

# A Simple and Robust Method to Quantify Exciton Dissociation Efficiency with High Precision in Non-Fullerene Organic Solar Cells

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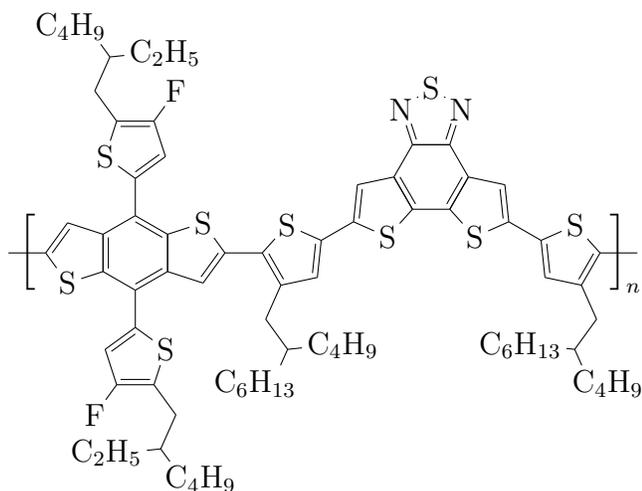
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## S1. CHEMICAL DEFINITIONS

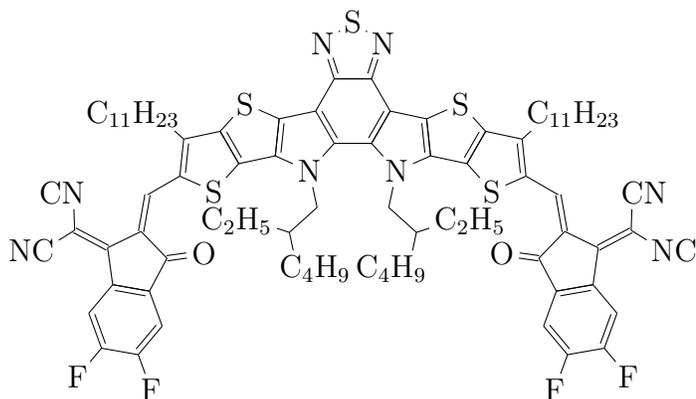
- D18:Y6

- D18: Poly[dithieno[3',2':3,4;2'',3'':5,6]benzo[1,2-c][1,2,5]thiadiazole(DTBT)]; purchased from *1-Material*



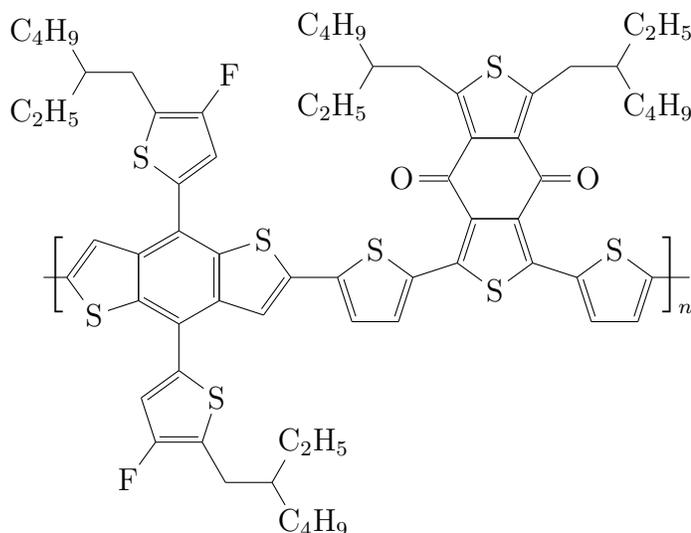
- Y6

- 2,2'-[[12,13-Bis(2-butyloctyl)-12,13-dihydro-3,9-2,2'-[[12,13-Bis(2-ethylhexyl)-12,13-dihydro-3,9-diundecylbisthieno[2'',3'':4',5']thieno[2',3':4,5]pyrrolo[3,2-e:2',3'-g][2,1,3]benzothiadiazole-2,10-diyl]bis[methylidyne(5,6-difluoro-3-oxo-1H-indene-2,1(3H)-diylidene)]]bis[propanedinitrile]; purchased from *1-Material*

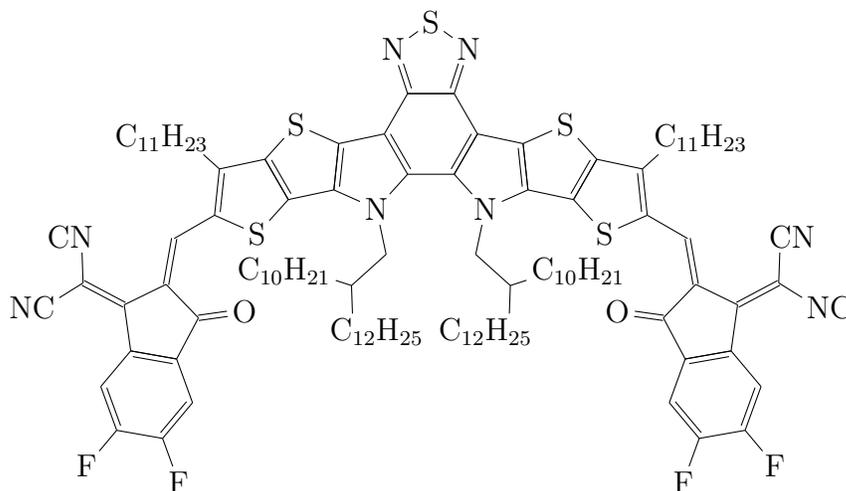


- PM6:DTY6

- PBDB-T-2F (**PM6**): Poly[(2,6-(4,8-bis(5-(2-ethylhexyl-3-fluoro)thiophen-2-yl)-benzo[1,2-b:4,5-b']dithiophene))-alt-(5,5-(1',3'-di-2-thienyl-5',7'-bis(2-ethylhexyl)benzo[1',2'-c:4',5'-c']dithiophene-4,8-dione)]; purchased from *1-Material*



- BTP-4F-24 (**DTY6**): 2,2'-((2Z,2'Z)-((12,13-bis(2-decylteradecyl)-3,9-diundecyl-12,13-dihydro-[1,2,5]thiadiazolo[3,4-e]thieno[2'',3'':4',5']thieno[2',3':4,5]pyrrolo[3,2-g]thieno[2',3':4,5]thieno[3,2-b]indole-2,10-diyl)bis(methanylylidene))bis(5,6-difluoro-3-oxo-2,3-dihydro-1H-indene-2,1-diylidene))dimalononitrile; purchased from *1-Material*



## S2. SOLAR CELL FABRICATION

The solar cells were built according to the stack ITO/PEDOT:PSS/PAL/PDIN/Silver using glass substrates (25 mm × 25 mm × 1 mm). The substrates were cleaned in ultrasonic baths of acetone, isopropanol and deionized water. For the transparent bottom electrode, Indium Tin Oxide (ITO) was deposited via sputtering to achieve a thickness of 170 nm. PALs were processed via spin coating under nitrogen atmosphere. D18:Y6 was dissolved with a

concentration of  $9 \text{ mg mL}^{-1}$  in chloroform and PM6:DTY6 with  $16 \text{ mg mL}^{-1}$  in o-xylene, both with the varying donor:acceptor ratios as provided in the main manuscript.

The blends were deposited via spin-coating. Serving as an electron transport layer, PDIN (purchased from Ossila) was dissolved in methanol with a concentration of  $2 \text{ mg mL}^{-1}$ , adding 0.3 vol% acetic acid (p.a. grade from Sigma Aldrich). It was deposited via spin-coating at 4000 rpm producing a 6 nm thick layer. Finally, a 100 nm thick layer of silver was deposited via thermal evaporation at a pressure of  $< 5 \times 10^{-5}$  mbar. The active area of a solar cell reads  $0.0925 \text{ cm}^2$ , limited by the contact area of the electrodes silver and ITO, respectively.

### **S3. CURRENT-VOLTAGE CHARACTERISTICS**

The current-voltage curves were recorded with a Keithley 2400 sourcemeter while illuminated with a sun simulator (Newport SP94063A-SR1-167, simulated AM1.5G, corrected for spectral mismatch). The cells were measured under nitrogen atmosphere at room temperature (kept approximately constant via fan). The  $JV$  sweeps were performed from  $-1 \text{ V}$  to  $1 \text{ V}$  obtaining 50 data points with dwell times of 50 ms and integrating over 1 NPLC (20 ms).

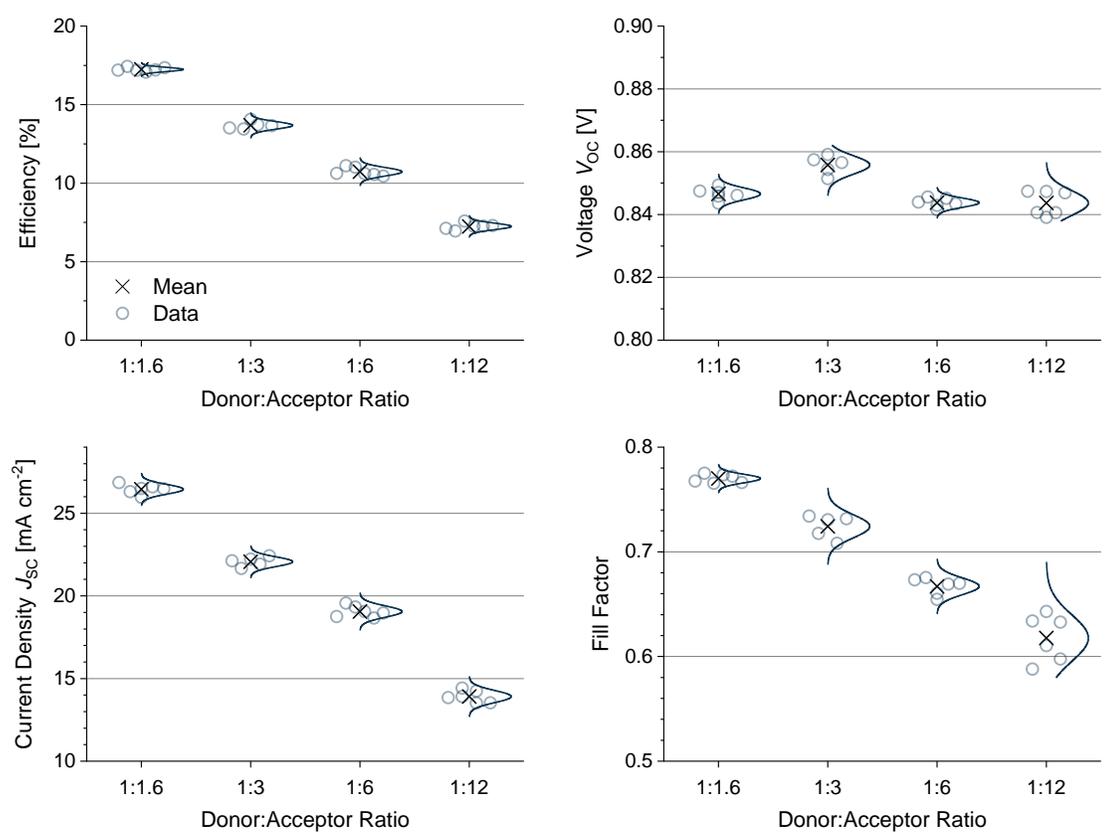


FIG. S1: Figures of merit for the D18:Y6 solar cells.

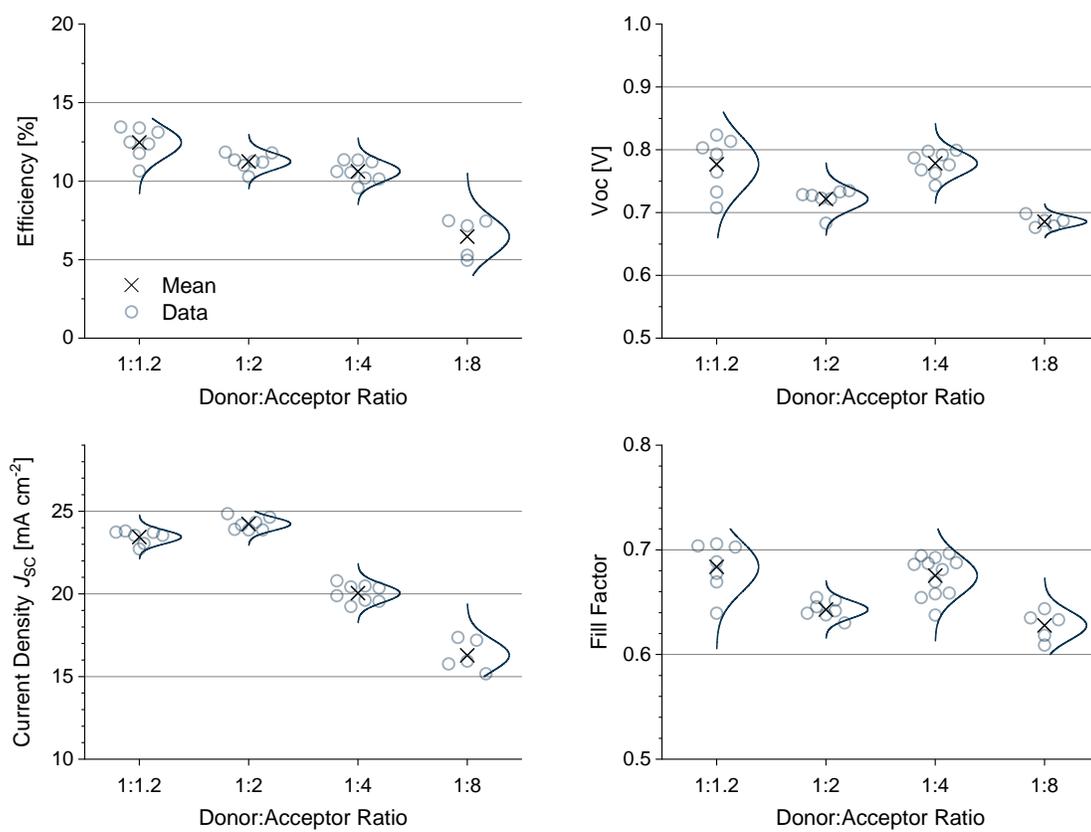


FIG. S2: Figures of merit for the PM6:DTY6 solar cells.

#### S4. PHOTOLUMINESCENCE MEASUREMENTS

All photoluminescence (PL) measurements were performed under inert atmosphere. For steady-state PL characterization, the devices were illuminated with a continuous-wave 532 nm laser. The beam was expanded using a TopHat beam converter to ensure homogeneous illumination of the active area. The emitted PL was filtered using a 600 nm long-pass filter and directed onto the entrance slit of a Czerny–Turner spectrograph (*Andor Shamrock 193i*) equipped with an InGaAs photodiode array detector (*Andor iDus DU490A*) cooled to  $-50^{\circ}\text{C}$ . Spectral response correction was applied using a calibrated tungsten reference lamp measured by *Fraunhofer CalLab PV Cells*. The excitation intensity corresponding to “1 sun” equivalent illumination was determined by adjusting the laser power such that the measured short-circuit current density ( $J_{\text{SC}}$ ) matched that obtained under solar simulator illumination (AM1.5G, corrected for spectral mismatch).

#### S5. OPTICAL MEASUREMENTS AND SIMULATIONS

Optical properties and current generation were simulated using the transfer matrix method as implemented in the *CODE/SCOUT* software package developed by W. Theiss. This method simulates light propagation through multiple layers, accounting for multiple reflections at interfaces and interference effects. This approach enables accurate modeling of reflectance ( $R$ ), transmittance ( $T$ ), and absorptance ( $A$ ) spectra.

Experimentally, reflection, transmission, and absorption spectra were recorded in the wavelength range of 280–1200 nm using a *PerkinElmer Lambda 950 UV/Vis/NIR* spectrophotometer equipped with an integrating sphere. Single layers of each material were prepared on glass substrates, and their thicknesses were determined using a *Veeco Dektak 150* stylus profilometer.

Based on these measurements, the complex refractive index spectra ( $n$  and  $k$ ) were parameterized by fitting a Kim oscillator model in *SCOUT*. The obtained complex refractive indices were then imported into a multilayer model representing the full solar cell stack. From this model, the wavelength-dependent absorptance of the photoactive layer,  $A_{\text{PAL}}(\lambda)$ , was obtained.

## S6. RESULTS FOR EXCITON DISSOCIATION EFFICIENCY WITH THE DONOR-ACCEPTOR VARIATION USING SIMULATED LAYER ABSORPTANCE

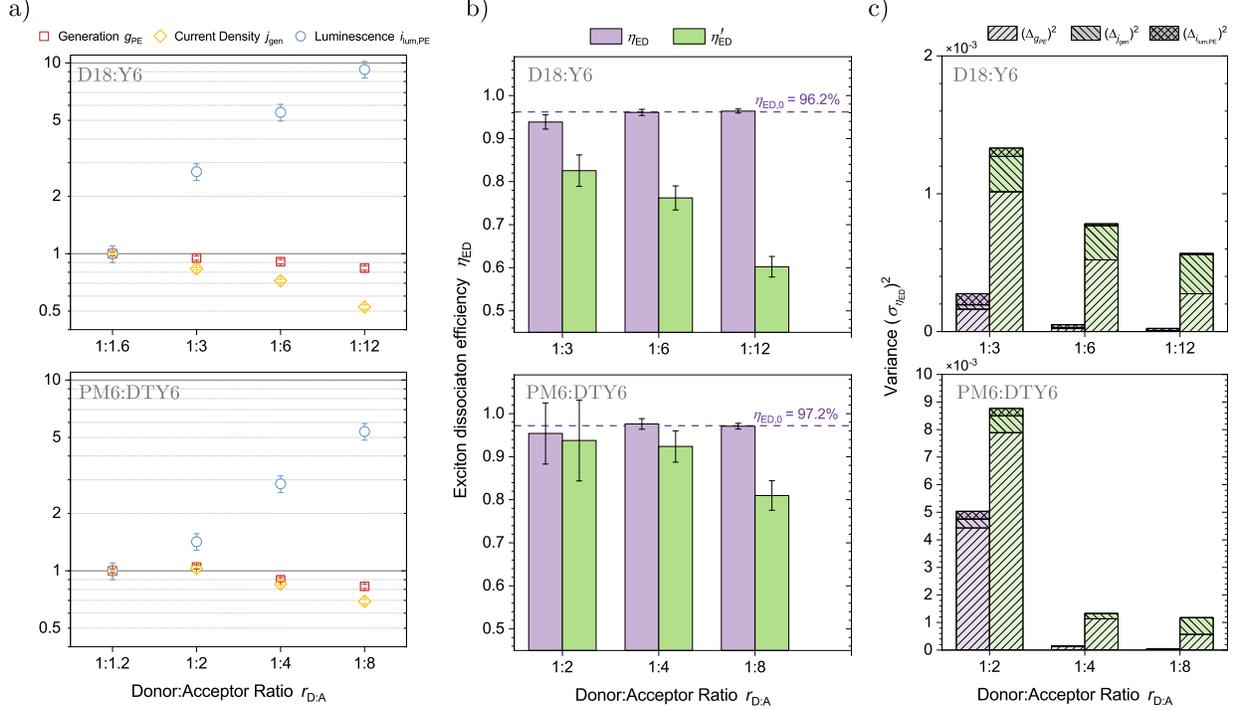


FIG. S3: Similar to Figure 5 in the main manuscript: Results for D18:Y6 (top row) and PM6:DTY6 (bottom row). (a) Evolution of the normalized quantities: integrated photogeneration of excitons  $g_{PE}$  (red) from layer absorptance simulation, generated current density  $j_{gen}$  (yellow), and exciton photoluminescence  $i_{lum,PE}$  (blue) as a function of the donor–acceptor ratio. (b) Exciton dissociation efficiencies of the reference devices ( $\eta_{ED}$ , purple) and the comparative devices ( $\eta'_{ED}$ , green), with the weighted mean shown as a dashed line. (c) Variance analysis of the values shown in (b), with the contributing uncertainty components from  $g_{PE}$ ,  $j_{gen}$ , and  $i_{lum,PE}$  encoded in the stacked bars. The results for the weighted mean of the obtained  $\eta_{ED}$  values are  $96.2 \pm 0.4$  for D18:Y6 and  $97.2 \pm 0.6$  for PM6:DTY6.

## S7. ERROR ESTIMATION FOR EXCITON DISSOCIATION EFFICIENCIES

The uncertainty in the calculated exciton dissociation efficiencies  $\eta_{ED}$  and  $\eta'_{ED}$  was evaluated by Gaussian error propagation. For all quantities, the standard deviations  $\sigma_x$  were determined from either repeated experimental measurements ( $i_{lum,PE}$  and  $j_{gen}$ ) or from systematic deviation if exceeding the statistical uncertainty ( $g_{PE}$ , see main text). According to the Gaussian law of error propagation, the total variance of  $\eta_{ED}$  is obtained as the quadratic

sum of all independent contributions:

$$\sigma_{\eta_{\text{ED}}}^2 = \underbrace{\left(\frac{\partial\eta_{\text{ED}}}{\partial g_{\text{PE}}}\sigma_{g_{\text{PE}}}\right)^2}_{\Delta_{g_{\text{PE}}}^2} + \underbrace{\left(\frac{\partial\eta_{\text{ED}}}{\partial j_{\text{gen}}}\sigma_{j_{\text{gen}}}\right)^2}_{\Delta_{j_{\text{gen}}}^2} + \underbrace{\left(\frac{\partial\eta_{\text{ED}}}{\partial i_{\text{lum,PE}}}\sigma_{i_{\text{lum,PE}}}\right)^2}_{\Delta_{i_{\text{lum,PE}}}^2}. \quad (1)$$

Here,  $\Delta_x = \frac{\partial\eta_{\text{ED}}}{\partial x}\sigma_x$  denotes the standard uncertainty contribution from each variable  $x$ , and  $\Delta_x^2$  its corresponding variance contribution, as depicted in Figure 5c of the main manuscript. The total propagated uncertainty is therefore

$$\sigma_{\eta_{\text{ED}}} = \sqrt{\Delta_{g_{\text{PE}}}^2 + \Delta_{j_{\text{gen}}}^2 + \Delta_{i_{\text{lum,PE}}}^2}. \quad (2)$$

### Error estimation for the reference efficiency $\eta_{\text{ED}}$

For the reference morphology, the exciton dissociation efficiency is defined as:

$$\eta_{\text{ED}} = \frac{g_{\text{PE}} - i_{\text{lum,PE}}}{j_{\text{gen}} - i_{\text{lum,PE}}}. \quad (3)$$

The individual variance contributions are then given by:

$$\Delta_{g_{\text{PE}}}^2 = \left[ \frac{1}{j_{\text{gen}} - i_{\text{lum,PE}}} \sigma_{g_{\text{PE}}} \right]^2, \quad (4)$$

$$\Delta_{j_{\text{gen}}}^2 = \left[ \frac{i_{\text{lum,PE}} - g_{\text{PE}}}{(j_{\text{gen}} - i_{\text{lum,PE}})^2} \sigma_{j_{\text{gen}}} \right]^2, \quad (5)$$

$$\Delta_{i_{\text{lum,PE}}}^2 = \left[ \frac{g_{\text{PE}} - j_{\text{gen}}}{(j_{\text{gen}} - i_{\text{lum,PE}})^2} \sigma_{i_{\text{lum,PE}}} \right]^2. \quad (6)$$

### Error estimation for the comparative efficiency $\eta'_{\text{ED}}$

For the comparative morphology, the exciton dissociation efficiency is given by:

$$\eta'_{\text{ED}} = \frac{j_{\text{gen}}}{g_{\text{PE}}} \cdot \frac{g_{\text{PE}} - i_{\text{lum,PE}}}{j_{\text{gen}} - i_{\text{lum,PE}}}. \quad (7)$$

The corresponding variance contributions read:

$$\Delta_{g_{\text{PE}}}^2 = \left[ \frac{-i_{\text{lum,PE}} j_{\text{gen}}}{g_{\text{PE}}^2 (i_{\text{lum,PE}} - j_{\text{gen}})} \sigma_{g_{\text{PE}}} \right]^2, \quad (8)$$

$$\Delta_{j_{\text{gen}}}^2 = \left[ \frac{i_{\text{lum,PE}} (i_{\text{lum,PE}} - g_{\text{PE}})}{g_{\text{PE}} (j_{\text{gen}} - i_{\text{lum,PE}})^2} \sigma_{j_{\text{gen}}} \right]^2, \quad (9)$$

$$\Delta_{i_{\text{lum,PE}}}^2 = \left[ \frac{j_{\text{gen}} (g_{\text{PE}} - j_{\text{gen}})}{g_{\text{PE}} (j_{\text{gen}} - i_{\text{lum,PE}})^2} \sigma_{i_{\text{lum,PE}}} \right]^2. \quad (10)$$

## S8. WEIGHTED MEAN OF EXCITON DISSOCIATION EFFICIENCY

The weighted mean of the exciton dissociation efficiency,  $\eta_{\text{ED}}$ , was determined using inverse-variance weighting, where the individual uncertainties are represented by their standard deviations  $\sigma_{\eta_{\text{ED},i}}$ :

$$\bar{\eta}_{\text{ED}} = \frac{\sum_i \frac{\eta_{\text{ED},i}}{\sigma_{\eta_{\text{ED},i}}^2}}{\sum_i \frac{1}{\sigma_{\eta_{\text{ED},0,i}}^2}}. \quad (11)$$

The corresponding standard uncertainty of the weighted mean is then given by:

$$\sigma_{\bar{\eta}_{\text{ED}}} = \sqrt{\frac{1}{\sum_i \frac{1}{\sigma_{\eta_{\text{ED},0,i}}^2}}}. \quad (12)$$

Here, each individual measurement  $\eta_{\text{ED},0,i}$  is weighted according to the inverse of its variance  $\sigma_{\eta_{\text{ED},0,i}}^2$ , ensuring that more precise measurements contribute more strongly to the mean.

## S9. ERROR PROPAGATION IN CONVENTIONAL OPTICAL SIMULATIONS

The optical simulation approach to directly obtain the reference exciton dissociation efficiency  $\eta_{\text{ED}}$  follows:

$$\eta_{\text{ED}} = \frac{J_{\text{gen}}}{J_{\text{gen,PE}}}, \quad (13)$$

where  $J_{\text{gen}}$  denotes the experimentally derived generation current density (approximated using  $J_{\text{SC}}$ ) and  $J_{\text{gen,PE}}$  the simulated generation current density of photogenerated excitons obtained from optical modeling of the layer stack.

To evaluate the uncertainty in  $\eta_{\text{ED}}$ , both uncertainties in  $J_{\text{gen}}$  and  $J_{\text{gen,PE}}$  must be considered. The experimental uncertainty  $\sigma_{J_{\text{gen}}}$  is symmetric (determined as the standard error on the mean), whereas the simulated current  $J_{\text{gen,PE}}$  exhibits an asymmetric uncertainty caused by variations in layer thickness, resulting in unequal deviations for increased or decreased thickness. Accordingly, both quantities are expressed as

$$J_{\text{gen}} = J_{\text{gen}}^0 \pm \sigma_{J_{\text{gen}}}, \quad (14)$$

$$J_{\text{gen,PE}} = J_{\text{gen,PE}}^0 \begin{matrix} +\sigma_{J_{\text{gen,PE},+}} \\ -\sigma_{J_{\text{gen,PE},-}} \end{matrix}. \quad (15)$$

The standard Gaussian error propagation for a quotient yields

$$\frac{\sigma_{\eta_{\text{ED}}}}{\eta_{\text{ED}}} = \sqrt{\left(\frac{\sigma_{J_{\text{gen}}}}{J_{\text{gen}}}\right)^2 + \left(\frac{\sigma_{J_{\text{gen,PE}}}}{J_{\text{gen,PE}}}\right)^2}. \quad (16)$$

To account for the asymmetric uncertainty in the simulated quantity, the upper and lower bounds of  $\sigma_{\eta_{\text{ED}}}$  are determined separately, by using the smaller simulated current ( $-\sigma_{J_{\text{gen,PE},-}}$ ) for the upper uncertainty and the larger simulated current ( $+\sigma_{J_{\text{gen,PE},+}}$ ) for the lower uncertainty:

$$\sigma_{\eta_{\text{ED},+}} = \eta_{\text{ED}} \sqrt{\left(\frac{\sigma_{J_{\text{gen}}}}{J_{\text{gen}}}\right)^2 + \left(\frac{\sigma_{J_{\text{gen,PE},-}}}{J_{\text{gen,PE}}}\right)^2}, \quad (17)$$

$$\sigma_{\eta_{\text{ED},-}} = \eta_{\text{ED}} \sqrt{\left(\frac{\sigma_{J_{\text{gen}}}}{J_{\text{gen}}}\right)^2 + \left(\frac{\sigma_{J_{\text{gen,PE},+}}}{J_{\text{gen,PE}}}\right)^2}. \quad (18)$$

Here,  $\sigma_{\eta_{\text{ED},+}}$  and  $\sigma_{\eta_{\text{ED},-}}$  represent the upper and lower standard uncertainty bounds, respectively.

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