

Supplementary Information

High-Performance LiFePO₄ Regeneration through Na-Induced Lattice Activation and Conductivity Rewiring

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Chemicals and materials

All chemical agents, such as C_2H_5OH and sucrose, were procured from Macklin Company. These chemical reagents were directly applied to recycle discarded LFP cathodes without additional purification steps. The discarded LFP cathode sheets were sourced from a company located in Hunan, China. Meanwhile, LFP cathodes, along with coin cell battery components, were obtained from Guangdong Couldrd New Energy Technology Co., Ltd. The components included coin cells, Celgard 2500 separator, polyvinylidene fluoride (PVDF), carbon black, aluminum (Al) foil, and metal discs. The electrolyte, a mixture of 1 M $LiPF_6$ dissolved in a volumetric ratio of 1:1:1 ethylene carbonate (EC), diethyl carbonate (DEC), and dimethyl carbonate (DMC), was purchased from DoDochem.

Procedure for the regenerated LFP

Harvesting $LiFePO_4$ material

Spent LFP batteries were first discharged in a saturated sodium chloride (NaCl) solution; this process continued until their voltage fell to below 1.0 V. After discharge, the batteries were manually disassembled to separate and collect the separator, as well as the cathode and anode sheets. To prepare spent LFP cathode materials, the pre-cut cathode sheets were soaked in deionized water, which allowed for the detachment of the aluminum (Al) foil from the cathode material. The cathode samples obtained from this step were then placed in an oven and dried at 70 °C for 3 hours to eliminate any residual moisture. Lastly, the dried cathode materials were ground for 5 minutes using a grinding device, resulting in the formation of powdered LFP samples. These powdered samples were designated as spent LFP, abbreviated as SLFP.

Spent LFP regeneration

Initially, the spent LFP was disassembled to obtain spent flakes. Subsequently, Li_2CO_3 and Na_2CO_3 were prepared at mass ratios of 100:0, 97.5:2.5, 95:5, and 90:10. An amount of Li_2CO_3 or Li_2CO_3/Na_2CO_3 1.1 times that corresponding to the lithium deficiency was required. The spent LFP, Li_2CO_3 and Na_2CO_3 were mixed in anhydrous ethanol using a ball-milled for 2 hours. Then, a sand bath at 80 °C was employed to evaporate the ethanol. The resulting product was heated in air at 500 °C to eliminate the conductive agent and binder. Next, 2 g of the oxidized material and 0.3 g of sucrose were ball-milled in 20 ml of anhydrous ethanol at a speed of 400

rpm for 2 hours. The obtained mixture was dried at 50 °C for 3 hours to remove the ethanol. After that, the dried material was preheated at 350 °C for 4 hours under an argon atmosphere, followed by reheating to 650 °C for 8 hours in an inert gas environment, with a heating rate of 5 °C/min.

Cell assembly and electrochemical measurements

The cathode material was mixed with conductive carbon black and PVDF binder in an NMP solvent at a mass ratio of 8:1:1 to form a uniform slurry. The slurry was then cast on an Al foil and vacuum-dried at 80 °C for 8 h. The above electrode film was cut into round discs with a diameter of 12 mm. The CR2025 coin cells were then assembled in an Ar-filled glovebox using Celgard 2400 membrane as the separator, Li metal foil as the counter electrode, and 1 mol L⁻¹ LiPF₆ (EC: DEC: DMC = 1:1:1 as solvent, volume ratio) as the electrolyte. Subsequently, galvanostatic charge/discharge tests were conducted on a LAND CT2001A battery tester in the voltage window of 2.5-4.2 V versus Li/Li⁺. CV with a sweep rate of 0.1 mV S⁻¹ and a voltage range of 2.5-4.2 V and EIS measurements in the frequency range of 0.01 Hz-100 kHz were carried out on a Solartron Analytical instrument.

Instrumentation

ICP-OES tests were conducted on a SHIMADZU ICPE-9000 spectrometer. X-ray diffraction (XRD) analysis was conducted to identify the composition of the synthesized materials. Transmission electron microscopy (TEM), scanning electron microscopy (SEM), and high-angle annular dark-field scanning transmission electron microscopy (HAADF-STEM) were employed to analyze the morphology and structure of the recovered LFP materials. X-ray photoelectron spectroscopy (XPS) measurements were carried out on a Thermo Fischer ESCALAB Xi+ instrument to determine the composition and valence states of the recovered LFP. An inductively coupled plasma optical emission spectrometer (ICP-OES) was used to analyze the elemental content of Li_{0.95}Na_{0.05}FePO₄.

Environmental and economic analysis

The EverBatt model developed by Argonne National Laboratory and the prospective cradle-to-

gate life cycle analysis (LCA) were employed to analyze different recycling routes on a per-unit-mass basis for spent LiFePO₄ batteries. The energy consumption and economic analysis for this work were calculated based on the process parameters obtained in our laboratory. Moreover, hydrometallurgical recycling route, traditional direct recycling route, and this work were calculated based on a combination of the typical process from EverBatt model and reported in literature¹⁻³. The details of the calculations and parameters are shown in Table S2-S10.

The total energy consumption for each recycling route was calculated as formula (1):

$$E_{\text{total}} = \sum_i m_i \times e_{u,i} + \sum_i n_i \times e_{v,i} + j \quad (1)$$

where m_i is the mass of input material i , $e_{u,i}$ is the unit embodied energy of material i (from EverBatt database), n_i is the consumption of input energy i during the process, and $e_{v,i}$ is the unit energy intensity of energy i , j is other input costs, including battery fee, process waste management, labour and fixed assets (from EverBatt database).

The total recycling cost encompasses the costs of materials, energy, and other miscellaneous inputs. It is calculated as formula (2):

$$\text{Recycling cost} = \sum_i m_i \times up_i + \sum_i n_i \times vp_i + k \quad (2)$$

Here, m_i is the mass of input material i , up_i is the unit price of input material i , and vp_i is the unit price of the process energy. The parameter k accounts for other fixed and variable costs, including battery acquisition, waste disposal, labor, and overhead expenses, all of which were derived from the EverBatt model.

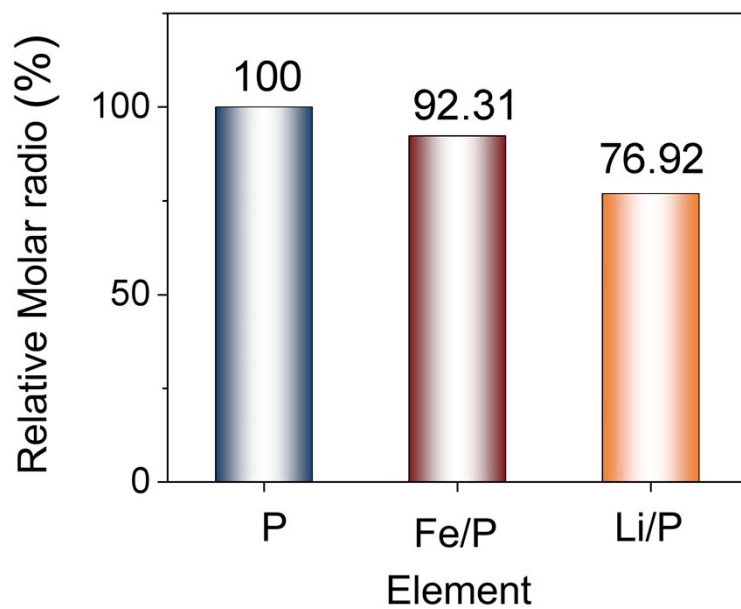
The total revenue generated from the recycled materials was calculated based on the market value of the recovered products. It is calculated as formula (3):

$$\text{Revenue} = \sum_i m_i \times rp_i \quad (3)$$

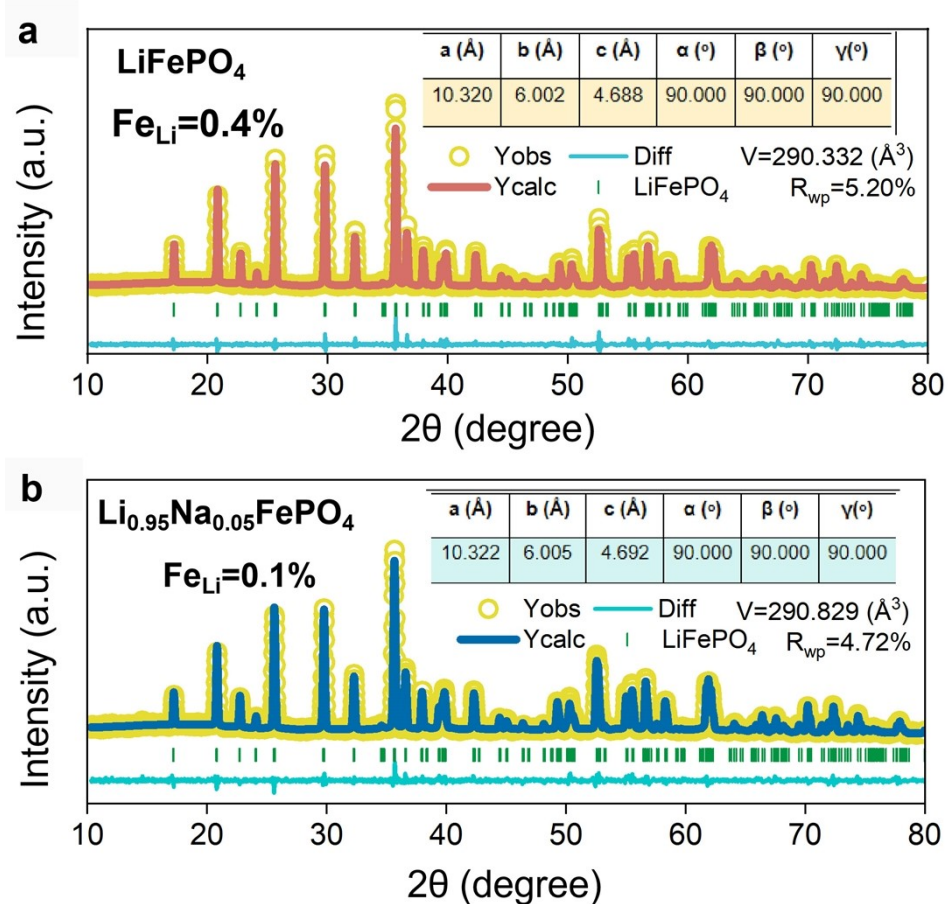
where m_i is the mass of input material i , and rp_i represents its unit market price.

Profit is the difference between revenue and recovered costs (formula (4)):

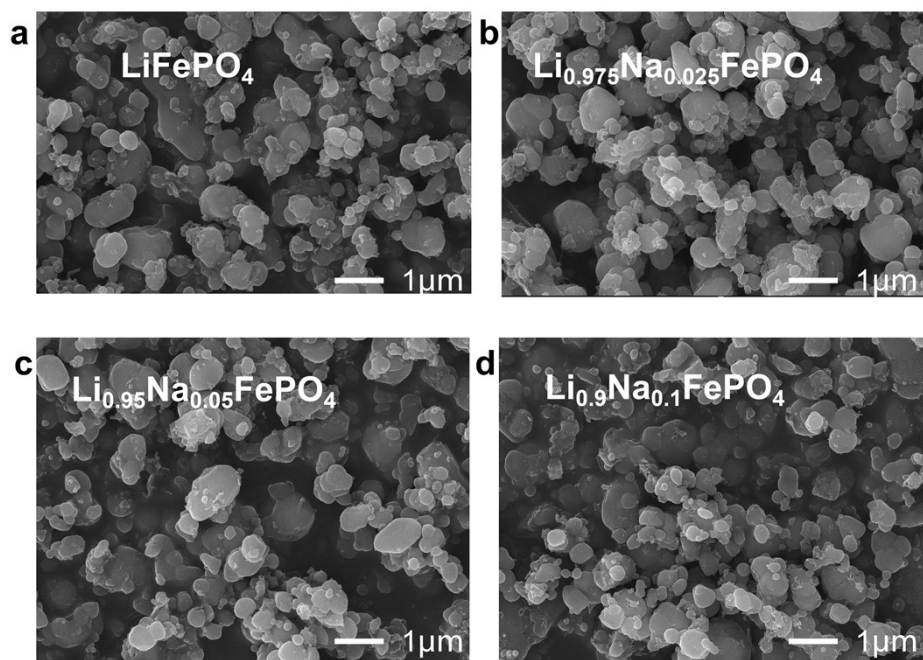
$$\text{Profit} = \text{Revenue} - \text{Recycling cost} \quad (4)$$



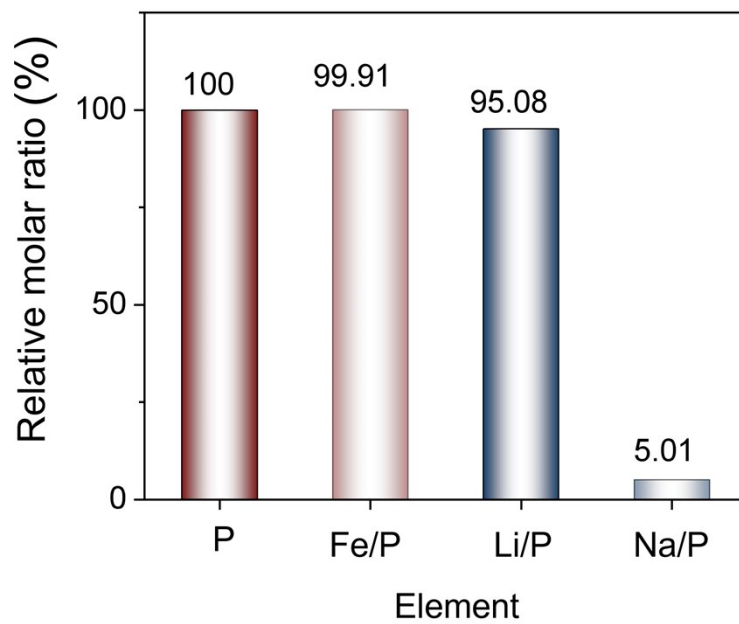
Supplementary Fig. 1 Molar ratio of each element in spent LiFePO₄.



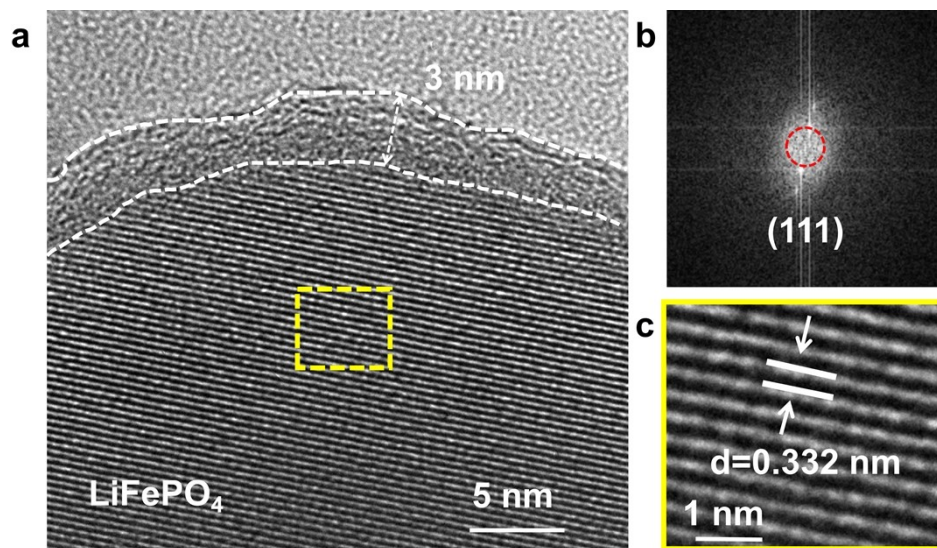
Supplementary Fig. 2 (a) Rietveld-refined XRD patterns of LiFePO₄ (Fe_{Li} = 0.4%). (b) Rietveld-refined XRD patterns of Li_{0.95}Na_{0.05}FePO₄ (Fe_{Li} = 0.1%).



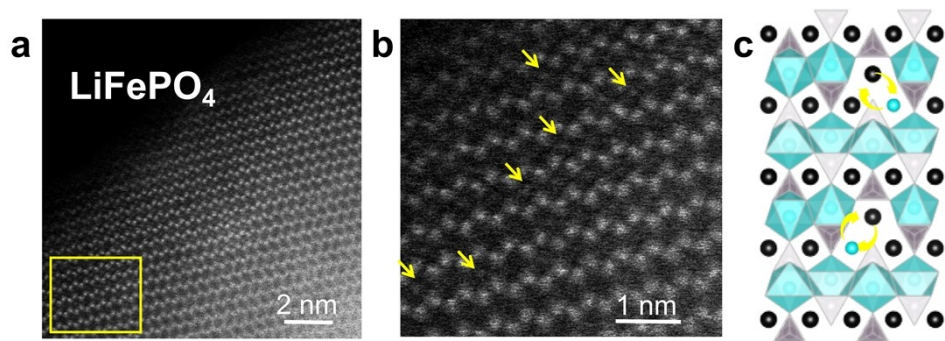
Supplementary Fig. 3 (a) SEM image of LiFePO_4 . (b) SEM image of $\text{Li}_{0.975}\text{Na}_{0.025}\text{FePO}_4$. (c) SEM image of $\text{Li}_{0.95}\text{Na}_{0.05}\text{FePO}_4$. (d) SEM image of $\text{Li}_{0.9}\text{Na}_{0.1}\text{FePO}_4$.



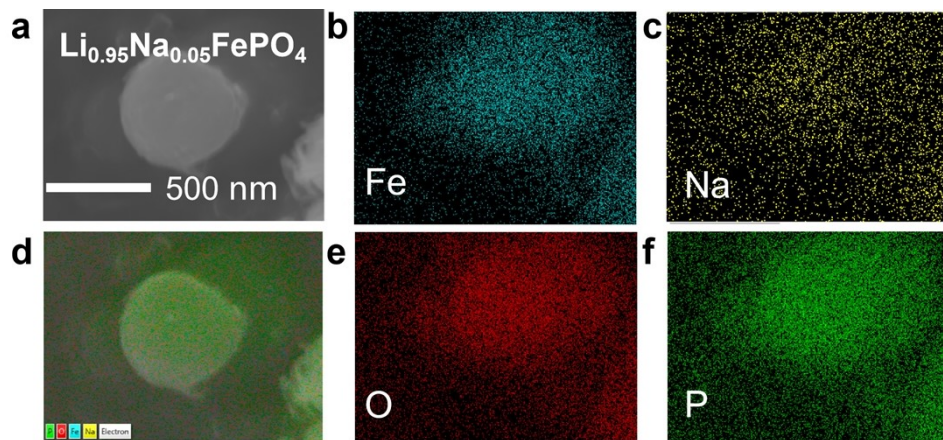
Supplementary Fig. 4 Molar ratio of each element of $\text{Li}_{0.95}\text{Na}_{0.05}\text{FePO}_4$.



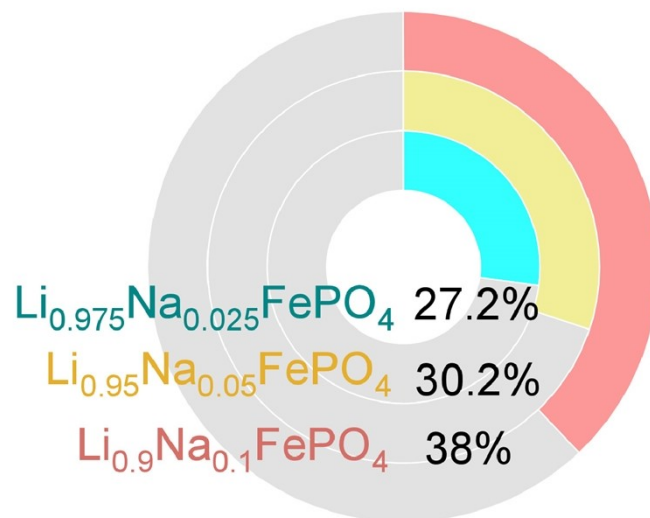
Supplementary Fig. 5 (a) The high-resolution TEM image of LiFePO_4 . (b) the Fast-Fourier-Transform (FFT) pattern of LiFePO_4 . (c) lattice spacing analysis of LiFePO_4 .



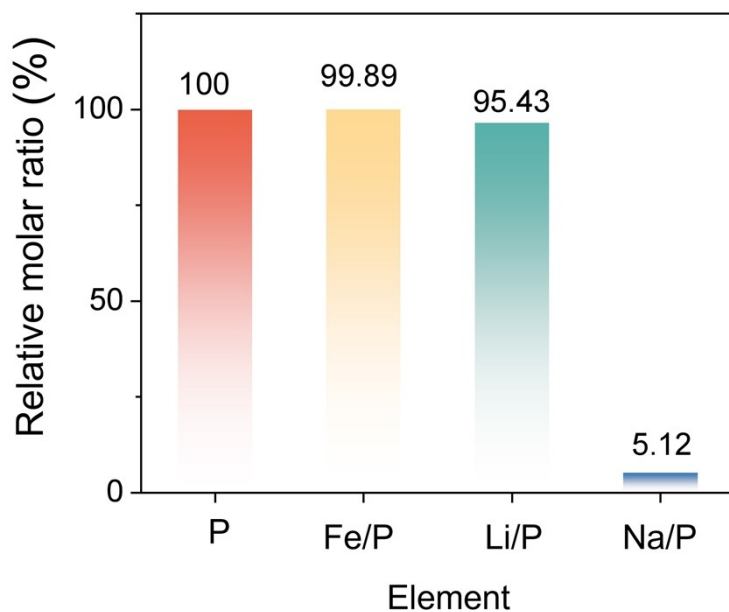
Supplementary Fig. 6 (a) AC STEM-HAADF-EDS mapping images of LiFePO_4 . (b) HRTEM images of LiFePO_4 . (c) Structural representation of Li-Fe anti-sites.



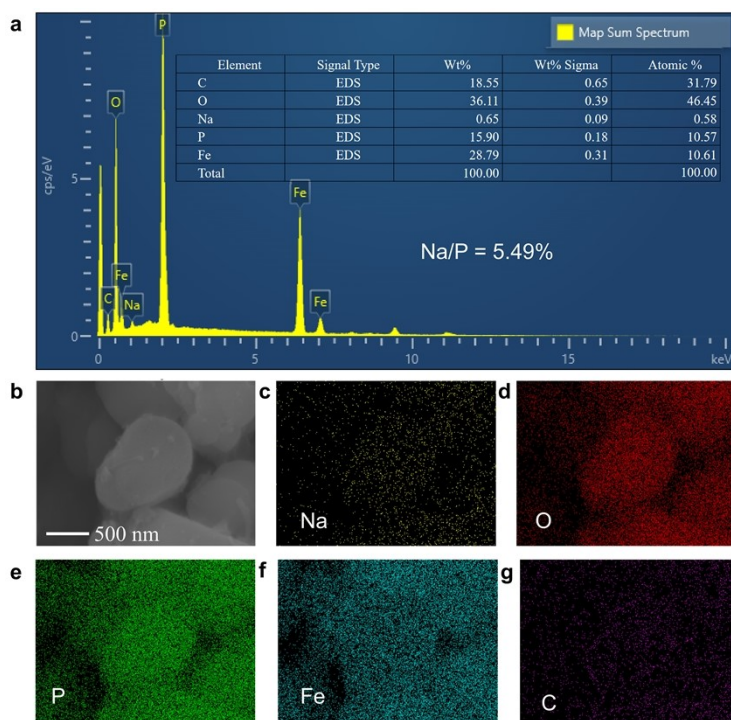
Supplementary Fig. 7 (a) The scanning transmission electron microscopy (STEM) image of $\text{Li}_{0.95}\text{Na}_{0.05}\text{FePO}_4$. (b-f) The corresponding energy-dispersive X-ray spectroscopy (EDS) elemental mapping images of Fe, Na, O, and P in the $\text{Li}_{0.95}\text{Na}_{0.05}\text{FePO}_4$ particle.



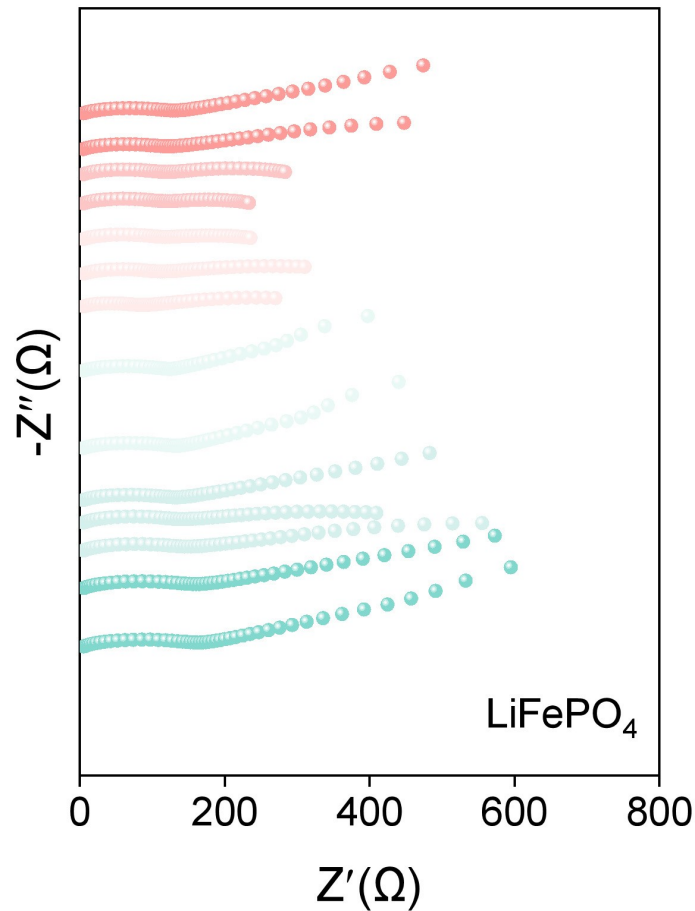
Supplementary Fig. 8 The relative ratio of Fe^{2+} to Fe^{3+} content.



Supplementary Fig. 9 Molar ratio of each element of $\text{Li}_{0.95}\text{Na}_{0.05}\text{FePO}_4$ after charging.



Supplementary Fig. 10 (a) EDS survey spectrum of $\text{Li}_{0.95}\text{Na}_{0.05}\text{FePO}_4$ particle after charging. (b-g) The corresponding EDS elemental mapping images of Fe, Na, O, C, and P in the $\text{Li}_{0.95}\text{Na}_{0.05}\text{FePO}_4$ particle after charging.



Supplementary Fig. 11 The in-situ EIS of cycled LiFePO₄ during charge/discharge.
Supplementary Eq. 1

$$2d \sin\theta = n\lambda$$

In this equation, d is the distance between adjacent parallel crystal planes, θ is the Bragg angle (half the angle between incident and diffracted X-rays), n is the positive integer diffraction order, and λ is the fixed wavelength of the incident X-ray (determined by the testing equipment)⁴.

Supplementary Eq. 2

$$I_p = 2.69 \times 10^5 \times n^{2/3} A D^{1/2} v^{1/2} C_{Li^+}$$

In this equation, I_p is the peak current, n is the number of electrons transferred during the reactions, A is the surface area of active electrodes (1.13 cm²), v indicates the scan rate, and C_{Li^+} is the Li-ions concentration of the LFP lattice⁵.

Supplementary Table 1. The comparison of regenerated LFP samples in previous work and this work.

Samples	Capacity (mAh g ⁻¹ , C)	Capacity retention	Ref.
regenerated LFP	147.9 at 1 C	86% after 500 cycles at 5 C	6
regenerated LFP	144 at 1 C	96% after 500 cycles at 5 C.	7
regenerated LFP	152.5 at 0.1 C	98.7% after 200 cycles at 1 C.	8
regenerated LFP	142.7 at 1 C	no degradation after 200 cycles at 1 C.	9
regenerated LFP	150.5 at 0.5 C	94.9% after 500 cycles at 0.5 C.	10
regenerated LFP	155.6 at 0.1 C	93% after 300 cycles at 1 C.	11
regenerated LFP	142.9 at 1 C	Nearly 100% after 200 cycles at 1 C.	12
regenerated LFP	164.2 at 0.1 C	93.1% after 800 cycles at 5 C.	13
regenerated LFP	150.0 at 0.2 C	82% after 300 cycles at 1 C.	14
regenerated LFP	124.3 at 2.0 C	92.1% after 400 cycles at 2 C.	15
Li _{0.95} Na _{0.05} FePO ₄	116.2 at 5.0 C	99 % after 400 cycles at 5 C.	This work

Supplementary Table 2. The process parameters for hydro process.

Process	Item	Dosage	Unit	Notes	
Crushing and screening	Input	spent LIBs	1.00	kg	1 MJ electricity produces 0.13 kg GHG and 0.67 L water. 1 kg diesel produces 45.6 MJ energy. The data is estimated based on Everbatt 2020. ~5 wt% NaCl solution is adopted for safe discharging. ⁴
		Energy	2.87	MJ	
	Output	LFP powder	0.35	kg	
		Cu/Al/steel	0.4	kg	
		graphite	0.17	kg	
		GHG	0.255	kg	
Acid leaching	Input	LFP powder	0.35	kg	
		H ₂ SO ₄	0.52	kg	
		H ₂ O ₂	0.76	L	
	Output	Energy	12.35	MJ	
		Leaching slag	0.41	kg	
		Leachate	1.48	kg	
Slag purification	Input	GHG	0.406	kg	
		Leaching slag	0.41	kg	

Leachate purification	Output	Energy	0.68	MJ	PH adjusted to 9.0-10.0 for Li ₂ CO ₃ precipitation. The solution degree of Na ₂ CO ₃ is 40 g/100g (30°C).
		FePO ₄	0.33	kg	
		GHG	0.193	kg	
	Input	Leachate	1.48	L	
		Na ₂ CO ₃	0.15	kg	
		NaOH	0.68	kg	
Fabrication	Output	Energy	0.71	MJ	
		Li ₂ CO ₃	0.065	kg	
		GHG	0.284	kg	
Fabrication	Input	FePO ₄	0.33	kg	Recycled FePO ₄ and Li ₂ CO ₃ were mixed and calcined at 700 °C for 6 h under inert atmosphere to regenerate battery-grade LFP cathode material.
		Li ₂ CO ₃	0.065	kg	
		Energy	4.175	MJ	
Fabrication	Output	R-LFP	0.28	kg	
		GHG	0.612	kg	

Supplementary Table 3. Cost analysis of hydro process.

Item	Dosage	Unit	Unit price	Cost (\$)	Data source
Energy	20.941	MJ	0.0186 \$/kWh	0.108	EverBatt
H ₂ SO ₄	0.52	kg	0.15 \$/kg	0.076	SMM
H ₂ O ₂	0.76	kg	0.39 \$/kg	0.298	SMM
NaOH	0.68	kg	0.31 \$/kg	0.213	SMM
Na ₂ CO ₃	0.15	kg	2.16 \$/kg	0.324	SMM
Battery fee	1	kg	3.86	3.86	Mysteel
Process	/	/	/	0.6	EverBatt 2020
Waste management	/	/	/	0.45	EverBatt 2020
Labor	/	/	/	0.52	EverBatt 2020
Fixed assets	/	/	/	0.561	EverBatt 2020
Cost (\$/kg)				7.01	

Supplementary Table 4. The process parameters for direct process.

Process	Item	Dosage	Unit	Notes	
Dismantling	Input	spent LIBs	1.00	kg	1 MJ electricity produces 0.13 kg GHG and 0.67 L water. 1 kg diesel produces 45.6 MJ energy. The data is estimated based on Everbatt 2020. ~5 wt% NaCl solution is adopted for safe discharging.
		Energy	2.87	MJ	
		cathode scrap	0.44	kg	
		separator/steel	0.28	kg	
	Anode scrap	0.26	kg		
	Output	GHG	0.038	kg	

Soaking	Input	cathode sheet	0.44	kg	To separate the active materials from Al foils to decompose the binder, large of deionized water is needed. was preheated at 350 °C for 4 hours under an argon atmosphere, followed by reheating to 650 °C for 8 hours in an inert gas environment, with a heating rate of 5 °C/min.
		Energy	0.156	MJ	
	Output	Water	0.35	kg	
		D-LFP	0.35	kg	
Relithiation/Annealing	Output	Al foil	0.07	kg	
		GHG	0.217	kg	
	Input	D-LFP	0.35	kg	
		Li ₂ CO ₃	0.02	kg	
		Sucrose	0.06	kg	
Output	Energy	1.422	MJ		
	R-LFP	0.31	kg		
		GHG	0.695	kg	

Supplementary Table 5. Cost analysis of direct approach.

Item	Dosage	Unit	Unit price	Cost (\$)	Data source
Energy	4.448	MJ	0.0186 \$/kWh	0.023	EverBatt 2020
Sucrose	0.06	kg	0.43 \$/kg	0.026	SMM
Li ₂ CO ₃	0.02	kg	13.8 \$/kg	0.276	SMM
Battery fee	1	kg	3.86 \$/kg	3.86	Mysteel
Process	/	/	/	0.42	EverBatt 2020
Waste management	/	/	/	0.6	EverBatt 2020
Labor	/	/	/	0.38	EverBatt 2020
Fixed assets	/	/	/	0.215	EverBatt 2020
Cost (\$/kg)				5.8	

Notes: SMM (<https://www.smm.cn/>); Mysteel (<https://m.mysteel.com/>).

Supplementary Table 6. The process parameters for this work.

Process		Item	Dosage	Unit	Notes
Dismantling	Input	spent LIBs	1.00	kg	1 MJ electricity produces 0.13 kg GHG and 0.67 L water. 1 kg diesel produces 45.6 MJ energy. The data is estimated based on Everbatt 2020. ~5 wt% NaCl solution is adopted for safe discharging.
		Energy	2.87	MJ	
		cathode scrap separator/steel	0.44	kg	
		Anode scrap	0.28	kg	
	Output	GHG	0.038	kg	
Soaking	Input	cathode sheet	0.44	kg	To separate the active materials from Al foils to decompose the binder, large of deionized water is needed.
		Energy	0.156	MJ	
		Water	0.35	kg	
	Output	Al foil	0.07	kg	
		GHG	0.217	kg	
Relithiation/Annealing	Input	D-LFP	0.35	kg	was preheated at 350 °C for 4 hours under an argon atmosphere, followed by reheating to 650 °C for 8 hours in an inert gas environment, with a heating rate of 5 °C/min.
		Li ₂ CO ₃	0.015	kg	
		Na ₂ CO ₃	0.007	kg	
		Sucrose	0.06	kg	
	Output	Energy	0.802	MJ	
		R-LFP	0.31	kg	
		GHG	0.395	kg	

Supplementary Table 7. Cost analysis of direct approach.

Item	Dosage	Unit	Unit price	Cost (\$)	Data source	
Energy	3.828	MJ	0.0186	0.020	EverBatt 2020	
			\$/kWh			
	Sucrose	0.06	kg	0.43 \$/kg	0.026	SMM
	Li ₂ CO ₃	0.015	kg	13.8 \$/kg	0.212	SMM
	Na ₂ CO ₃	0.007	kg	2.16 \$/kg	0.015	SMM
Battery fee	1	kg	3.86 \$/kg	3.86	Mysteel	
Process	/	/	/	0.42	EverBatt 2020	
Waste management	/	/	/	0.258	EverBatt 2020	
Labor	/	/	/	0.144	EverBatt 2020	
Fixed assets	/	/	/	0.215	EverBatt 2020	
Cost (\$/kg)				5.17		

Notes: SMM (<https://www.smm.cn/>); Mysteel (<https://m.mysteel.com/>).

Supplementary Table 8. Revenue and profit of different recycling approaches (\$ kg⁻¹, cell).

		Hydro	Direct	This work
Revenue	Al	0.22	0.22	0.22
	LFP	3.99	11.88	14.69
Cost		7.01	5.8	5.17
Profit		-2.8	6.3	9.74

Supplementary Table 9. LCA of different recycling approaches.

	Hydro	Direct	This work
Total energy (MJ kg ⁻¹ , cell)	20.941	4.448	3.828
Fossil fuels	14.265	3.752	3.186
Coal	4.425	2.316	2.154
Natural gas	4.518	0.362	0.315
Diesel (kg kg ⁻¹)	0.115	0.081	0.712
VOC	0.338	0.235	0.208
CO	1.426	0.892	0.816
NOx	3.582	1.914	1.825
PM10	0.235	0.241	0.236
PM2.5	0.188	0.155	0.142
SOx	0.765	1.312	1.245
BC	0.101	0.030	0.027
OC	0.037	0.028	0.026
CH ₄	2.015	2.531	2.486
N ₂ O	0.026	0.033	0.031
CO ₂	1256	1618	1546
CO ₂ (w/C in VOC & CO) (scaled)	1328	1635	1552
GHG (kg kg ⁻¹ cell)	1.75	0.95	0.65
Revenue (\$ kg ⁻¹ , cell)	4.21	12.1	14.91
Cost (\$ kg ⁻¹ , cell)	7.01	5.8	5.17
Profit (\$ kg ⁻¹ , cell)	-2.8	6.3	9.74

Supplementary Table 10. Energy consumption of different recycling methods (MJ kg⁻¹, cell).

Methods	Material input	Energy input
Hydro-	14.512	6.429
Direct	4.036	0.412

Methods	Material input	Energy input
This work	3.472	0.356

Reference

1. Lv, X. W.; Lin, J.; Zhang, X. D.; Huang, Q. R.; Sun, X.; Fan, E. S.; Chen, R. J.; Wu, F. and Li, L., *Adv. Energy Mater.*, 2024, **14**, 2402560.
2. Xu, P.; Dai, Q.; Gao, H.; Liu, H.; Zhang, M.; Li, M.; Chen, Y.; An, K.; Meng, Y. S.; Liu, P.; Lu, J.; Chen, Z., *Joule*, 2020, **4**, 2609-2626.
3. Wang, X. J.; Zheng, S. L.; Zhang, Y.; Zhang, Y.; Qiao, S.; Long, Z. Q.; Zhao, B. and Li, Z. F., *Waste Manage.*, 2022, **153**, 31-40.
4. J. Li, S. Li and Q. Li, *Mater. Res. Innov.*, 2015, **19**, 4.
5. H. Xue, Y. Wu, Z. Wang, Y. Shen, Q. Sun, G. Liu, D. Yin, L. Wang, Q. Li and J. Ming, *ACS Appl. Mater. Interfaces*, 2021, **13**, 40471-40480.
6. D. Tang, G. J. Ji, J. X. Wang, Z. Liang, W. Chen, H. C. Ji, J. Ma, S. Liu, Z. F. Zhuang and G. M. Zhou, *Adv. Mater.*, 2024, **36**, 2309722.
7. J. Tang, H. T. Qu, C. B. Sun, X. Xiao, H. C. Ji, J. X. Wang, J. F. Li, G. J. Ji, X. Zhang, H. M. Cheng and G. M. Zhou, *Adv. Mater.*, 2025, **37**, 2420238.
8. L. Q. Zhang, H. P. Gao, Y. W. Zhu, I. Tran, W. Tang, J. Lin, A. U. Mu, J. L. Wu, W. Li, D. Nordlund and D. Wang, *Adv. Energy Mater.*, 2025, **15**, 2406084.
9. L. Yang, B. C. Zhang, S. Chen, Q. Pan, W. Y. Li, C. L. Gan, W. T. Deng, G. Q. Zou, H. S. Hou and J. Liu, *Chem. Commun.*, 2024, **60**, 9384-9387.
10. S. P. Hao, Y. L. Lv, Y. Zhang, S. W. Liu, Z. L. Tan, W. Liu, Y. G. Xia, W. Yin, Y. Q. Liao, H. J. Ji and M. Liu, *Energy Environ. Sci.*, 2025, **18**, 3750-3760.
11. Y. X. Lin, T. S. Wang, C. C. Gao, X. X. Zhang, W. Yu, M. Wang, C. Yang and J. H. Zhang, *Adv. Sci.*, 2025, **12**, 2504683.
12. Y. Y. Li, Q. F. Liu, W. Q. Yu, C. C. Li, Z. T. Fei, Q. Meng and P. Dong, *Sep. Purif. Technol.*, 2025, **370**, 133059.
13. S. R. Nie, Y. H. Xia, Y. Z. Xiao, W. H. Lin, G. Y. Yang, W. L. Peng, S. K. Peng, F. B. Meng, R. Z. Hu and B. Yuan, *ACS Appl. Mater. Interfaces*, 2025, **17**, 21257-21268.
14. T. S. Wang, C. C. Gao, Z. Q. Zheng, W. Yu, M. Wang, C. Yang and J. H. Zhang, *Adv. Funct. Mater.*, 2025, **35**, 2502930.
15. Y. Y. Liu, J. Bai, R. Y. Shi, P. Y. Wang, K. Xiao, S. Y. Wang, S. Y. Qiu, X. L. Wang, X. B. Zhu, K. S. Yang and M. Liu, *Adv. Mater.*, 2025, e11246.
16. J. Lin, E. Fan, X. Zhang, Z. Li, Y. Dai, R. Chen, F. Wu and L. Li, *Adv. Energy Mater.*, 2022, **12**, 2201174.