during  $\text{NO}_3^-$ RR. In addition, the use of  $\text{CPE}_{dl}$  rather than an ideal capacitor accounts for the depressed semicircular response, which is commonly associated with surface heterogeneity, roughness, distributed active sites, and non-uniform adsorption environments on electrocatalyst surfaces. Therefore, the EIS results support that activation/reconstruction effectively lowers the

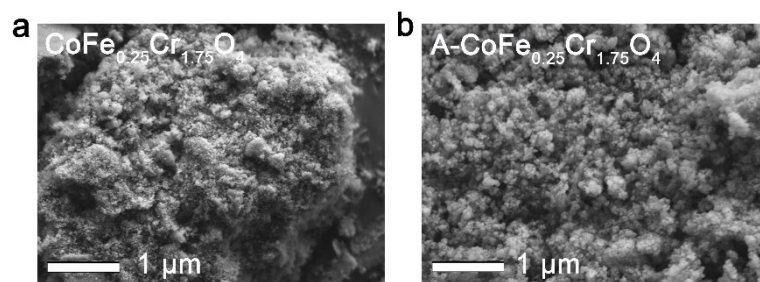
interfacial kinetic barrier and facilitates NO<sub>3</sub>RR.

### Turnover frequency calculations

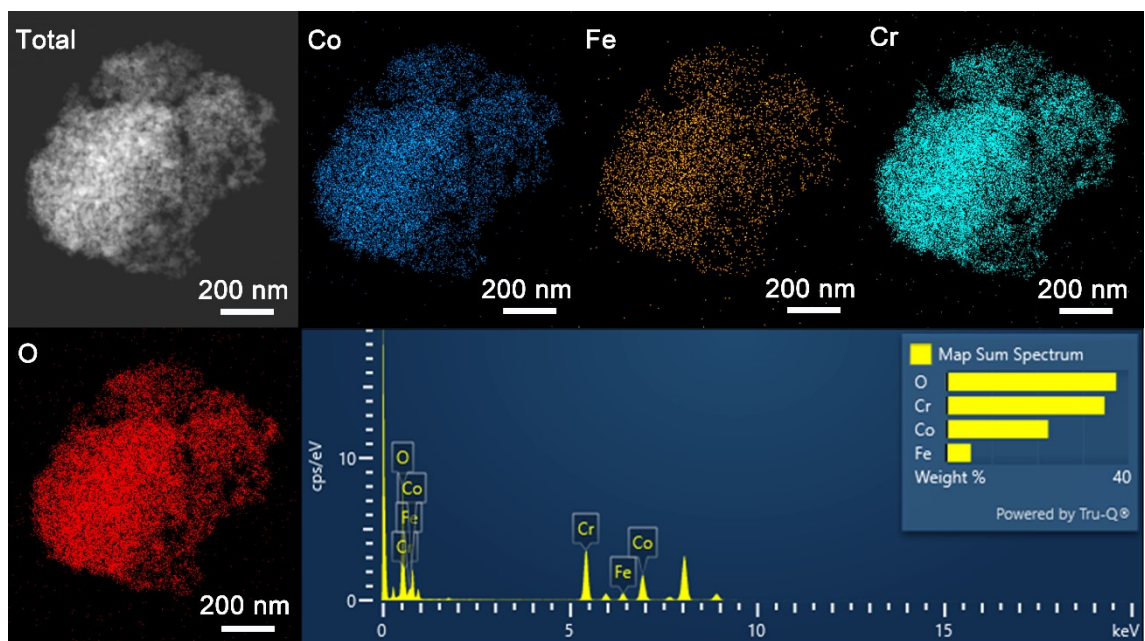
The TOF is calculated according to the equation:  $T = j \cdot A \cdot F E_{\text{NH}_3} / (8 \cdot F \cdot n)$ , Where  $j$  is the current density normalized by BET surface area,  $A$  is the BET surface area;  $F$  is the Faraday constant (96485 C mol<sup>-1</sup>);  $n$  is the mole number of active atoms on the electrode. The number of active sites ( $n$ ) is calculated as:  $n_{\text{bulk}} = m_{\text{ox}} / M_{\text{ox}}$ , where  $m_{\text{ox}}$  is the mass of the catalyst,  $M_{\text{ox}}$  is the molecular weight of the catalyst. Take CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub> as an example, to convert  $n_{\text{bulk}}$  to  $n$ , if Co+Fe is assumed to be the active sites,  $n = 1.25 \times n_{\text{bulk}}$ .



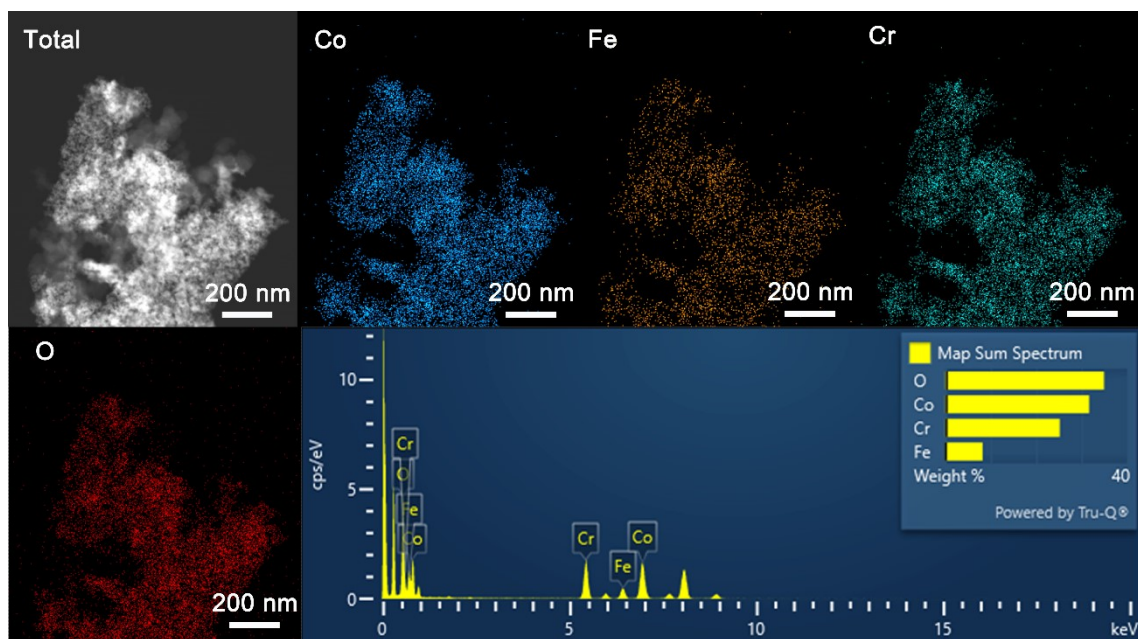
**Fig. S1** XRD pattern of  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$ .



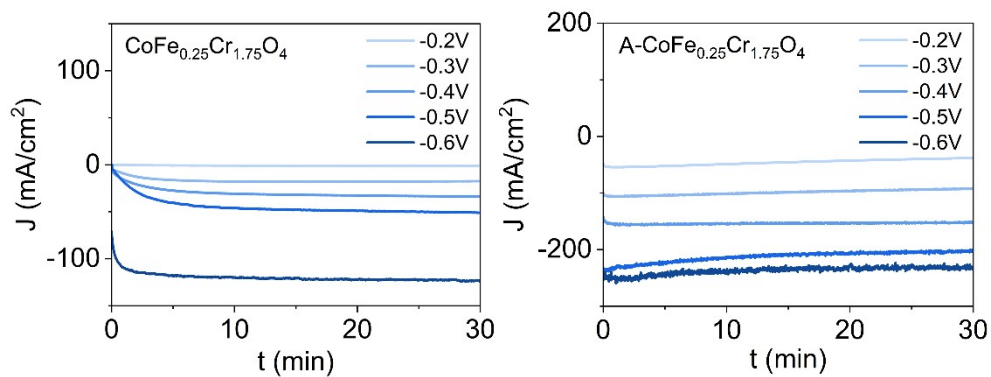
**Fig. S2** SEM images of **a**  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$ , and **b** activated  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  (A- $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$ ).



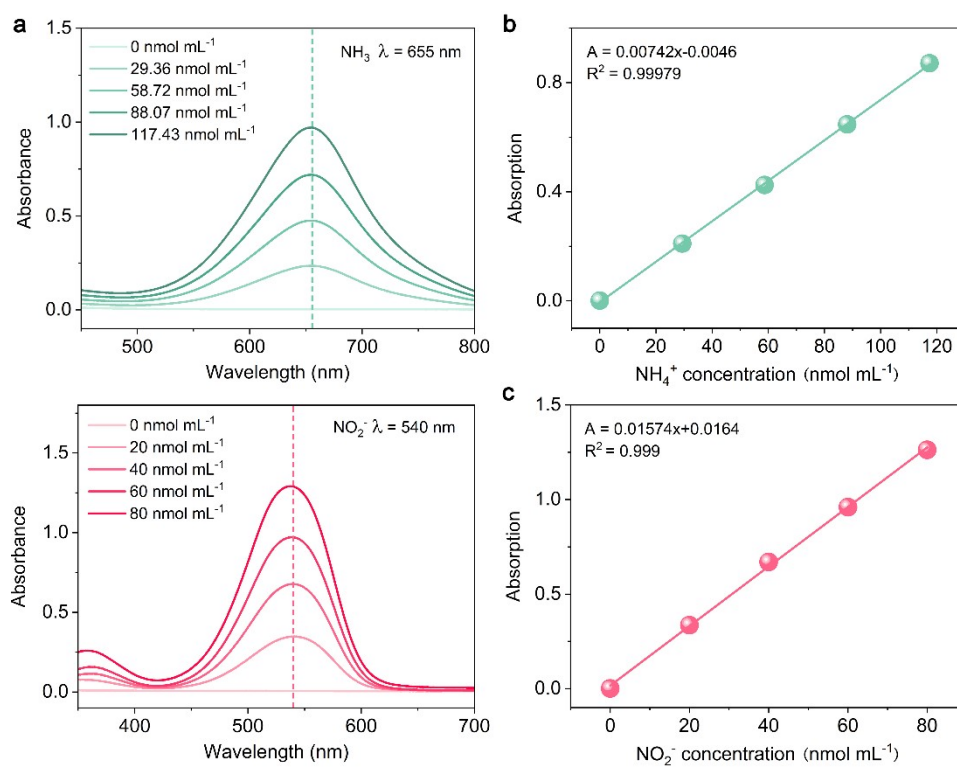
**Fig. S3** EDS mapping images of  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$ .



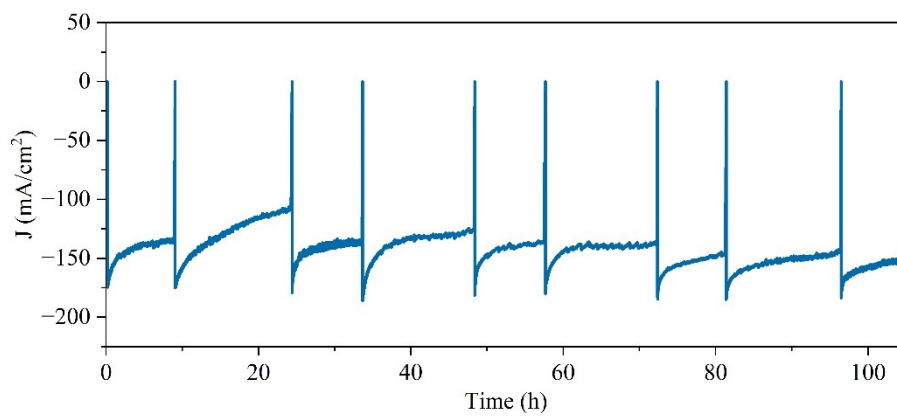
**Fig. S4** EDS mapping images of A-CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub>.



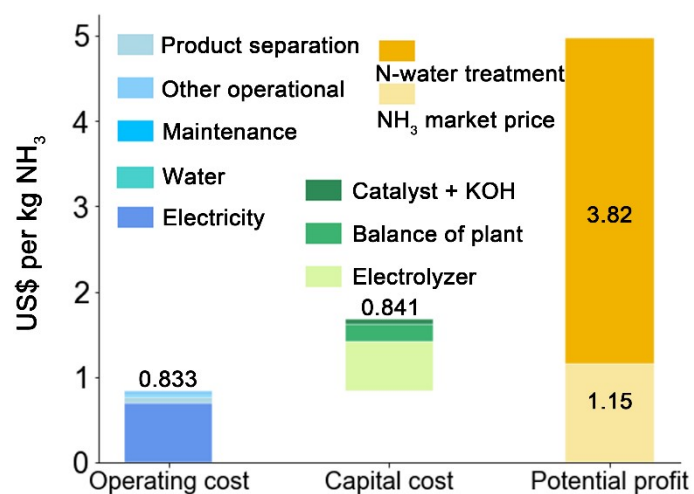
**Fig. S5** Chronoamperometry curves of  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  and  $\text{A-CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  in 1 M KOH + 0.1 M  $\text{KNO}_3$  electrolyte under different potentials in H-cell.



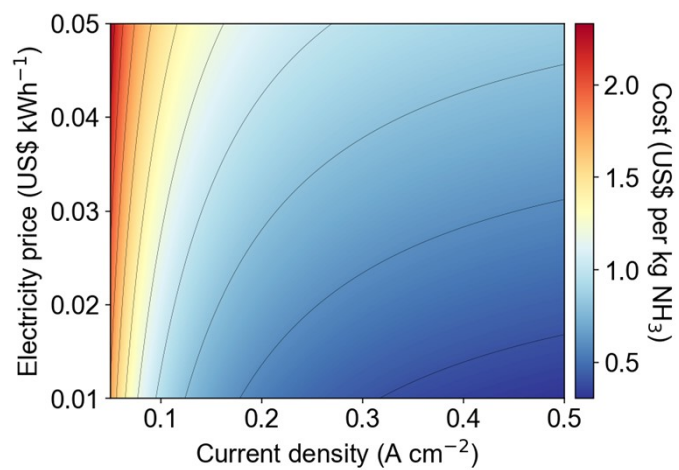
**Fig. S6** UV-vis curves of **a**  $\text{NH}_4^+$  and **c**  $\text{NO}_2^-$ . **b** Calibration curve at 655 nm for different  $\text{NH}_4^+$  concentrations. **d** Calibration curve at 540 nm for different  $\text{NO}_2^-$  concentrations.



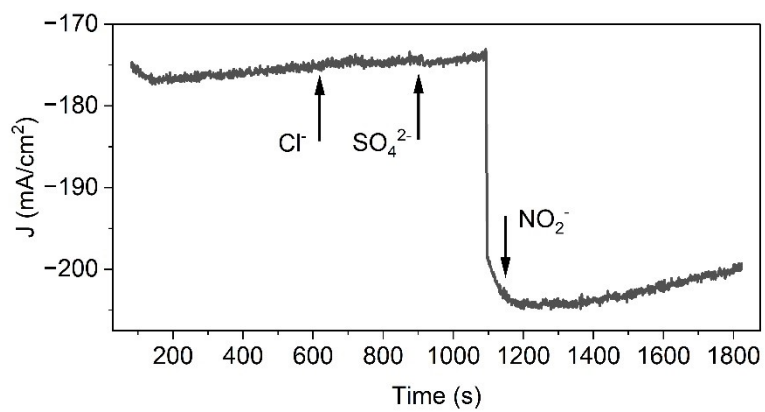
**Fig. S7** Long-term CA stability test (larger 100 hours) for A-CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub> at -0.4 V/RHE. The periodic spikes in the current curve indicate electrolyte repositioning.



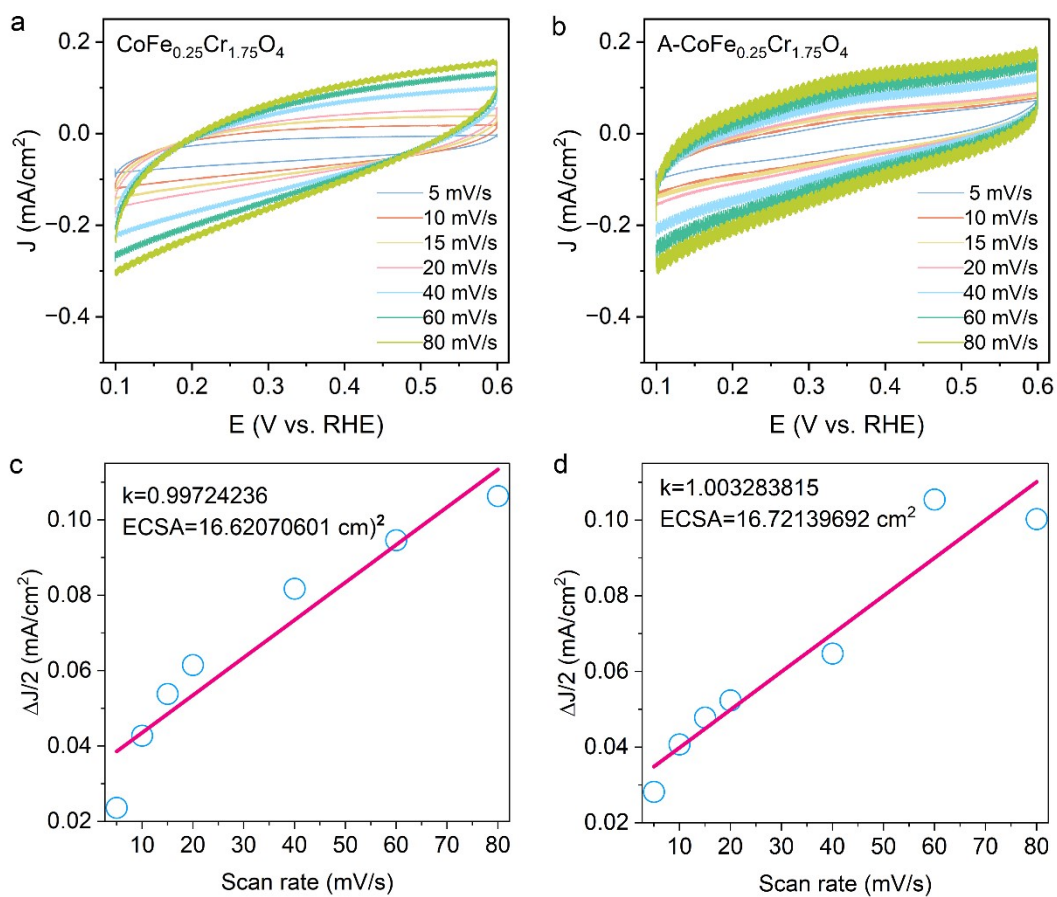
**Fig. S8** Breakdown of production cost of NH<sub>3</sub> synthesis by NO<sub>3</sub>RR and its potential profits. The total cost is US\$1.674 per kg NH<sub>3</sub>. Potential profits include selling NH<sub>3</sub> at the market price as well as the operational expenses of wastewater treatment through nitrate removal.



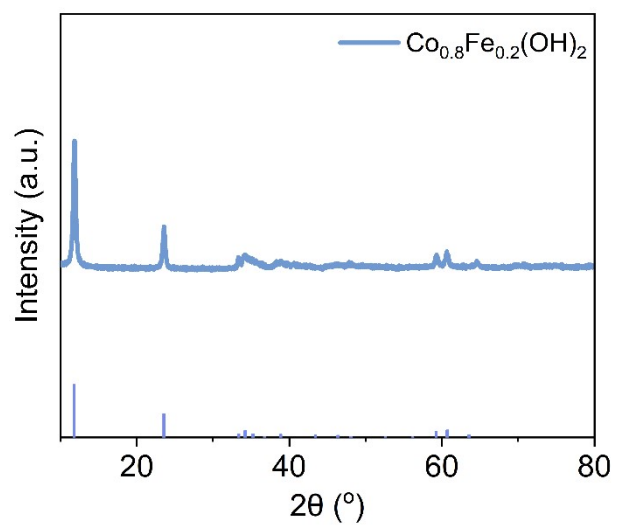
**Fig. S9** Contour map for  $\text{NH}_3$  synthesis costs as a function of current density and electricity price.



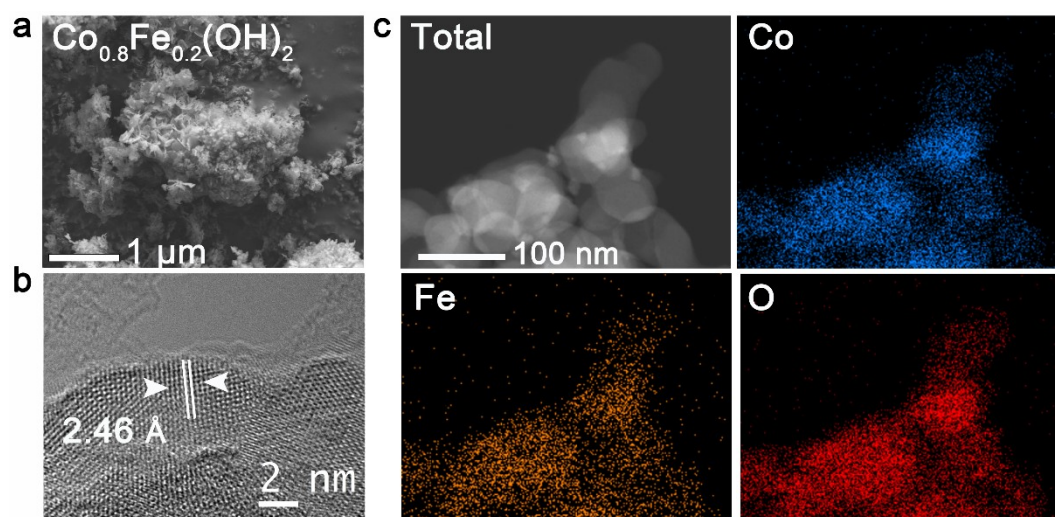
**Fig. S10** Stability test using interfering ions ( $\text{Cl}^-$ ,  $\text{SO}_4^{2-}$  and  $\text{NO}_2^-$ ).



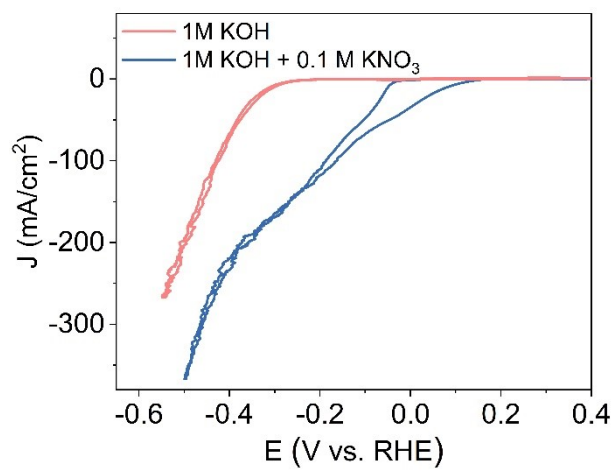
**Fig. S11** CV curves of (a) CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub>, (b) A-CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub>, and the corresponding fitting of (c) CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub> and (d) A-CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub> to obtain double-layer capacitances at scan rates of 80, 60, 60, 40, 20, 15, 10 and 5 mV s<sup>-1</sup> in 1 M KOH. The geometry area of the working electrode (glassy carbon) is 0.196 cm<sup>2</sup>, and the catalyst loading is 0.2 mg cm<sup>-2</sup>.



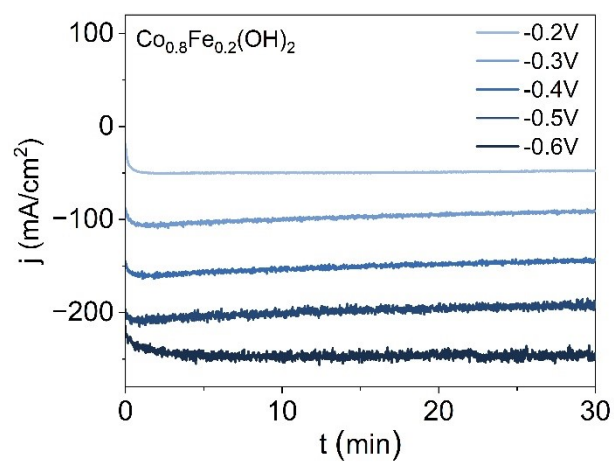
**Fig. S12** XRD pattern of  $\text{Co}_{0.8}\text{Fe}_{0.2}(\text{OH})_2$ .



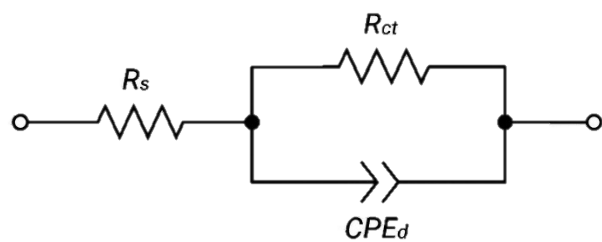
**Fig. S13** a SEM, b HRTEM, and corresponding c EDS mapping images of  $\text{Co}_{0.8}\text{Fe}_{0.2}(\text{OH})_2$ .



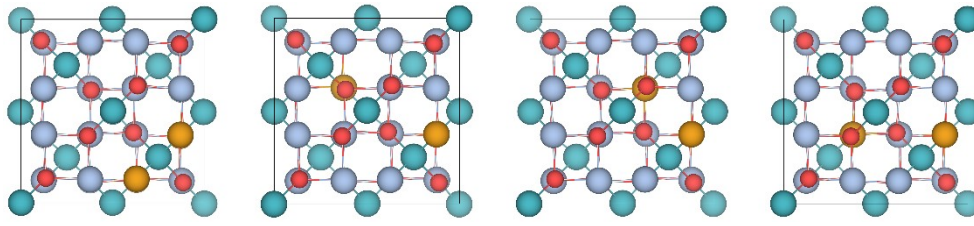
**Fig. S14** Cyclic voltammetry curves of  $\text{Co}_{0.8}\text{Fe}_{0.2}(\text{OH})_2$ .



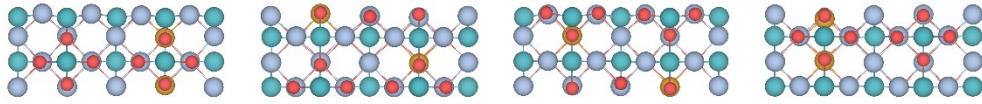
**Fig. S15** Chronoamperometry curves of  $\text{Co}_{0.8}\text{Fe}_{0.2}(\text{OH})_2$  in 1 M KOH + 0.1 M  $\text{KNO}_3$  electrolyte under different potentials in H-cell.



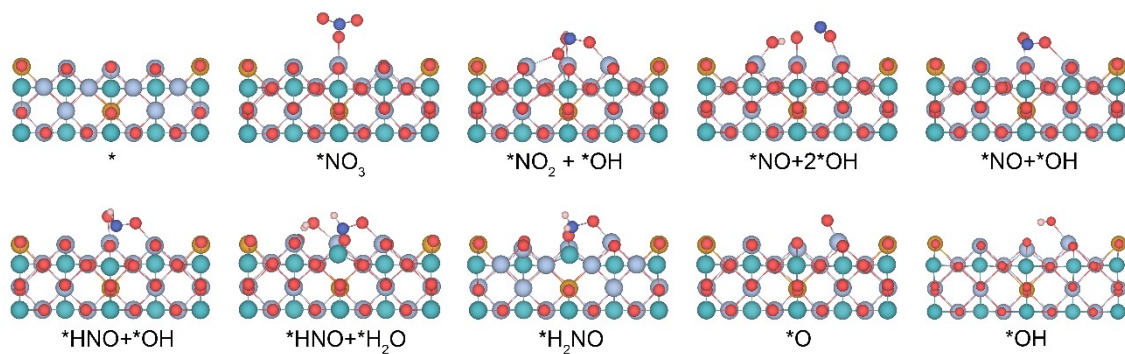
**Fig. S16** Equivalent circuit for electrochemical impedance spectroscopy.



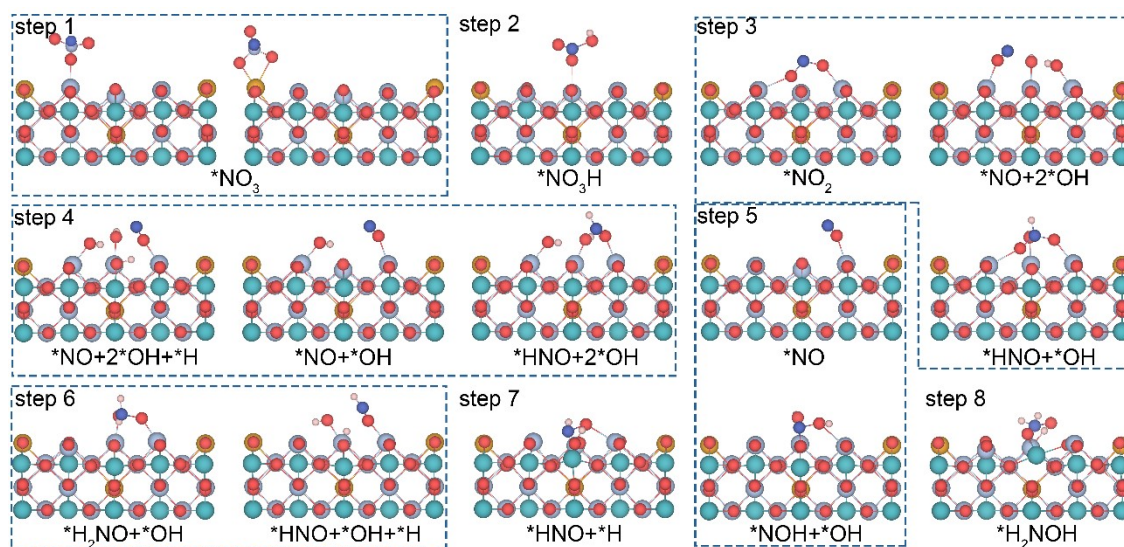
**Fig. S17** Possible structure configurations of bulk  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$ . Red, orange, light blue and dark blue atoms indicate the oxygen, iron, chromium, and cobalt atoms.



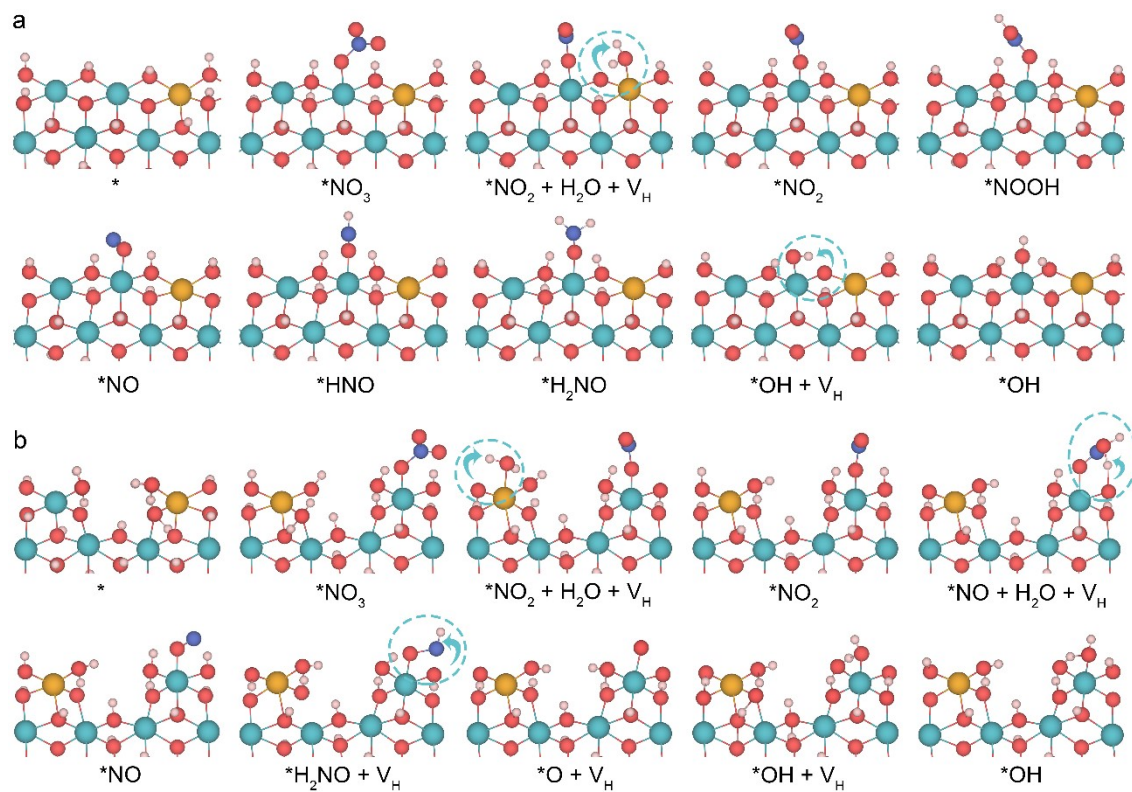
**Fig. S18** Possible configurations of CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub> (1 1 0) surface. Red, orange, light blue and blue atoms indicate the oxygen, iron, chromium, and cobalt atoms.



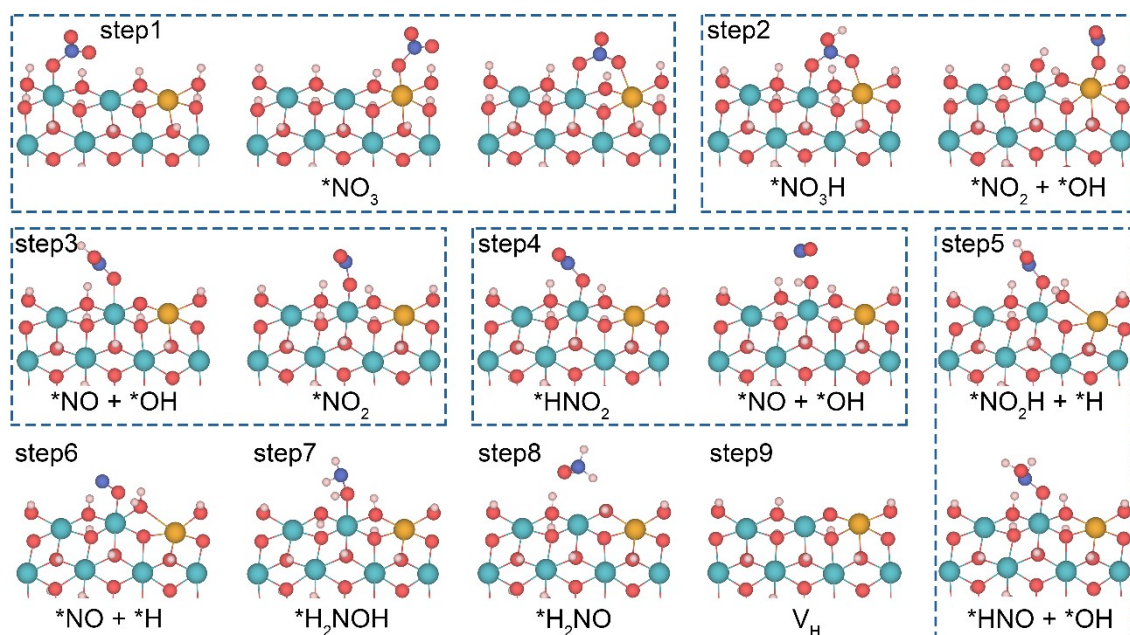
**Fig. S19** The most stable configurations of intermediates on  $CoFe_{0.25}Cr_{1.75}O_4$  (110) surface during  $NO_3RR$ . Red, orange, light blue, blue, dark blue, and pink atoms indicate the oxygen, iron, chromium, cobalt, nitrogen and hydrogen atoms.



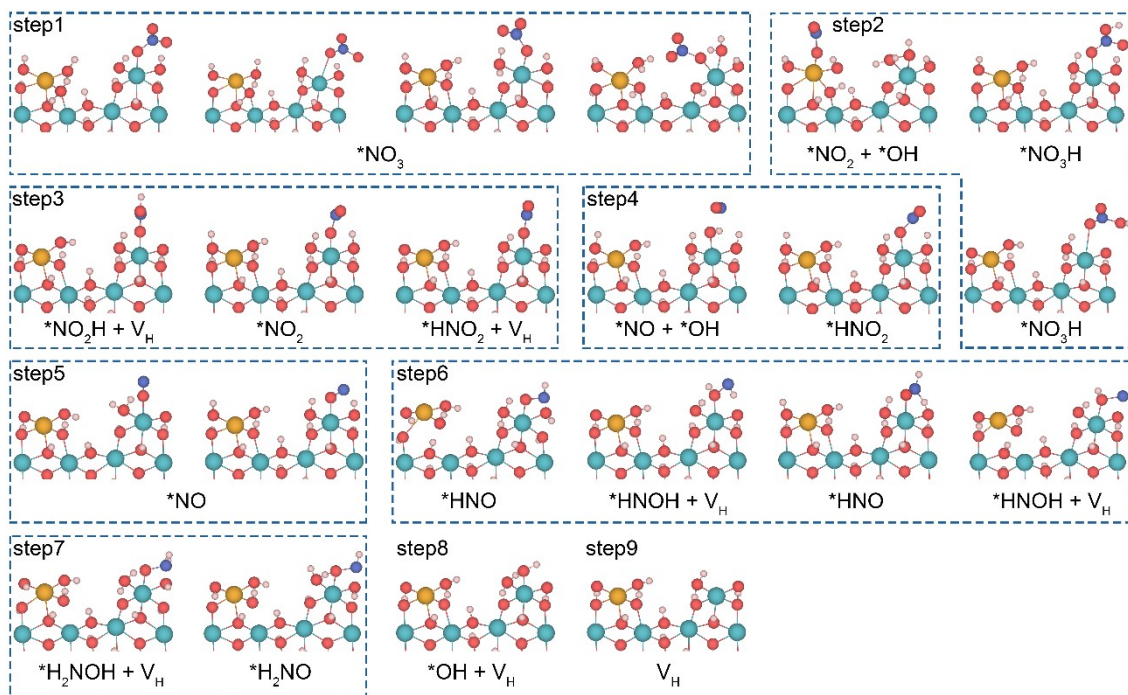
**Fig. S20** The other possible configurations of intermediates on  $\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$  (110) surface during  $\text{NO}_3\text{RR}$ . Red, orange, light blue, blue, dark blue, and pink atoms indicate the oxygen, iron, chromium, cobalt, nitrogen and hydrogen atoms.



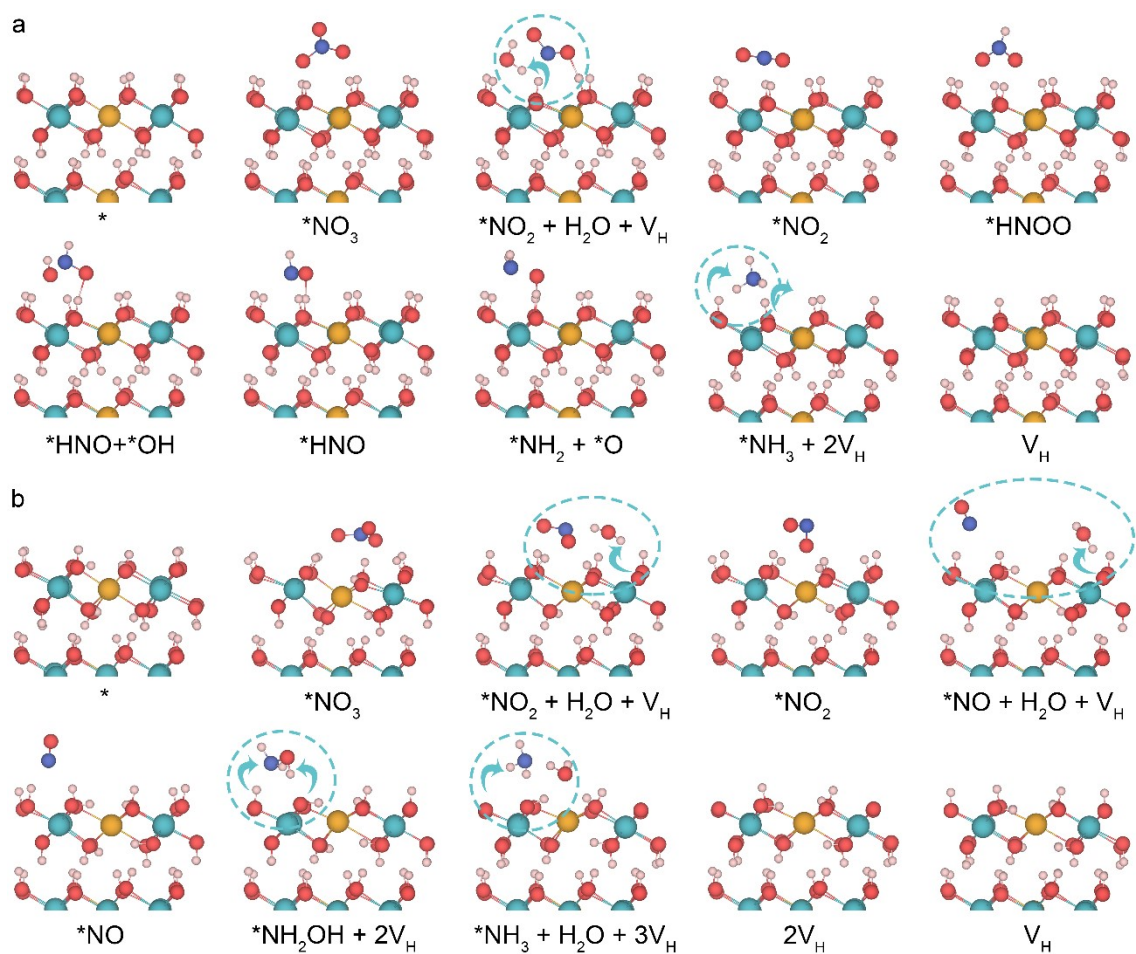
**Fig. S21** The most stable configurations of intermediates on **a** Co<sub>0.8</sub>Fe<sub>0.2</sub>(OH)<sub>2</sub> and **b** A-CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub> (100) surfaces during NO<sub>3</sub>RR. Red, orange, blue, dark blue, and pink atoms indicate the oxygen, iron, cobalt, nitrogen and hydrogen atoms.



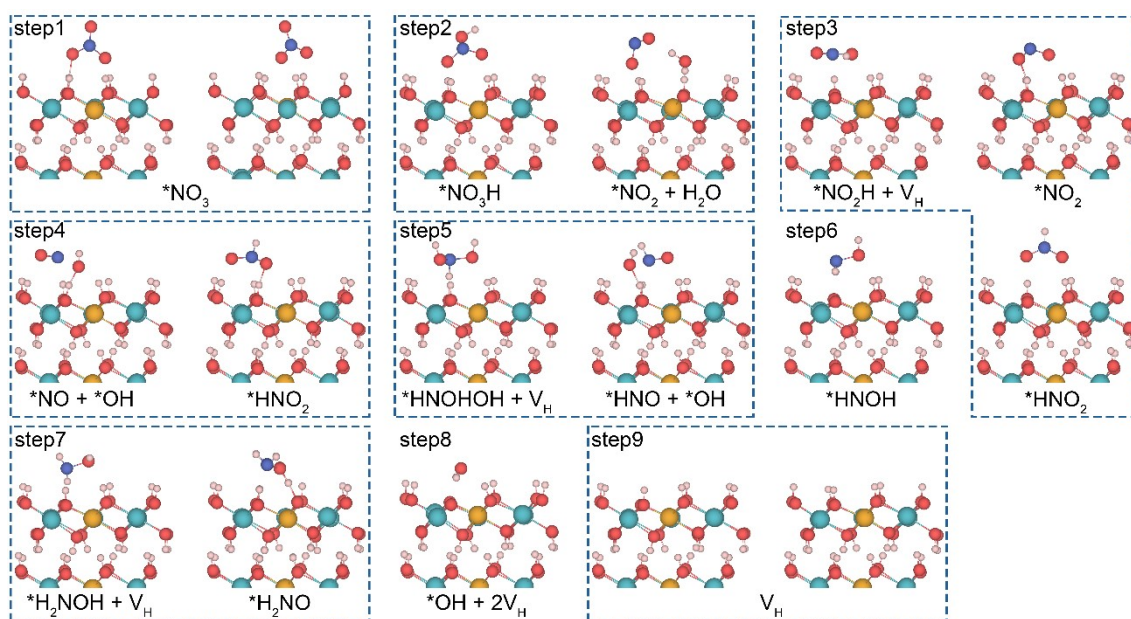
**Fig. S22** The other possible configurations of intermediates on Co<sub>0.8</sub>Fe<sub>0.2</sub>(OH)<sub>2</sub> (100) surface during NO<sub>3</sub>RR. Red, orange, blue, dark blue, and pink atoms indicate the oxygen, iron, cobalt, nitrogen and hydrogen atoms.



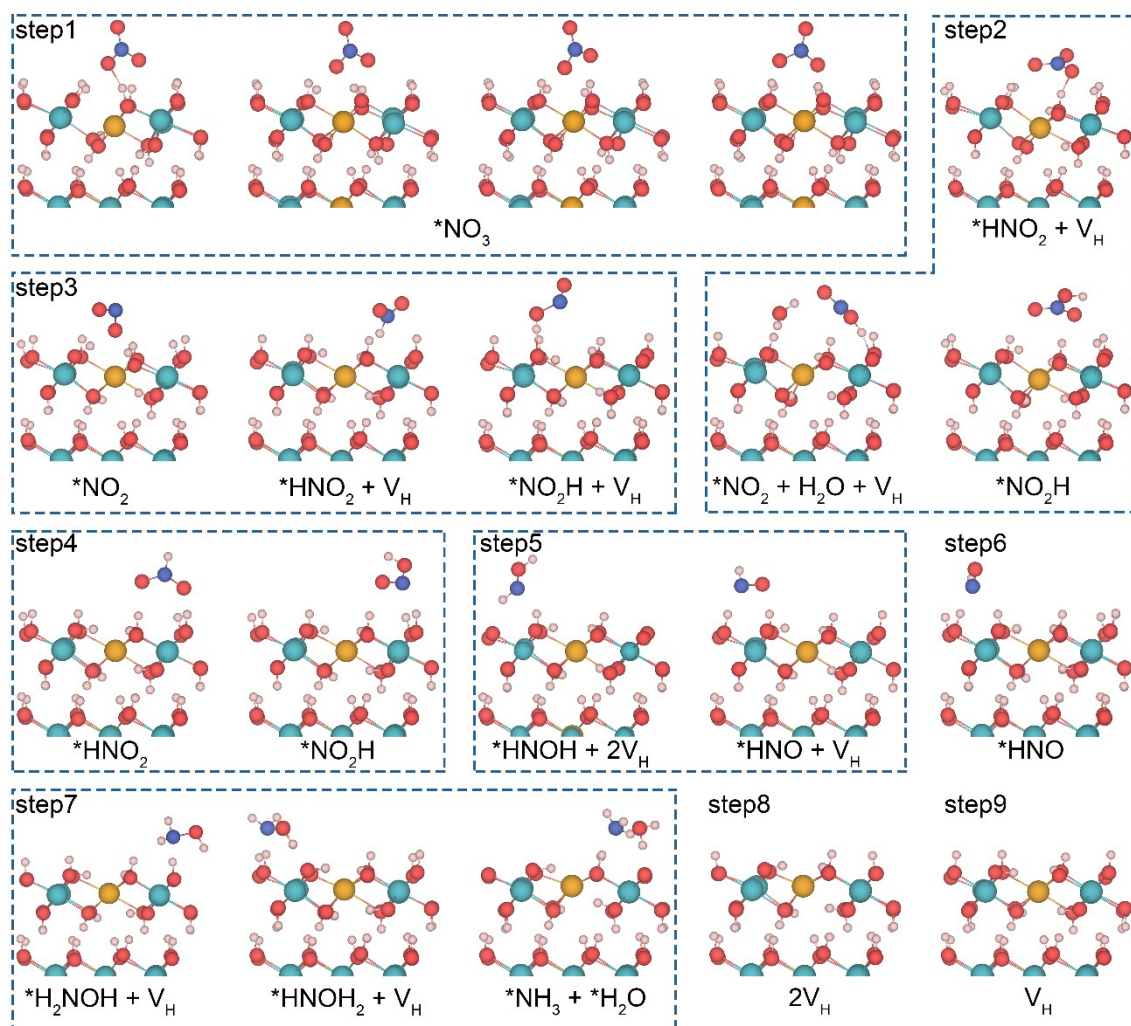
**Fig. S23** The possible configurations of intermediates on A-CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub> (100) surface during NO<sub>3</sub>RR. Red, orange, blue, dark blue, and pink atoms indicate the oxygen, iron, cobalt, nitrogen and hydrogen atoms.



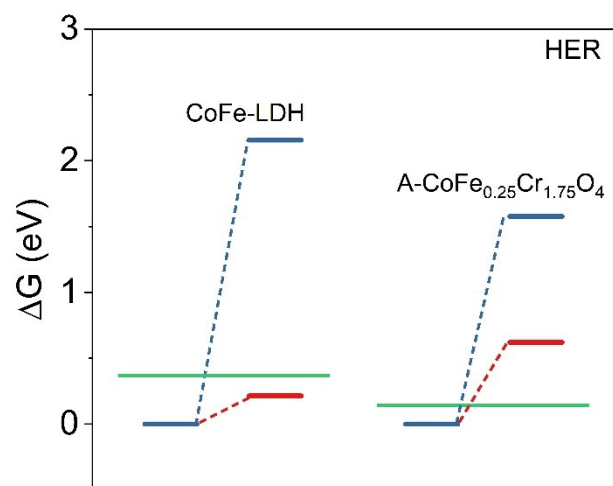
**Fig. S24** The most stable configurations of intermediates on **a**  $Co_{0.8}Fe_{0.2}(OH)_2$  and **b**  $A-CoFe_{0.25}Cr_{1.75}O_4$  (001) surfaces during  $NO_3RR$ . Red, orange, blue, dark blue, and pink atoms indicate the oxygen, iron, cobalt, nitrogen and hydrogen atoms.



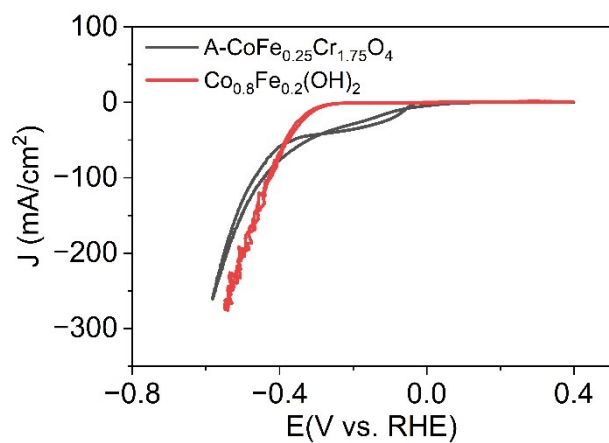
**Fig. S25** The other possible configurations of intermediates on  $Co_{0.8}Fe_{0.2}(OH)_2$  (001) surface during  $NO_3RR$ . Red, orange, blue, dark blue, and pink atoms indicate the oxygen, iron, cobalt, nitrogen and hydrogen atoms.



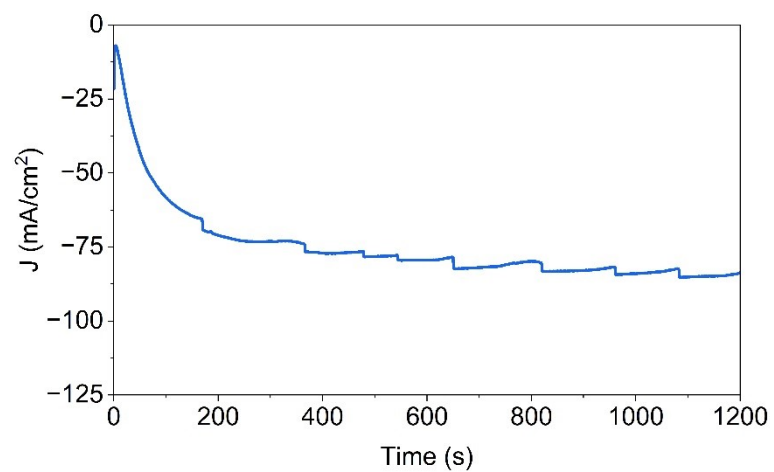
**Fig. S26** The other possible configurations of intermediates on A-CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub> (001) surface during NO<sub>3</sub>RR. Red, orange, blue, dark blue, and pink atoms indicate the oxygen, iron, cobalt, nitrogen and hydrogen atoms.



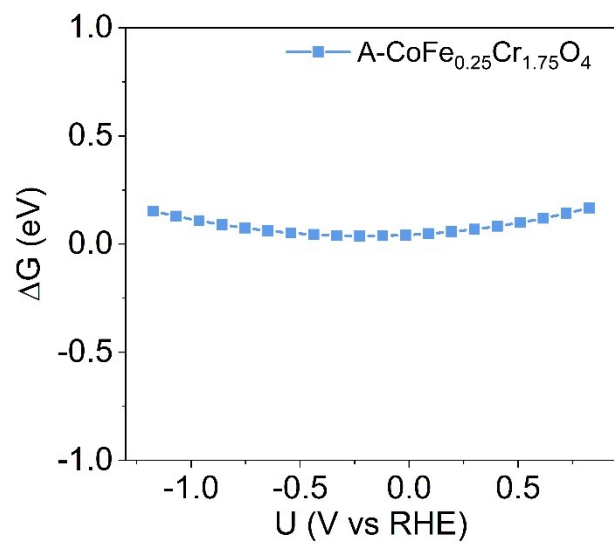
**Fig. S27** Gibbs free energies of the hydrogen evolution reaction on  $\text{Co}_{0.8}\text{Fe}_{0.2}(\text{OH})_2$  and  $\text{A-CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$ . Blue and red lines indicate whether the protons in the generated  $\text{H}_2$  are single proton or two protons from lattice-hydrogen. Green line indicates the limiting potential of  $\text{NO}_3\text{RR}$  on  $\text{Co}_{0.8}\text{Fe}_{0.2}(\text{OH})_2$  and  $\text{A-CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$ .



**Fig. S28** Cyclic voltammetry curves of A-CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub> and Co<sub>0.8</sub>Fe<sub>0.2</sub>(OH)<sub>2</sub> in 1 M KOH electrolyte.



**Fig. S29** Chronoamperometry curves for A-CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub> at -0.2 V/RHE in 1 M KOH electrolyte.



**Fig. S30** The constant potential calculation of NO<sub>3</sub>RR potential-determining step on A-CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub>.

**Table S1.** Curve fit parameters<sup>a</sup> for Co *K*-edge EXAFS of pristine CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub>.

| Path | $d^b/\text{\AA}$ | $N$    | $R/\text{\AA}$ | $\sigma^2/\text{\AA}^2$ |
|------|------------------|--------|----------------|-------------------------|
| Co-O | 1.943            | 4.4(2) | 1.97(2)        | 0.003(3)                |

<sup>a</sup> $S_0^2$  is fixed as 0.74703, obtained from Co foil fitting.  $\Delta E_0$  is refined as a global fit parameter, returning a value of  $(4 \pm 1)$  eV. Data ranges:  $3 \leq k \leq 12 \text{\AA}^{-1}$ ,  $1.0 \leq R \leq 2.0 \text{\AA}$ . The number of variable parameters is 4, out of a total of 5.59 independent data points. R factor for this fit is 0.16%. <sup>b</sup>The distance is from the crystal structure of Co<sub>2</sub>O<sub>3</sub>. <sup>c</sup>The Debye-Waller factor was fixed to reduce the number of variables.

**Table S2.** Curve fit parameters<sup>a</sup> for Co *K*-edge EXAFS of A-CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub>.

| Path | $d^b/\text{\AA}$ | $N$    | $R/\text{\AA}$ | $\sigma^2/\text{\AA}^2$ |
|------|------------------|--------|----------------|-------------------------|
| Co-O | 1.943            | 4.5(2) | 1.95(6)        | 0.003 <sup>c</sup>      |

<sup>a</sup> $S_0^2$  is fixed as 0.74703, obtained from Co foil fitting.  $\Delta E_0$  is refined as a global fit parameter, returning a value of  $(3 \pm 1)$  eV. Data ranges:  $3 \leq k \leq 12 \text{\AA}^{-1}$ ,  $1.0 \leq R \leq 2.0 \text{\AA}$ . The number of variable parameters is 3, out of a total of 5.5 independent data points. R factor for this fit is 0.4%. <sup>b</sup>The distance is from the crystal structure of Co<sub>2</sub>O<sub>3</sub>. <sup>c</sup>The Debye-Waller factor is fixed to reduce the number of variables.

**Table S3.** Curve fit parameters<sup>a</sup> for Co *K*-edge EXAFS for CoFe<sub>0.25</sub>Cr<sub>1.75</sub>O<sub>4</sub> after reaction.

| Path | $d^b/\text{\AA}$ | $N$    | $R/\text{\AA}$ | $\sigma^2/\text{\AA}^2$ |
|------|------------------|--------|----------------|-------------------------|
| Co-O | 1.943            | 4.5(3) | 1.97(9)        | 0.004 <sup>c</sup>      |

<sup>a</sup> $S_0^2$  is fixed as 0.74703, obtained from Co foil fitting.  $\Delta E_0$  is refined as a global fit parameter, returning a value of  $(4 \pm 1)$  eV. Data ranges:  $3 \leq k \leq 12 \text{\AA}^{-1}$ ,  $1.0 \leq R \leq 2.0 \text{\AA}$ . The number of variable parameters is 3, out of a total of 5.5 independent data points. R factor for this fit is 1.2%. <sup>b</sup>The distance is from the crystal structure of Co<sub>2</sub>O<sub>3</sub>. <sup>c</sup>The Debye-Waller factor is fixed to reduce the number of variables.

**Table S4.** Curve fit parameters<sup>a</sup> for Co *K*-edge EXAFS for pristine Co<sub>0.8</sub>Fe<sub>0.2</sub>(OH)<sub>2</sub>.

| Path | $d^b/\text{\AA}$ | $N$              | $R/\text{\AA}$ | $\sigma^2/\text{\AA}^2$ |
|------|------------------|------------------|----------------|-------------------------|
| Co-O | 2.097            | 6.0 <sup>c</sup> | 2.07(2)        | 0.006(2)                |

<sup>a</sup> $S_0^2$  is fixed as 0.74703, obtained from Co foil fitting.  $\Delta E_0$  is refined as a global fit parameter, returning a value of  $(3 \pm 1)$  eV. Data ranges:  $3 \leq k \leq 12 \text{\AA}^{-1}$ ,  $1.0 \leq R \leq 2.1 \text{\AA}$ . The number of variable parameters is 3, out of a total of 6.0 independent data points. R factor for this fit is 2.4%. <sup>b</sup>The distance is from the crystal structure of  $\alpha$ -Co<sub>0.8</sub>Fe<sub>0.2</sub>(OH)<sub>2</sub>. <sup>c</sup>The coordination number is fixed to reduce the number of variables.

## Technoeconomic analysis (TEA)

**Table S5** Input parameters for the TEA model.

|                                      |                               |
|--------------------------------------|-------------------------------|
| NH <sub>3</sub> production rate      | 1,000 kg day <sup>-1</sup>    |
| Operating time                       | 350 days year <sup>-1</sup>   |
| Electrolyzer base cost <sup>15</sup> | 550 USD kW <sup>-1</sup>      |
| Balance of plant <sup>16</sup>       | 35% of the electrolyzer cost  |
| Maintenance cost <sup>17</sup>       | 2.5% of the electrolyzer cost |

|   |                              |
|---|------------------------------|
| Installation cost                                     | 12% of the electrolyzer cost |
| Catalysts cost  | 5% of the electrolyzer cost  |
| KOH cost  | 5% of the electrolyzer cost  |
| Product separation costs                              | 10% of the electricity cost  |
| Other operational costs                               | 10% of the electrolyzer cost |
| Plant lifetime  | 20 years                     |
| Discount rate   | 5%                           |
| Electric price (USD kWh <sup>-1</sup> ) <sup>18</sup> | 0.03                         |

**Noted:** The total cost is separated into 7 components, namely the **capital cost**, **electricity cost**, **maintenance cost**, **product separation cost**, **water cost**, **balance of plant cost** and **other operational costs**.<sup>19,20</sup>

**For 0.1 M NaNO<sub>3</sub>:**

The charge required to produce per 1000 kg NH<sub>3</sub>:

$$Q = \frac{n(NH_3) \times N \times F}{FE} = \frac{1 \times 10^6 g \times 8 \times 96485 \frac{C}{mol}}{17 \frac{g}{mol} \times 0.94} = 4.825 \times 10^{10} C$$

The current required to sustain the process:

$$I = \frac{Q}{t} = \frac{4.825 \times 10^{10} C}{86400 s} = 558449 A$$

Area of electrolyzer:

$$area = \frac{I}{0.096 A cm^{-2}} = \frac{558449 A}{0.096 A cm^{-2}} = 581.7 m^2$$

Based on the E4tech/Element Energy report<sup>15</sup> and DOE H2A analysis for central grid electrolysis,<sup>16</sup> the electrolyzer cost for the stack component is 550 USD kW<sup>-1</sup> with a reference current density of 400 mA cm<sup>-2</sup> at 1.75 V. The total **electrolyzer cost** is calculated as:

*Electrolyzer cost*

$$= \frac{550 USD kW^{-1}}{1000 \frac{W}{kW}} \times \frac{400 mA cm^{-2}}{1000 \frac{mA}{A}} \times 1.75 V \times \frac{581.7 m^2}{0.0001 \frac{m^2}{cm^2}} \times 1.12 = 2508290.4 USD$$

Considering the capital recovery factor (CRF) based on a 5% discount rate (denote as *i* in the equation below), with the lifetime of 20 years:

$$CRF = \frac{i(1+i)^{20}}{i(1+i)^{20} - 1} = 0.0802$$

With the operation of 350 days per year and NH<sub>3</sub> production rate of 1000 kg day<sup>-1</sup>, the electrolyzer cost per kg of NH<sub>3</sub> is:

$$Electrolyzer\ cost = 2508290.4 USD \times \frac{0.0802}{350 days} \times \frac{1}{1000 kg/day} = 0.574 USD kg NH_3^{-1}$$

**Capital cost:**

$$\text{Capital cost} = \text{Electrolyzer cost} + \text{catalyst cost} + \text{KOH cost} = 0.632 \text{ USDkgNH}_3^{-1}$$

**Balance of plant cost:**

$$\text{Balance of plant cost} = \text{Electrolyzer cost} \times 35\% = 0.201 \text{ USDkgNH}_3^{-1}$$

**Maintenance cost:**

$$\text{Maintenance cost} = \text{Electrolyzer cost} \times 2.5\% = 0.014 \text{ USDkgNH}_3^{-1}$$

**Other operational costs:**

$$\text{Other operational cost} = \text{Electrolyzer cost} \times 10\% = 0.057 \text{ USDkgNH}_3^{-1}$$

The power required is calculated by:  $P = UI$  ( )  
 $= E_{ox}^0 - E_{re} + E_1$ , where  $E_{ox}^0 = 1.23 \text{ V}$ ,  $E_{re}$  is the cathodic potential,  $E_1$  is the overpotential

$$\text{Power required} = 1.73 \text{ V} \times 558449 \text{ A} \times \frac{\text{MW}}{10^6 \text{ W}} = 0.966 \text{ MW}$$

**Electricity cost:**

$$\text{Electricity cost} = \frac{0.966 \text{ MW}}{1000 \frac{\text{kW}}{\text{MW}}} \times 24 \text{ h} \times \frac{0.03 \text{ USD}}{\text{kWh}} \times \frac{1}{1000 \text{ kg/day}} = 0.697 \text{ USD kgNH}_3^{-1}$$

**Product separation costs:**

$$\text{Product separation costs} = \text{Electricity cost} \times 10\% = 0.07 \text{ USD kgNH}_3^{-1}$$

The water flow rate needed for anodic OER reaction is:

$$H_2O \text{ in anode} = 558449 \text{ A} \times \frac{1}{4e^-} \times \frac{96485 \text{ C}}{\text{mol}} \times \frac{0.018 \text{ kg}}{\text{mol}} \times \frac{0.2642 \text{ gal}}{\text{kg}} \times \frac{86400 \text{ s}}{\text{day}} = 594.718 \frac{\text{gal}}{\text{day}}$$

**Water Cost:**

$$\text{Water cost} = 594.718 \frac{\text{gal}}{\text{day}} \times \frac{0.0054 \text{ USD}}{\text{gal}} \times \frac{1}{1000 \text{ kg/day}} = 0.003 \text{ USDkgNH}_3^{-1}$$

**Total cost:**

$$\begin{aligned} \text{Total cost} &= 0.632 \text{ USDkgNH}_3^{-1} + 0.201 \text{ USDkgNH}_3^{-1} + 0.014 \text{ USDkgNH}_3^{-1} \\ &+ 0.057 \text{ USD kgNH}_3^{-1} + 0.697 \text{ USD kgNH}_3^{-1} + 0.07 \text{ USD kgNH}_3^{-1} + 0.003 \text{ USDkgNH}_3^{-1} \\ &= 1.674 \text{ USDkgNH}_3^{-1} \end{aligned}$$

When dilute nitrate-contaminated water is considered as the feed, nitrate pre-concentration introduces

an additional cost. Concentrating  $\text{NO}_3^-$  from 0.5 mM to 0.1 M requires an approximately 200-fold enrichment.<sup>21,22</sup> Based on reported electro dialysis energy consumption and extrapolation to this concentration factor, the additional electricity demand is estimated to be approximately 28 kWh  $\text{kgNH}_3^{-1}$ , corresponding to 0.84 USD  $\text{kgNH}_3^{-1}$  at an electricity price of 0.03 USD  $\text{kWh}^{-1}$ . Accordingly, the ammonia production cost would increase from 1.674 to approximately 2.514 USD  $\text{kgNH}_3^{-1}$ .

**Table S6** Comparing the performance of our work with other reported electrocatalysts for  $\text{NO}_3\text{RR}$ .

| Material   | electrolyte                              | Potential (V) | Faradic Efficiency (%) | Yield Rate ( $\text{mg}\cdot\text{h}^{-1}\cdot\text{mg}^{-1}$ ) | Energy Efficiency (%) | Ref.             |
|--|--|---------------|------------------------|---|-----------------------|------------------|
| A-<br>$\text{CoFe}_{0.25}\text{Cr}_{1.75}\text{O}_4$ | 1M KOH +<br>0.1M $\text{KNO}_3$          | -0.1          | 94                     | 17.23   | 35.4                  | <b>This work</b> |
| CuCo<br>nanosheets                                   | 1M KOH +<br>0.1M $\text{KNO}_3$          | -0.1          | 60                     | 1.00  | 22.7                  | [23]             |
| CoP-CNS  | 1M KOH +<br>0.1M $\text{KNO}_3$          | -0.1          | 58                     | 0.80  | 21.9                  | [24]             |
| NiFe-LDH   | 1M KOH +<br>0.1M $\text{KNO}_3$          | -0.1          | 80                     | 3.08  | 30.2                  | [25]             |
| $\text{Ni}_{0.75}\text{Fe}_{0.25}(\text{OH})_2$      | 1M KOH +<br>0.1M $\text{KNO}_3$          | -0.1          | 75                     | 1.28  | 28.35                 | [26]             |
| NiNC   | 0.1 M<br>NaOH + 0.5<br>M $\text{NaNO}_3$ | -0.1          | 55                     | 0.12  | 21.04                 | [27]             |
| CuNC   | 0.1 M<br>NaOH + 0.5<br>M $\text{NaNO}_3$ | -0.1          | 20                     | 0.50  | 5.98                  | [27]             |
| Fe-PPy   | 0.1 M KOH<br>+ 0.1 M<br>$\text{KNO}_3$   | -0.3          | 100                    | 1.02  | 35.12                 | [28]             |
| CrNC   | 0.05 M<br>PBS + 0.16<br>M $\text{KNO}_3$ | -0.2          | 92                     | 0.34  | 28.94                 | [29]             |
| MnNC   | 0.05 M<br>PBS + 0.16<br>M $\text{KNO}_3$ | -0.2          | 90                     | 0.05  | 27.68                 | [29]             |
| FeNC   | 0.05 M<br>PBS + 0.16<br>M $\text{KNO}_3$ | -0.2          | 75                     | 0.02  | 23.25                 | [29]             |
| CuNC   | 0.05 M<br>PBS + 0.16<br>M $\text{KNO}_3$ | -0.2          | 82                     | 0.07  | 26.25                 | [29]             |

|                       |  |      |    |       |       |      |
|-----------------------|--|------|----|-------|-------|------|
| MoNC                  | 0.05 M<br>PBS + 0.16<br>M KNO <sub>3</sub>             | -0.2 | 55 | 0.07  | 17.24 | [29] |
| PdNC                  | 0.05 M<br>PBS + 0.16<br>M KNO <sub>3</sub>             | -0.2 | 65 | 0.05  | 18.50 | [29] |
| LaNC                  | 0.05 M<br>PBS + 0.16<br>M KNO <sub>3</sub>             | -0.2 | 40 | 0.05  | 12.18 | [29] |
| CeNC                  | 0.05 M<br>PBS + 0.16<br>M KNO <sub>3</sub>             | -0.2 | 80 | 0.05  | 24.36 | [29] |
| Cu <sub>2</sub> O NCs | 0.1 M<br>NaSO <sub>4</sub> + 8<br>mM NaNO <sub>3</sub> | -0.3 | 93 | 7.58  | 26.07 | [30] |
| CuCo aerogel          | 1.0 M KOH<br>+ 0.07 M<br>KNO <sub>3</sub>              | -0.2 | 98 | 35.94 | 36.64 | [31] |
| Ru                    | H-B process  | -    | -  | 1.03  | 61    | [32] |

**Table S7** The parameters related to Nyquist plots.

| Sample   | R <sub>s</sub> / Ω | R <sub>ct</sub> / Ω | CPE <sub>dl</sub> |
|--|--------------------|---------------------|-------------------|
| CoFe <sub>0.25</sub> Cr <sub>1.75</sub> O <sub>4</sub>   | 5.02               | 61.79               | 0.955             |
| A-CoFe <sub>0.25</sub> Cr <sub>1.75</sub> O <sub>4</sub> | 5.29               | 10.21               | 0.441             |
| Co <sub>0.8</sub> Fe <sub>0.2</sub> (OH) <sub>2</sub>    | 5.60               | 9.43                | 0.485             |

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