

## Electronic Supplementary Information

### **Magneto-responsive deformable coating with lubricant self-replenishment towards on-demand scale repellence**

Danna Liu,<sup>ab†</sup> Jiexin Li,<sup>ab†</sup> Ran Zhao,<sup>ab</sup> Yingbo Li,<sup>ab</sup> Li Dong,<sup>c</sup> Yang Wang,<sup>ab</sup> Weizhe Gao,<sup>ab</sup> Xiaosong Deng,<sup>ab</sup> and Jingxin Meng<sup>\*ab</sup>

<sup>a</sup>Laboratory of Bio-inspired Smart Interface Science, Technical Institute of Physics and Chemistry, Chinese Academy of Sciences, Beijing 100190, P. R. China. Email : mengjx628@mail.ipc.ac.cn

<sup>b</sup>University of Chinese Academy of Sciences, Beijing 100049, P. R. China.

<sup>c</sup>Department of Orthodontics, Peking University School and Hospital of Stomatology, Beijing 100081, P. R. China

\* Corresponding authors

† These authors have contributed equally to this work

## Contents:

<b>1. Supplementary Notes</b> .....	3
<b>1.1 Materials</b> .....	3
<b>1.2 Characterization</b> .....	3
<b>1.3 Theoretical criterion and energy calculation for stable lubricating film formation</b> .....	4
<b>1.4 The calculation of Gibbs energy barrier of scale nucleus</b> .....	5
<b>1.5. The calculation of the interfacial energies</b> .....	7
<b>2. Supplementary Figures</b> .....	8
<b>Fig. S1.</b> Schematic illustration depicting the fabrication process of MRDC. ....	8
<b>Fig. S2.</b> Selection of lubricants.....	9
<b>Fig. S3.</b> Photograph of the experimental set-up for adjusting the magnetic field strength. .	10
<b>Fig. S4.</b> The effect of pore diameters on lubricant spreading area. ....	11
<b>Fig. S5.</b> Schematic illustration of lubricant transport and replenishment processes. ....	12
<b>Fig. S6.</b> Magnetization as a function of magnetic field strength for the MRDC with the mass ratios of PDMS:Co varying from 5:1 to 5:5. ....	13
<b>Fig. S7.</b> Schematic illustrations of stability tests and corresponding WCA of lubricant-free MRDC.....	14
<b>Fig. S8.</b> The corrosion resistance performance of the lubricant-free MRDC. ....	15
<b>Fig. S9.</b> SAs of the MRDC after immersion in acidic (2 M), alkaline (2 M), and saline solution (2 M) for different times. ....	16
<b>3. Supplementary Tables</b> .....	17
<b>Table S1.</b> Comparison of surface energy of different liquid systems .....	17
<b>Table S2.</b> Summary of interfacial energy across different interfaces .....	18
<b>Table S3.</b> Summary of surface energy of materials .....	19
<b>4. References</b> .....	20

## **1. Supplementary Notes**

### **1.1 Materials**

Polydimethylsiloxane (PDMS, Sylgard 184) was purchased from Dow Corning (USA). n-Hexane, Calcium chloride anhydrous (96%), nanometer calcium carbonate (50 nm), sodium sulfate anhydrous (99%), sodium chloride, rhodamine B and paraffin liquid were purchased from Macklin Biochemical Technology Co., Ltd. (China). Co (99.9% metals basis,  $\leq 500$  nm), silicone oil PMX-200 (10 mPa.s, neat) and sodium hydroxide were purchased from Aladdin Chemical (China). Ethylenediamine tetraacetic acid disodium salt (EDTA- $\text{Na}_2$ , AR) was purchased from Sinopharm Chemical Reagent Co., Ltd. (China).  $\text{SiO}_2$  nanoparticles (R972) were purchased from Lijie Chemical Co., Ltd (China). Commercial polyurethane sponge (thickness: 3 mm) was purchased from Yunzongcheng New Materials Manufacturer (China). Krytox 100 was purchased from DuPont (USA). All aqueous solutions were prepared using deionized water (Milli-Q system, 18.2  $\text{M}\Omega\cdot\text{cm}$ , Bedford, MA, USA). All reagents were used directly without further purification.

### **1.2 Characterization**

Surface morphology was observed using an environmental scanning electron microscope (ESEM) (FEI, Quanta FEG 250, USA). Magnetic field strength was measured using a Gauss meter (Tunkia, TD8620, China). Energy dispersive spectrometry (EDS) analysis was conducted to observe the distribution of magnetic particles within the PDMS matrix. Room-temperature hysteresis loops of MRDC samples with varying Co contents were measured using a vibrating sample magnetometer (VSM, Lakeshore 7404, Lake Shore, USA). The replenishing process was recorded using a Sony camera (FDR-AXP55). The surface tension and interfacial tension were measured using the pendant drop method. The deposited scale was quantified using Inductively Coupled Plasma Atomic Emission Spectroscopy (ICP-AES, Varian 710-OES, USA). The contact angle of air and water was measured using an SCA-20 instrument at room temperature (Data-physics, Germany). The adhesion force between the lubricant and surfaces was evaluated using a high-sensitivity microelectromechanical balance system (DCAT 11, Data-physics, Germany). A Laser scanning confocal microscope (OLS-4500, Olympus, Japan) was employed to map the 3D surface topography and determine the average surface roughness ( $R_a$ ) of the samples.

### 1.3 Theoretical criterion and energy calculation for stable lubricating film formation

According to the lubricating film stability conditions, three overall system energies need to be compared:  $E_1$  (lubricant in mineral solution wetting the surface),  $E_2$  (mineral solution in air wetting the surface), and  $E_3$  (lubricant in air wetting the surface). A stable lubricating film can theoretically form if the following conditions are satisfied:  $\Delta E_1 = E_2 - E_1 > 0$  and  $\Delta E_2 = E_2 - E_3 > 0$ .<sup>1</sup>

Here,  $\Delta E_1$  and  $\Delta E_2$  can be expressed as:

$$\Delta E_1 = R (\gamma_{l_2} \cos\theta_{l_2} - \gamma_{l_1} \cos\theta_{l_1}) - \gamma_{l_1 l_2} \quad (S1)$$

$$\Delta E_2 = R (\gamma_{l_2} \cos\theta_{l_2} - \gamma_{l_1} \cos\theta_{l_1}) + \gamma_{l_1} - \gamma_{l_2} \quad (S2)$$

where  $R$  represents the roughness coefficient of the MDL with a rough structure ( $R = 2.02$ ), and the roughness coefficient is the ratio of the actual area to the projected area. The symbols  $\gamma_{l_1}$ ,  $\gamma_{l_2}$  and  $\gamma_{l_1 l_2}$  represent the interfacial energy of the mineral solution in air ( $l_1$ ), the interfacial energy of the lubricant ( $l_2$ ) in air, and the interfacial energy between the mineral solution and the lubricant, respectively. The  $\gamma_{l_1}$  is  $72.4 \text{ mJ/m}^2$  and  $\theta_{l_1}$  is  $142.2^\circ$ . The energy relationships between three common lubricants (*i.e.*, Krytox 100, silicone oil, and liquid paraffin) and saturated  $\text{CaSO}_4$  solution are compared.

By using the hanging drop method and a contact angle meter, various contact angle values and a series of interfacial energy values were obtained. Through these values,  $\Delta E_1$  and  $\Delta E_2$  can be calculated. The relevant values and calculation results are listed in Table S1.

#### 1.4 The calculation of Gibbs energy barrier of scale nucleus

The value of  $\Delta G$  was determined by  $f(m, x)$  is expressed as

$$\Delta G = kf(m, x) = \frac{1}{2} \left\{ 1 + \left( \frac{1 - mx}{g} \right)^3 + x^3 \left[ 2 - 3 \left( \frac{x - m}{g} \right) + \left( \frac{x - m}{g} \right)^3 \right] + 3mx^2 \left( \frac{x - m}{g} - 1 \right) \right\} \quad (S3)$$

where

$$g = (1 + x^2 - 2mx)^{1/2} \quad (S4)$$

And  $k$  is a constant for scale crystal nucleation.  $x = R/r_c$ ,  $R$  represents roughness radius of the surface,  $r_c$  represents the critical nucleus size. We used the approach developed by Ghasemi *et al.* to determine the value of  $m$ .

The first case is MRDC with stable lubricant film. According to Young's equation,  $\theta_1$  can be written as

$$\gamma_{nk} = \gamma_{sk} - \gamma_{ns} \cos \theta_1 \quad (S5)$$

while the  $\theta_2$  can be written as

$$\gamma_{nk} = \gamma_{ns} - \gamma_{sk} \cos \theta_2 \quad (S6)$$

where  $n, s, k$  represents scale nucleus, salt solution and Krytox 100, respectively. By subtraction of these equations,  $m_1$  can be calculated as

$$m_1 = \cos \theta_1 = \frac{\gamma_{sk}}{\gamma_{ns}} (1 + \cos \theta_2) - 1 \quad (S7)$$

In contrast, after depletion of lubricant film, the scale nucleus was directly contact with the rough surface of MRDC. In this case,  $\theta_3$  can be calculated as

$$\gamma_{nm} = \gamma_{sm} - \gamma_{ns} \cos \theta_3 \quad (S8)$$

Where  $m_2$  and  $\theta_3$ . The interfacial tension of MRDC-D-salt solution ( $\gamma_{sm}$ ) can be calculated using Young's equation

$$\gamma_{sm} = \gamma_{ma} - \gamma_{sa} \cos \theta_4 \quad (S9)$$

where  $\gamma_{ma}$  and  $\gamma_{sa}$  represent the interfacial tension of the rough surface of MRDC-D-air and salt solution-air, respectively.  $\theta_4$  is the contact angle of a  $\text{CaSO}_4$  solution droplet on the rough surface

of MRDC-D in air. The interfacial tension of scale nucleus-rough surface of MRDC-D can be calculated as reported<sup>2</sup>

$$\gamma_{nm} = \gamma_n + \gamma_m - 2\sqrt{\gamma_n \gamma_m} \quad (\text{S10})$$

where  $\gamma_n$  and  $\gamma_m$  represent the surface energy of the scale nucleus and the rough surface of MRDC-D, respectively. Therefore,  $m_2$  ( $m_2 = \cos \theta_3$ ) can be calculated by combination of equation (S8), (S9) and (S10).

The PDMS surface were also directly contacted with the scale nucleus. Therefore, the value of  $m_3$  can be calculated the same way as  $m_2$ . The above-mentioned interfacial tension was summarized in Table S2. Having all these parameters, we found that the value of  $m_1$ ,  $m_2$  and  $m_3$  were -0.91, 0.55, 0.36, respectively.

## 1.5. The calculation of the interfacial energies

Both of  $\gamma_{cs}$  and  $\gamma_{sm}$  can be calculated using Young's equation

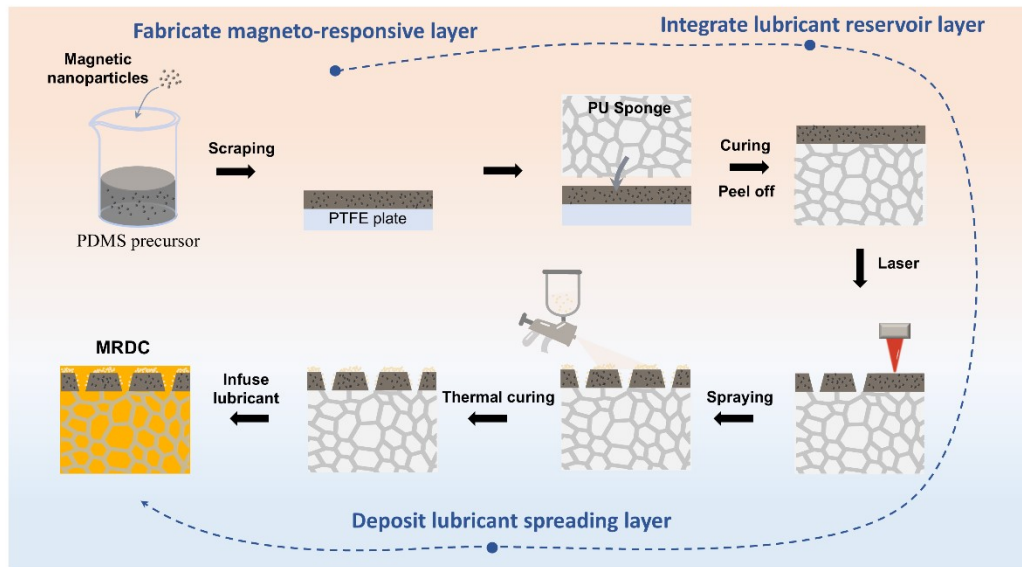
$$\gamma_{cs} = \gamma_{ca} - \gamma_{sa} \cos \theta_5 \quad (S11)$$

According to a previous research, the value of the contact angle of a CaSO<sub>4</sub> solution droplet on the CaSO<sub>4</sub> substrate was 0°. <sup>3</sup> Then the interfacial energy between scale crystal and rough surface of MRDC ( $\gamma_{cm}$ ) can be expressed as<sup>4</sup>

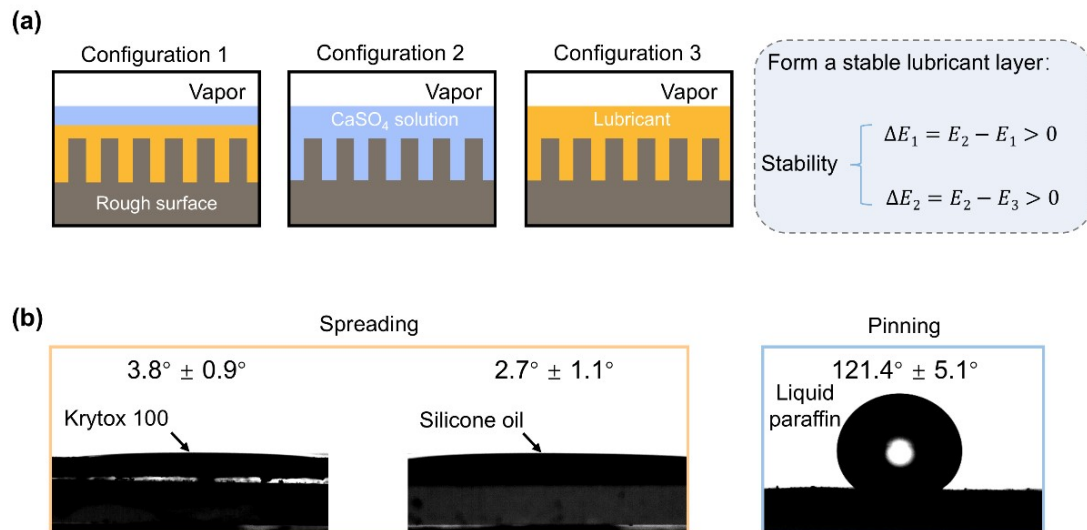
$$\gamma_{cm} = \left( \sqrt{\gamma_c^{LW}} - \sqrt{\gamma_m^{LW}} \right)^2 + 2 \left( \sqrt{\gamma_c^+ \gamma_c^-} + \sqrt{\gamma_m^+ \gamma_m^-} - \sqrt{\gamma_c^+ \gamma_m^-} - \sqrt{\gamma_m^+ \gamma_c^-} \right) \quad (S12)$$

where  $\gamma^+$ ,  $\gamma^-$  and  $\gamma^{LW}$  represent the polar components from the Lewis acid and base sites and the nonpolar component of surface energy, respectively. The contact angles of three standard liquids (water, glycerol and n-hexadecane) are required to calculate  $\gamma_m$ , the related results were also shown in Table S3. Therefore, we can obtain the value of  $\gamma_{cs}$ ,  $\gamma_{sm}$  and  $\gamma_{cm}$  was -12.7 mJ/m<sup>2</sup>, 58.4 and 18.0 mJ/m<sup>2</sup>, respectively. The adhesion work between PDMS surface and scale crystal ( $W_{cp}^a$ ) can also be calculated the same way as above and the value of  $\gamma_{sp}$  and  $\gamma_{cp}$  was 44.3 mJ/m<sup>2</sup> and 3.46 mJ/m<sup>2</sup>, respectively.

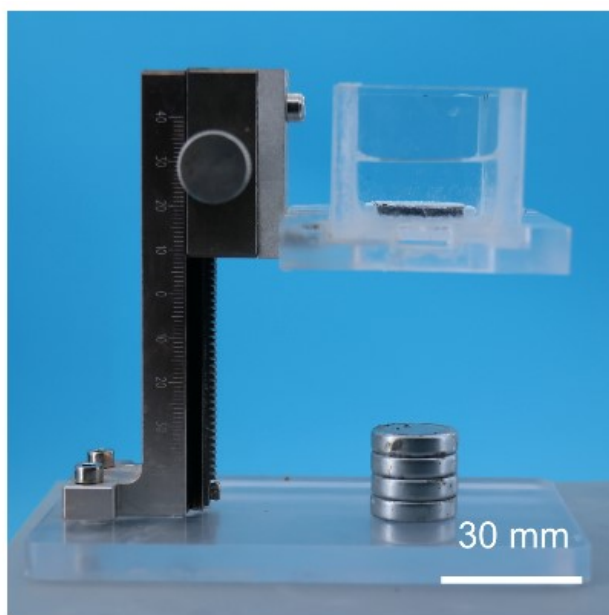
## 2. Supplementary Figures



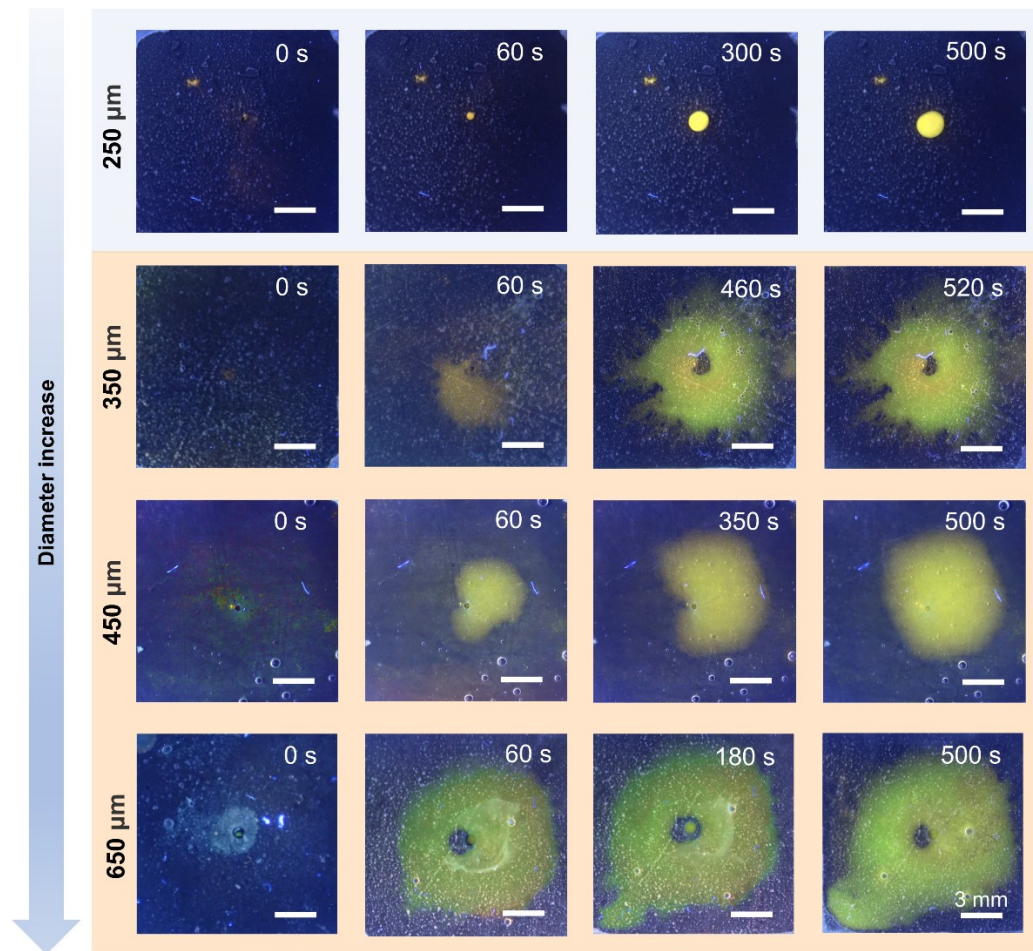
**Fig. S1.** Schematic illustration depicting the fabrication process of MRDC.



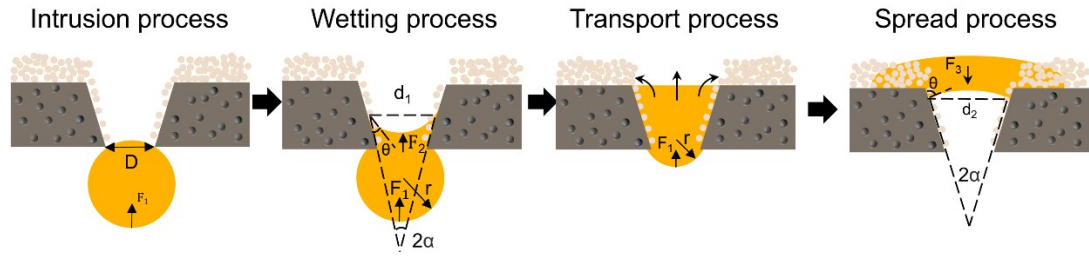
**Fig. S2.** Selection of lubricants. (a) Schematic diagrams of the working conditions required to maintain a stable lubricating film. (b) Contact angles of Krytox 100, silicone oil, and liquid paraffin measured on the MRDC surface.



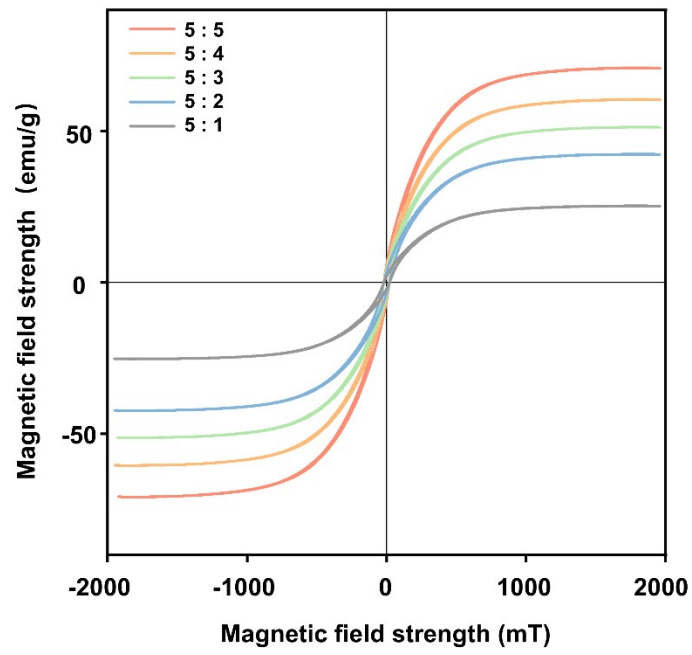
**Fig. S3.** Photograph of the experimental set-up for adjusting the magnetic field strength.



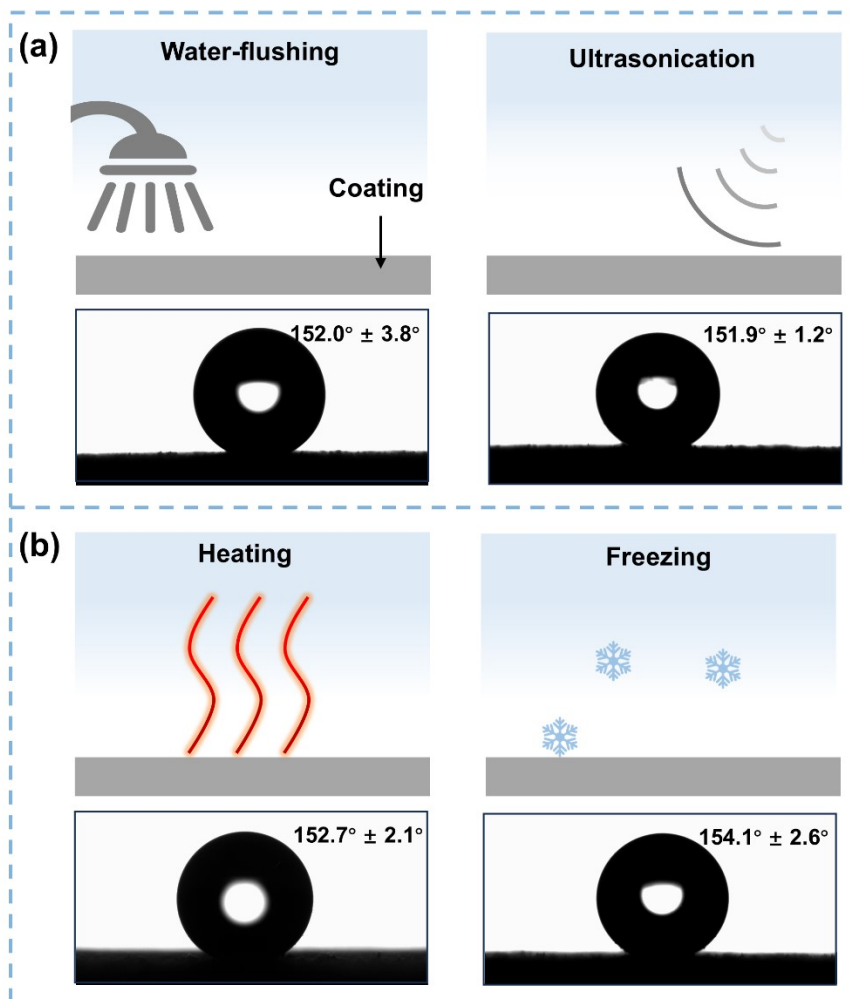
**Fig. S4.** The effect of pore diameters on lubricant spreading area.



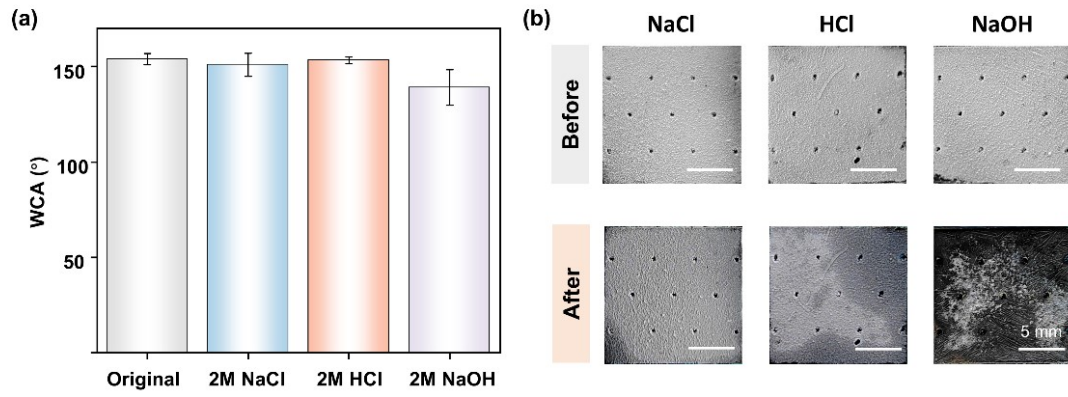
**Fig. S5.** Schematic illustration of lubricant transport and replenishment processes. Lubricant replenishment from the LRL to the upper LSL involves intrusion, wetting, transport, and spreading processes.  $F_1$ ,  $F_2$ , and  $F_3$  denote the surface tension, capillary force, and drag force, respectively.



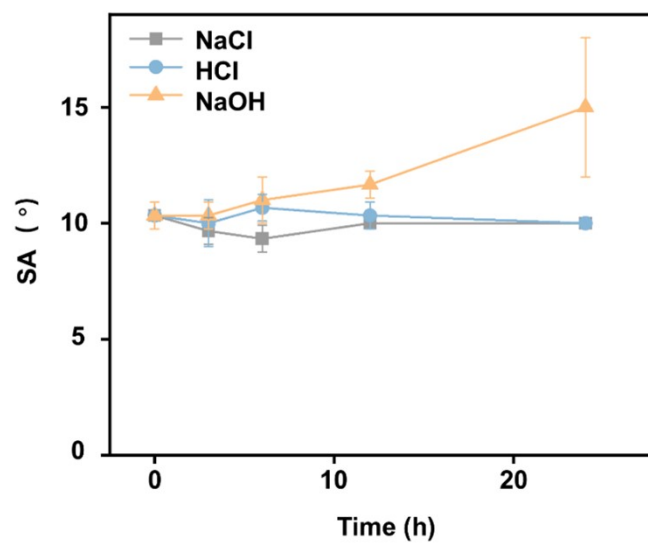
**Fig. S6.** Magnetization as a function of magnetic field strength for the MRDC with the mass ratios of PDMS:Co varying from 5:1 to 5:5.



**Fig. S7.** Schematic illustrations of stability tests and corresponding WCA of lubricant-free MRDC. (a) Mechanical stability evaluation *via* water flushing and underwater ultrasonication. (b) Thermal stability evaluation *via* hot water immersion and freezing.



**Fig. S8.** The corrosion resistance performance of the lubricant-free MRDC. (a) The WCA of lubricant-free MRDC original and after immersion in acidic, alkaline, and saline solution for 12h. (b) Optical image before and after immersion in acidic, alkaline, and saline solution.



**Fig. S9.** SAs of the MRDC after immersion in acidic (2 M), alkaline (2 M), and saline solution (2 M) for different times.

### 3. Supplementary Tables

**Table S1.** Comparison of surface energy of different liquid systems

Lubricant	$\gamma_{l_2}$ (mJ/m <sup>2</sup> )	$\gamma_{l_1l_2}$ (mJ/m <sup>2</sup> )	$\theta_{l_1}$ (°)	$\theta_{l_2}$ (°)	$\Delta E_1$ (mJ/m <sup>2</sup> )	$\Delta E_2$ (mJ/m <sup>2</sup> )
Krytox 100	16.3	53.0	142.2	3.8	95.4	92.4
Silicone oil	17.8	34.1	142.2	2.2	117.4	96.9
Paraffin liquid	28.5	42.2	142.2	121.4	43.3	41.7

**Table S2.** Summary of interfacial energy across different interfaces

Interface	Interfacial energy	Value (mJ/m <sup>2</sup> )	Data source
CaSO <sub>4</sub> solution-Krytox 100	$\gamma_{sk}$	53	Experiment
CaSO <sub>4</sub> solution-MRDC	$\gamma_{sm}$	58.4	Equation (S9)
Scale nucleus-CaSO <sub>4</sub> solution	$\gamma_{ns}$	95	Reference <sup>5</sup>
Scale nucleus-MRDC	$\gamma_{nm}$	6.36	Equation (S10)
MRDC-air	$\gamma_{ma}$	27.3	Experiment
Scale nucleus-PDMS	$\gamma_{np}$	10.1	Equation (S10)
CaSO <sub>4</sub> solution-PDMS	$\gamma_{sp}$	44.3	Equation (S9)
Scale crystal-CaSO <sub>4</sub> solution	$\gamma_{cs}$	-12.7	Equation (S11)
Scale crystal-MRDC	$\gamma_{cm}$	18.0	Equation (S12)
Scale crystal-PDMS	$\gamma_{cp}$	3.46	Equation (S12)

**Table S3.** Summary of surface energy of materials

Material	$\gamma$ (mJ/m <sup>2</sup> )	$\gamma^{\text{LW}}$ (mJ/m <sup>2</sup> )	$\gamma^+$ (mJ/m <sup>2</sup> )	$\gamma^-$ (mJ/m <sup>2</sup> )
CaSO <sub>4</sub>	59.7	41.1	1.3	65.5
MRDC-D	27.7	27.7	0	0.61
PDMS	20.7	20.7	0	0

**Note:**  $\gamma$  denotes surface tension.  $\gamma^{\text{LW}}$  is the Lifshitz-van der Waals component of surface energy.  $\gamma^+$  and  $\gamma^-$  are the polar components from the Lewis acid and Lewis base sites, respectively.

## 4. References

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