

Supplementary Information: *Bridging dimensions: Combining one- and two-photon 3D printing for microfluidic device fabrication*

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S1 Design Details

After 1PP (one photon polymerization) channel resolution target characterization (**Figure S1**), the 1PP manifold (**Figure S2**), 1PP adapter (**Figure S3**), and 2PP (two photon polymerization) chip (**Figure S4**) were optimized for seamless integration.

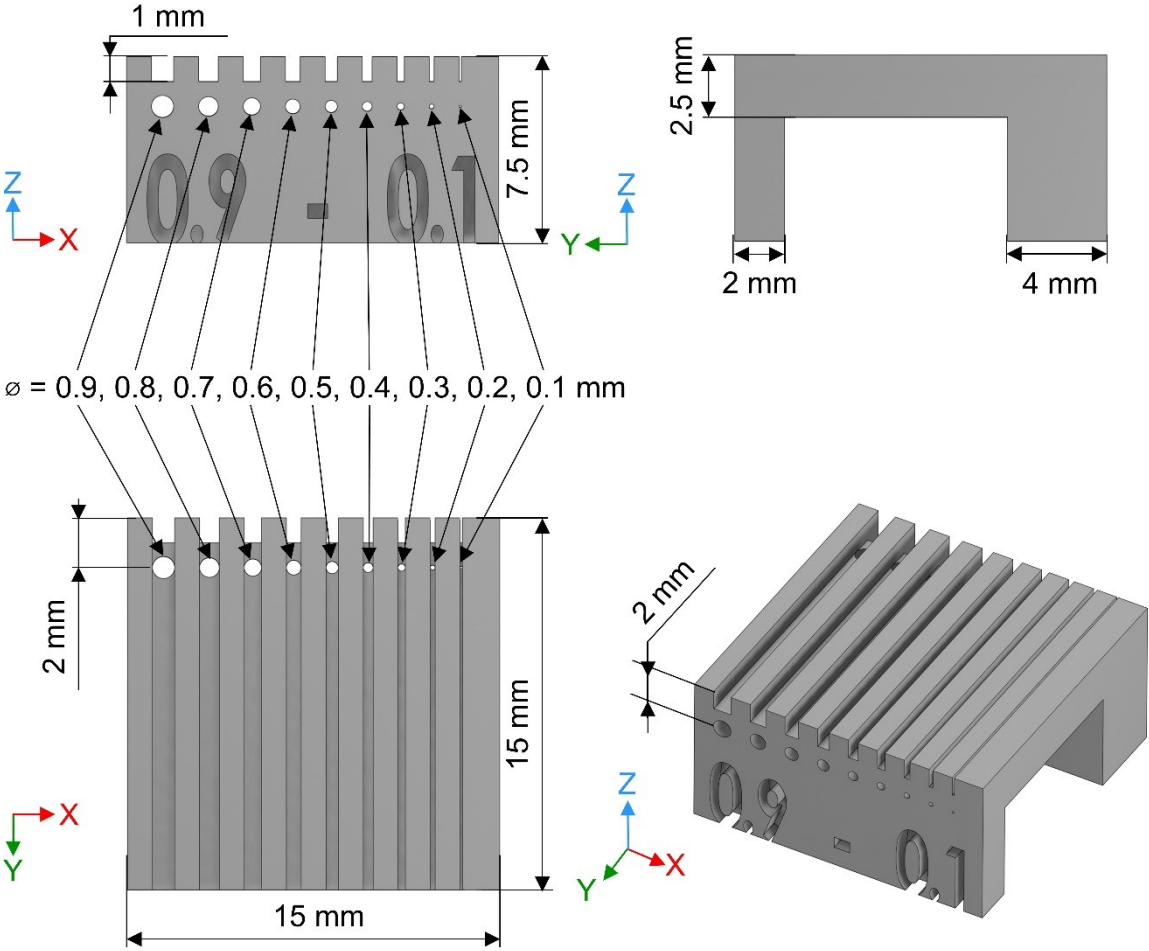


Figure S1: Dimensions of the 1PP channel resolution target to identify smallest reliable microchannel diameter by SLA.

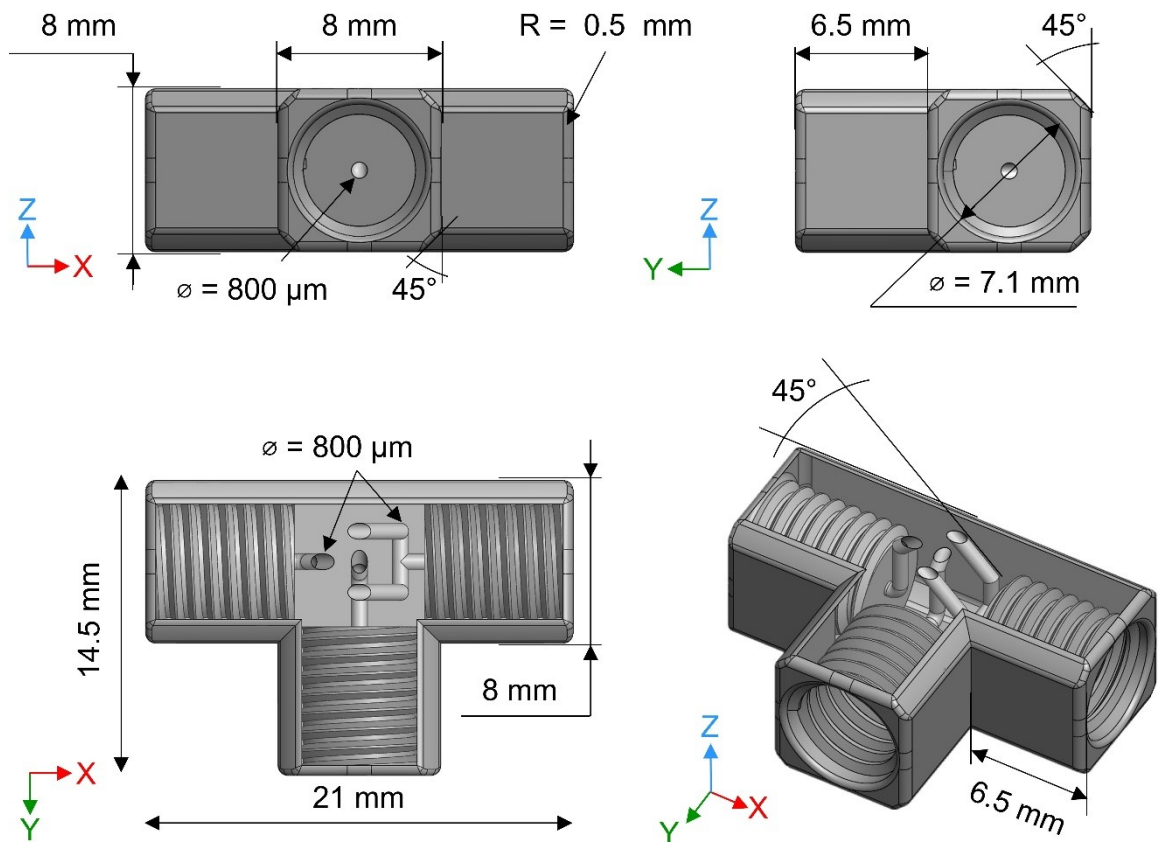


Figure S2: Dimensions of the 1PP manifold. Threads were modeled to receive right-handed 1/4-28 UNF fluid connectors. The thread depth is 9.25 mm. All interface channels to the 2PP chip egress the manifold at a 45° angle.

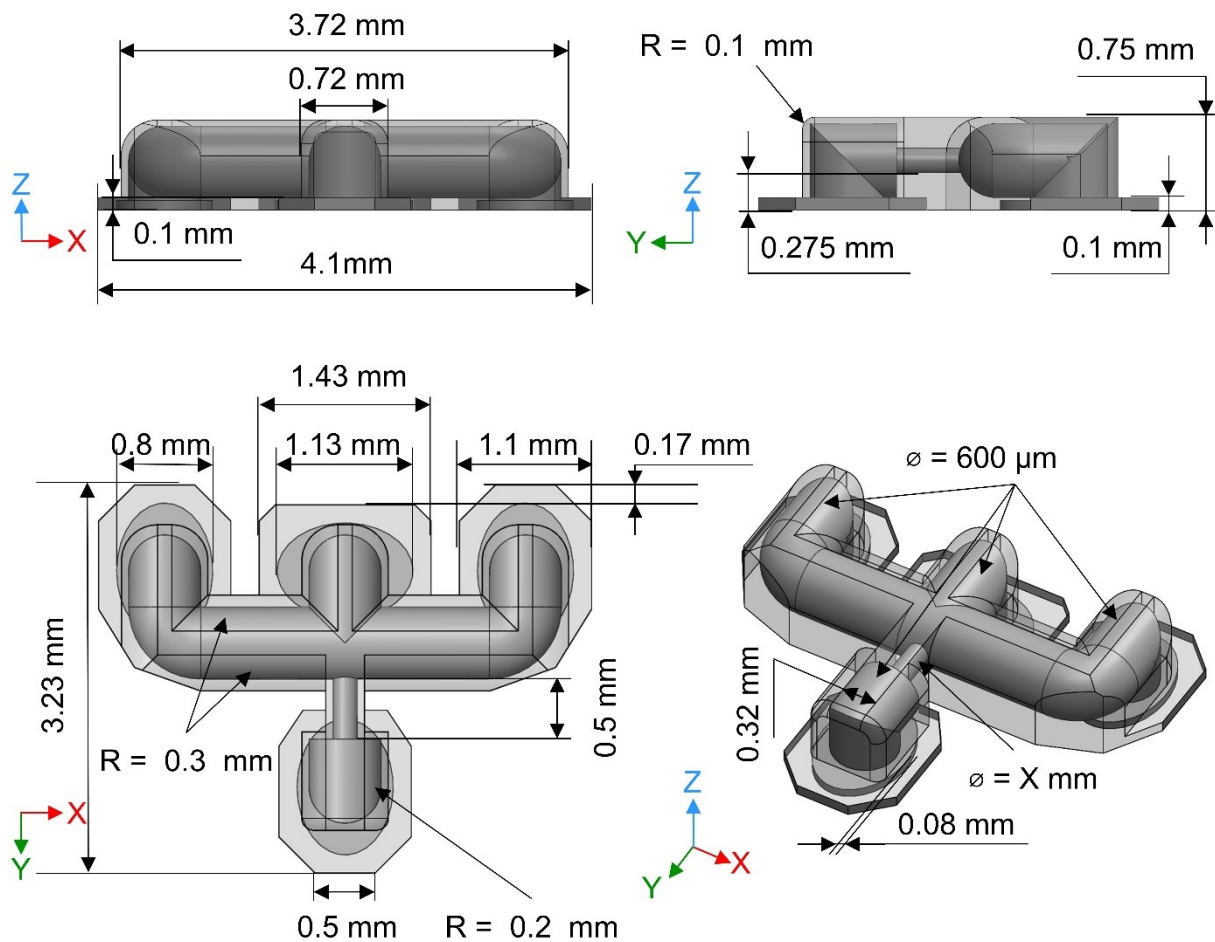


Figure S3: Dimensions of the 2PP chip. Nozzle orifices of $X = 250, 350,$ and $500 \mu\text{m}$ were designed. Flange thickness includes a design tolerance of $\Delta Z = 100 \mu\text{m}$, while tolerances of $\Delta X = 300$ and $\Delta Y = 170 \mu\text{m}$ are included in the flange design itself.

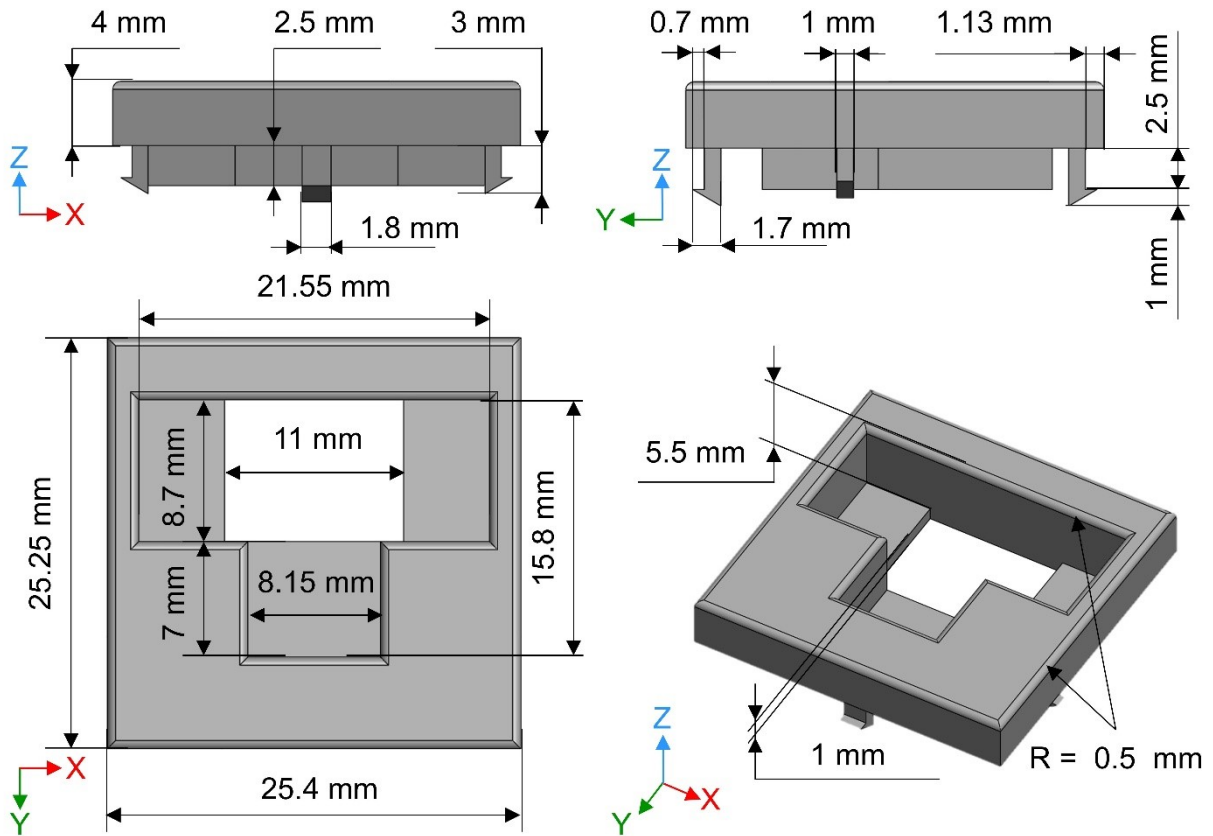


Figure S4: Dimensions of the 1PP adapter. The reusable adapter is secured with a click-fit into the square mounting positions of the 2PP sample holder. Design tolerances were optimized to ensure a snug fit of the 1PP manifold.

S2 1PP Manifold Surface Roughness

The maximum surface height (S_z), the maximum surface peak height (S_p), and maximum surface valley height (S_v) were calculated according to **Equations S1-S3**.

$$S_z = S_p + S_v \quad \text{Eq. S1}$$

$$S_p = \max_A(z_{com}(x, y) - z_{mean}(x, y)) \quad \text{Eq. S2}$$

$$S_v = \left| \min_A(z_{com}(x, y) - z_{mean}(x, y)) \right| \quad \text{Eq. S3}$$

The maximum profile height $R_{z,x}$ or $R_{z,y}$, maximum profile peak height $R_{p,x}$ or $R_{p,y}$ and maximum profile valley height $R_{v,x}$ or $R_{v,y}$ were calculated according to **Equations S4-S9**.

$$R_{z,x} = R_{p,x} + R_{v,x} \quad \text{Eq. S4}$$

$$R_{p,x} = \max_y(z_{com}(x, y) - z_{mean}(x, y)) \quad x = \text{const.} \quad \text{Eq. S5}$$

$$R_{v,x} = \left| \min_y(z_{com}(x, y) - z_{mean}(x, y)) \right| \quad x = \text{const.} \quad \text{Eq. S6}$$

$$R_{z,y} = R_{p,y} + R_{v,y} \quad \text{Eq. S7}$$

$$R_{p,y} = \max_x(z_{com}(x, y) - z_{mean}(x, y)) \quad y = \text{const.} \quad \text{Eq. S8}$$

$$R_{v,y} = \left| \min_x(z_{com}(x, y) - z_{mean}(x, y)) \right| \quad y = \text{const.} \quad \text{Eq. S9}$$

Table S1: Roughness parameters over the whole surface and along cuts at $x = 1190.16 \mu\text{m}$ and $y = 2167.14 \mu\text{m}$ using a 4% cutoff value.

roughness parameter	surface	$x = 1190.16 \mu\text{m}$	$y = 2167.14 \mu\text{m}$
arithmetical mean height / μm	$S_a = 13$	$R_{a,x} = 17$	$R_{a,y} = 10$
maximum height / μm	$S_z = 123$	$R_{z,x} = 64$	$R_{z,y} = 50$
maximum peak height / μm	$S_p = 55$	$R_{p,x} = 42$	$R_{p,y} = 32$
maximum valley height / μm	$S_v = 68$	$R_{v,x} = 22$	$R_{v,y} = 18$

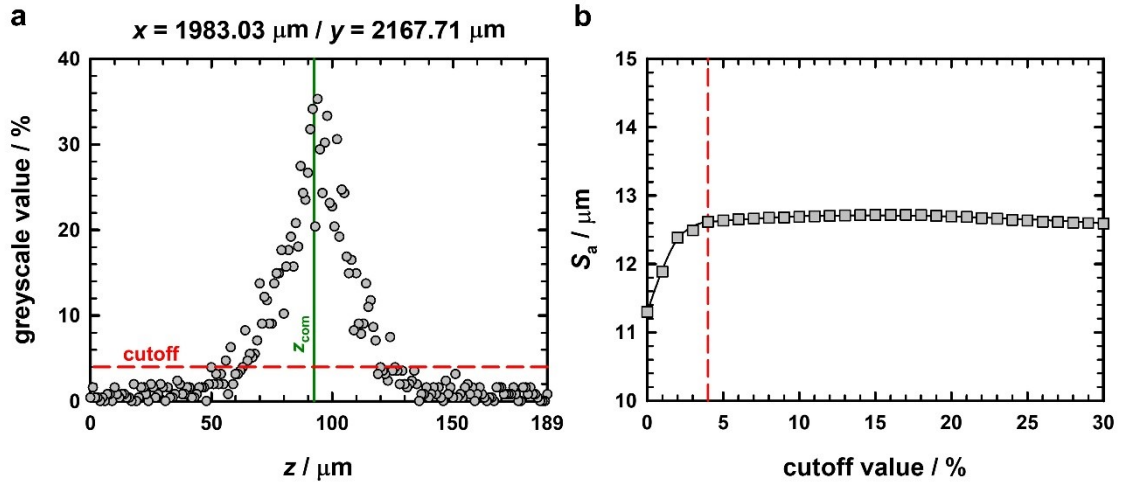


Figure S5: 1PP surface roughness quantification. **(a)** Greyscale values of the pixel at position $X = 1983.03 \mu\text{m}$ and $Y = 2167.71 \mu\text{m}$ plotted as a function of height Z . **(b)** The arithmetical surface mean height S_a plotted as a function of the cutoff value (red dashed line). This cutoff defines the minimum greyscale value required for a pixel to contribute to the surface height z_{com} via a center of mass (green line) quantification. A cut-off value of 4% (red dashed line) was chosen since S_a reaches a plateau of $\approx 13 \mu\text{m}$ for cutoff values above this threshold.

S3 Manufacturing Workflow

The 1PP manifold and adapter are fabricated by 1PP SLA (**Figure S6**). Both are mounted in the 2PP sample holder (**Figure S7**). A tight fit between the 1PP manifold and adapter is important for bottom-up placement in the 2PP DLW 3D printer (**Figure S7e**). After 2PP chip manufacturing, residual resin is pushed out of the microchannels by connecting a syringe via the 1PP manifold and rinsing with isopropanol and PGMEA. A final UV curing step of the completed device is detailed in **Section 4.4**. In addition, an imaging window was introduced to improve optical transparency (**Figure 5**).

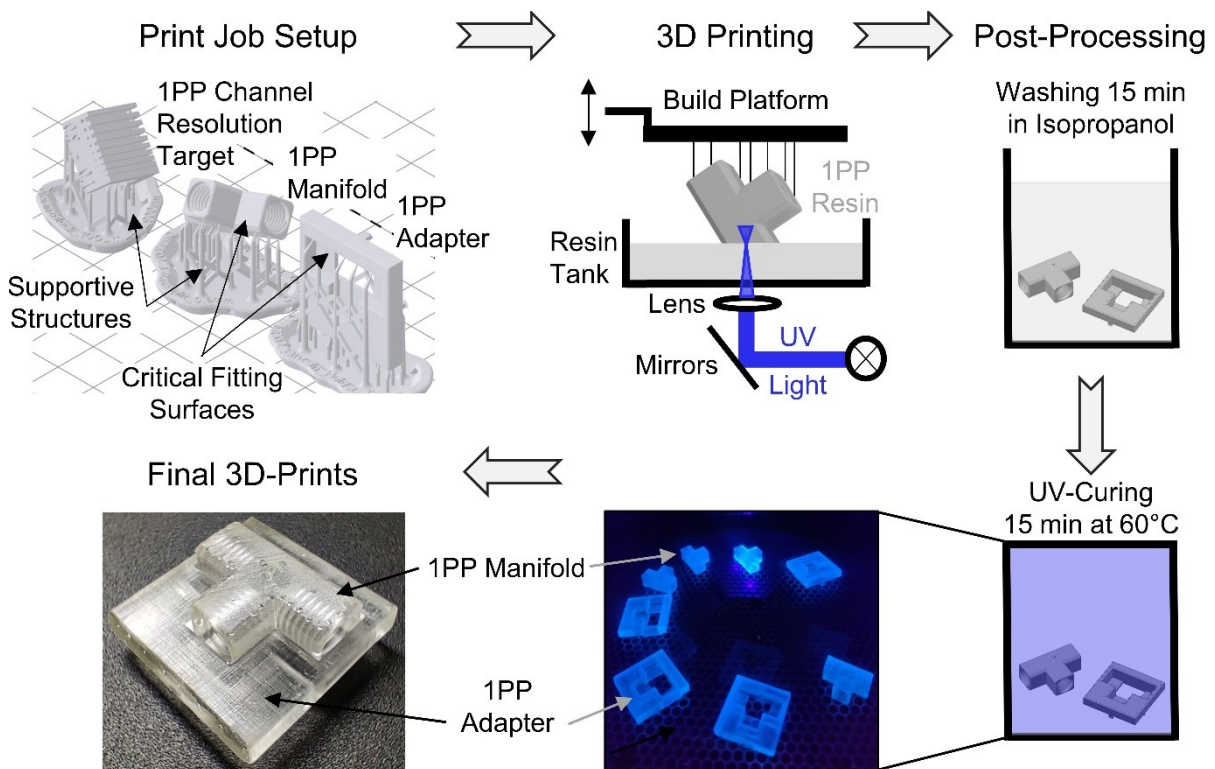


Figure S6: Schematic of the 1PP SLA workflow. After print job configuration, the part was printed. Post-processing includes washing off uncured resin, followed by blow-drying using pressurized air. Once all residual resin was removed, parts were UV-cured for 15 min at 60 °C. Supports were subsequently removed, and the parts can be used without further modification.

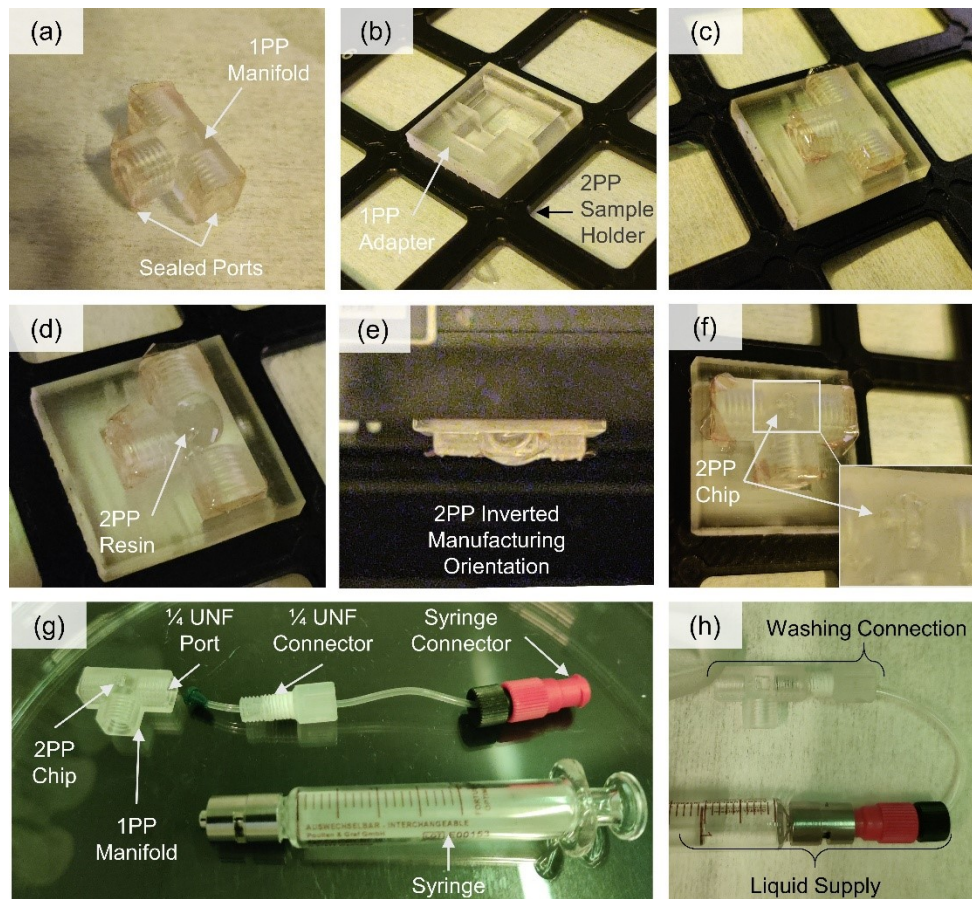


Figure S7: Ex situ 2PP chip fabrication workflow. (a) 1PP manifold ports are sealed with polyimide adhesive tape. (b) The 1PP adapter is clipped into the 2PP sample holder (black). (c) The sealed 1PP manifold is pushed into the 1PP adapter. (d) IP-S is placed atop the 1PP manifold to cover the interfacing microchannels (arrow). (e) The 2PP sample holder is placed upside down in the 2PP-3D printer, and the print job is started. (f) 1PP manifold with 2PP chip fabricated on top (arrow). (g-h) Microfluidic channels are washed by connecting a syringe to the 1PP manifold and gently flushing with PGMEA, isopropanol, and air.

S4 Microfluidic Bubble Generation Setup

Reproducible bubble production is shown in **Video S1**, while **Figure S8** illustrates how the microfluidic device is connected to the gas and liquid supply

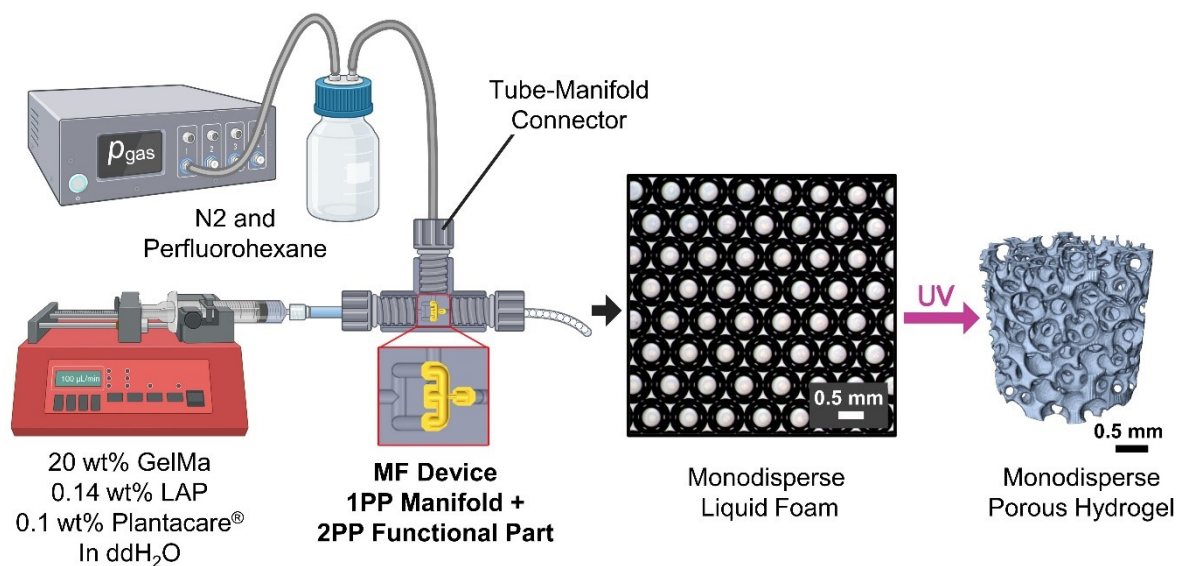


Figure S8: Schematic of the microfluidic bubble generation setup. Tubing connects a syringe pump to the 1PP manifold inlet port to deliver the continuous liquid phase. The dispersed gaseous phase is also connected to the 1PP manifold and is delivered by a pressure controller. Bubble formation proceeds inside the 2PP chip orifice, resulting in a monodisperse foam, which is collected and then crosslinked by UV light to yield a solid porous hydrogel.