

Supplementary Information

Abbreviations

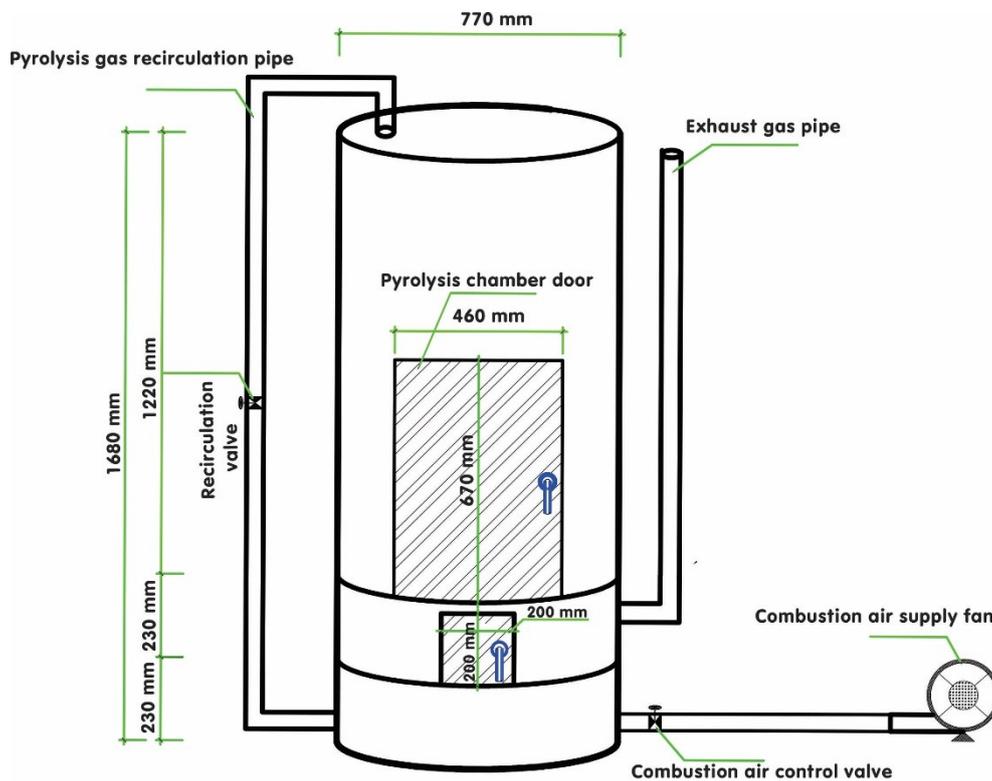
Ads_dos:	Adsorbent dosage
ANN:	artificial neural networks
BET:	Brunauer–Emmett–Teller
CGW:	Carbonized garment waste biochars
CGW400:	CGW was carbonized at temperatures of 400 °C
CGW600:	CGW was carbonized at temperatures of 600 °C
CGW800:	CGW was carbonized at temperatures of 800 °C
CGW900:	CGW was carbonized at temperatures of 900 °C
Cr:	Chromium
Cr_con:	Cr ion concentration
EDX:	Energy-Dispersive X-ray Spectroscopy
FTIR:	Fourier Transform Infrared Spectroscopy
LR:	Linear Regression
MAE:	Mean Absolute Error
ML:	Machine learning
RF:	Random forests
RMSE:	Root Mean Square Error
R ² :	Coefficient of determination
SEM:	Scanning Electron Microscopy
SVM:	Support vector machines
Pb:	Lead
Pb_con:	Pb ion concentration
PFO:	Pseudo-first-order
PSO:	Pseudo-second-order
q _e :	Adsorption capacity
q _{m,cal} :	Calculated adsorption capacity
q _{e,exp} :	Experimental adsorption capacity
XRD:	X-ray Diffraction
Time:	Contact time

SI-1: Pyrolysis reactor description

The reactor consists of a cylindrical stainless-steel chamber (Inox 304) with a total height of 1.68 m and an internal diameter of 0.77 m, providing a total working capacity of 12 kg of

garment waste per batch. The inner wall is insulated with a 10–15 cm refractory ceramic layer to minimize heat loss and maintain stable thermal conditions during operation. The lower section of the reactor houses the primary combustion chamber, which is fueled by liquefied petroleum gas and is connected to an adjustable air supply valve that precisely regulates combustion intensity and airflow.

A distinctive feature of this design is the incorporation of an organic vapor recirculation loop that continuously redirects volatile gases and organic vapors generated during pyrolysis back into the combustion zone. This feedback mechanism provides 30–50% of the total heating energy, thereby reducing external fuel consumption and improving overall energy efficiency. An exhaust gas outlet is installed to safely discharge non-condensable gases. At the same time, thermocouples (type K, ± 1 °C accuracy) are embedded at multiple points within the chamber to monitor and control temperature profiles in real time.



NOTES:

- Lower Door: 200 × 200 (mm)
- Upper Door: 670 × 460 (mm)
- Inner Layer: Stainless Steel 201, thick: 2 mm
- Outer Layer: Mild Steel, 3 mm thick
- Air Supply Pipe: Galvanized Steel, thick: 2 mm
- Air Supply Pipe Diameter: Ø48 mm
- Exhaust gas outlet pipe diameter: Ø72 mm
- Pyrolysis recirculation pipe diameter: Ø48 mm

Fig. S1. Schematic design of the vertical anaerobic pyrolysis reactor for converting garment waste into multifunctional materials

SI-2: Adsorption equations

The adsorption capacity of CGW at a specific contact time (q_t , mg/g) and at equilibrium (q_e , mg/g) was determined using equations (1) and (2):

$$q_e = \frac{(C_o - C_e)V}{W} \quad (1)$$

$$q_t = \frac{(C_o - C_t)V}{W} \quad (2)$$

where C_o , C_t , and C_e (mg/L) denote the initial, time-dependent and equilibrium concentrations of Pb(II) or Cr(VI) in solution, respectively; V (L) is the volume of the metal solution, and W (g) is the dry weight of the biochar adsorbent.

To investigate the adsorption rate and mechanism, the kinetic data were fitted using three established models: the pseudo-first-order, pseudo-second-order and Elovich models. Their respective linearized equations are expressed using equations (3), (4) and (5):

Pseudo - first - order model: $\ln(q_e - q_t) = \ln q_e - k_1 t$ (3)

Pseudo - second - order model: $\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} t$ (4)

Elovich model: $\frac{t}{q_t} = \frac{1}{\beta} \ln \left(\frac{\alpha \beta}{\beta} \right) + \frac{1}{\beta} \ln t$ (5)

In these equations, q_e and q_t (mg/g) represent the adsorption capacities at equilibrium and at time t (min), respectively. k_1 (min^{-1}) and k_2 ($\text{g} \cdot \text{mg}^{-1} \cdot \text{min}^{-1}$) are the rate constants for the pseudo-first-order and pseudo-second-order models. In the Elovich equation, α ($\text{mg} \cdot \text{g}^{-1} \cdot \text{min}^{-1}$) corresponds to the initial adsorption rate, while β ($\text{g} \cdot \text{mg}^{-1}$) reflects the degree of surface coverage and activation energy associated with chemisorption.

By comparing the regression coefficients (R^2) and the agreement between experimental and theoretical q_e values, the dominant adsorption mechanism - whether physisorption or chemisorption - was determined.

Equilibrium adsorption data for Pb(II) and Cr(VI) were further analyzed using three classical isotherm models - Langmuir, Freundlich, and Sips - to describe the interactions between the metal ions and the heterogeneous surface of CGW. The corresponding model equations are given as equations (6), (7), and (8):

Langmuir model: $q_e = \frac{q_m K_L C_e}{1 + K_L C_e}$ (6)

Freundlich model: $q_e = K_F C_e^{\frac{1}{n}}$ (7)

$$\text{Sips model: } q_e = \frac{q_m (bC_e)^{\frac{1}{n}}}{1 + (bC_e)^{\frac{1}{n}}} \quad (8)$$

Where, q_e (mg/g) and q_m (mg/g) are the equilibrium and maximum adsorption capacity of the adsorbents, respectively; b is the Langmuir constant related to the free adsorption energy (L/mg); C_e is the equilibrium concentration of Pb(II) or Cr(VI) (mg/L); K_L (L/mg) is the Langmuir constant; K_F (mg/g) is the Freundlich constant; n is the adsorption intensity.

Here, q_e (mg/g) and q_m (mg/g) represent the equilibrium and maximum adsorption capacities, respectively. C_e (mg/L) denotes the equilibrium concentration of Pb(II) or Cr(VI). K_L (L/mg) is the Langmuir affinity constant related to the free energy of adsorption, K_F ((mg·g⁻¹)(L·mg⁻¹)^{1/n}). n are the Freundlich constants associated with adsorption capacity and intensity. In contrast, b and n in the Sips model correspond to the heterogeneity and energy distribution of the surface binding sites.

SI-3: Machine learning

The dataset was partitioned into training (80%) and testing (20%) subsets using stratified random sampling via the `caret::createDataPartition()` function (`seed = 42`)¹ to ensure proportional representation of adsorption capacity values. Data preprocessing included centering and scaling for Linear Regression (LR) and Random Forest (RF) models, and min–max normalization to [0,1] for Support Vector Machine (SVM) models using `caret::preprocess()`. This structured preprocessing ensured numerical stability, improved model convergence and enhanced comparability across algorithms.

Four supervised learning algorithms were applied to predict the adsorption capacity of Pb(II) and Cr(VI): ANN, LR, RF and SVM. Each model was trained, tuned and validated using 10-fold cross-validation to prevent overfitting.

Artificial Neural Network (ANN): A single-hidden-layer neural network was trained using the `caret::nnet` package. Grid search optimization was performed over hidden layer sizes (2–20 nodes), with a fixed `decay = 0.01` and `maxit = 50,000` iterations. The optimal model consisted of four hidden neurons, achieving high convergence stability and predictive accuracy. **Linear Regression (LR):** Implemented via ordinary least squares, the LR model served as a baseline due to its interpretability and minimal computational cost. No hyperparameter tuning was required. **Random Forest (RF):** The RF model was constructed using the `caret::rf` package, with a 10-fold cross-validation grid search over `mtry` (1–4) and `min.node.size` (1, 2, 4), `maxdepth` (10, 20, 30, unlimited), and `ntree` (100, 500, 1000). The optimal configuration was `mtry = 2`, `ntree = 500`, `nodesize = 5`, and `maxnodes = NULL`,

providing a strong balance between bias and variance. Support Vector Machine (SVM): The SVM model, implemented via the e1071 package, underwent random search optimization across kernel types (linear, polynomial, radial), cost parameter C (0.01–10), gamma (0.001–0.1), and polynomial degree (1–3). The best performance was achieved with a polynomial kernel, C = 10, degree = 3, gamma = 0.1, and epsilon = 0.1. Each model was evaluated with a fixed random seed (42) to ensure reproducibility. The final trained models were benchmarked against each other based on their predictive performance metrics.

The performance of all models was quantitatively assessed using three standard statistical metrics: Coefficient of determination (R^2), Root Mean Square Error (RMSE), and Mean Absolute Error (MAE). These were computed according to Equations (9)–(11):

$$R^2 = 1 - \frac{\sum_{i=1}^n (y_i - \hat{y}_i)^2}{\sum_{i=1}^n (y_i - \bar{y})^2} \quad (9)$$

$$RMSE = \sqrt{\frac{1}{n} \sum_{i=1}^n (y_i - \hat{y}_i)^2} \quad (10)$$

$$MAE = \frac{1}{n} \sum_{i=1}^n |y_i - \hat{y}_i| \quad (11)$$

where y_i denotes the experimentally measured adsorption capacity, \hat{y}_i is the predicted value, \bar{y} represents the mean of observed values, and n is the total number of samples.

The R^2 value indicates the proportion of variance in the experimental data explained by the model; values approaching 1.0 indicate a superior model fit. The RMSE provides a quadratic measure of prediction deviation, emphasizing larger errors, while the MAE quantifies the mean absolute deviation, offering a linear measure of overall prediction accuracy². By integrating these complementary metrics, a comprehensive evaluation of each model's robustness, generalization, and predictive precision was achieved.

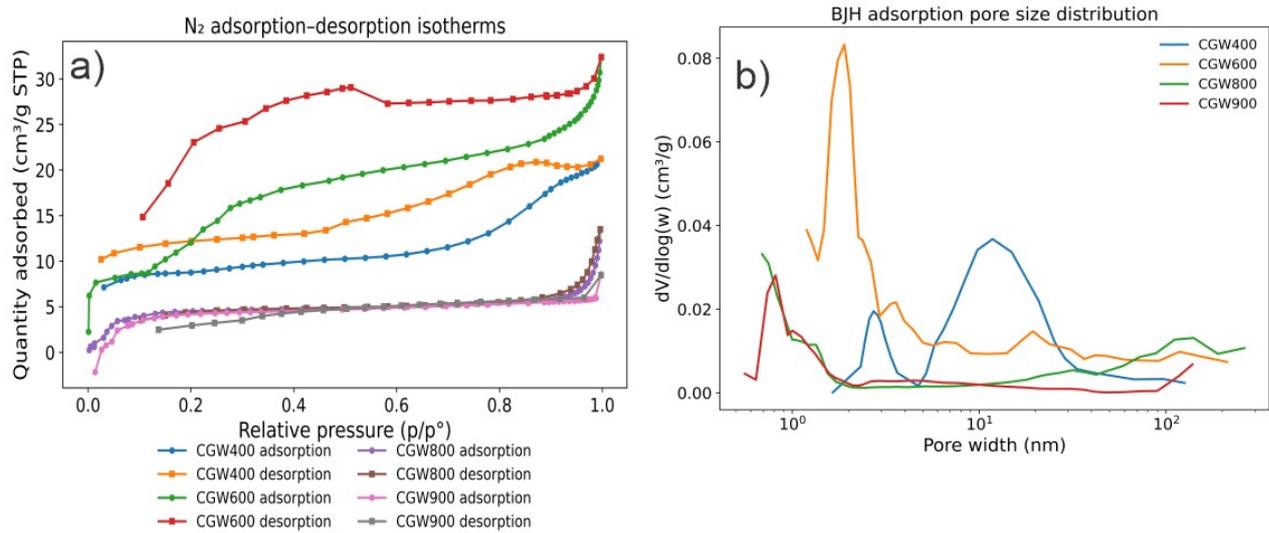


Fig. S2. (a) Nitrogen adsorption–desorption isotherms and (b) pore size distribution curves of CGW400, CGW600, CGW800 and CGW900

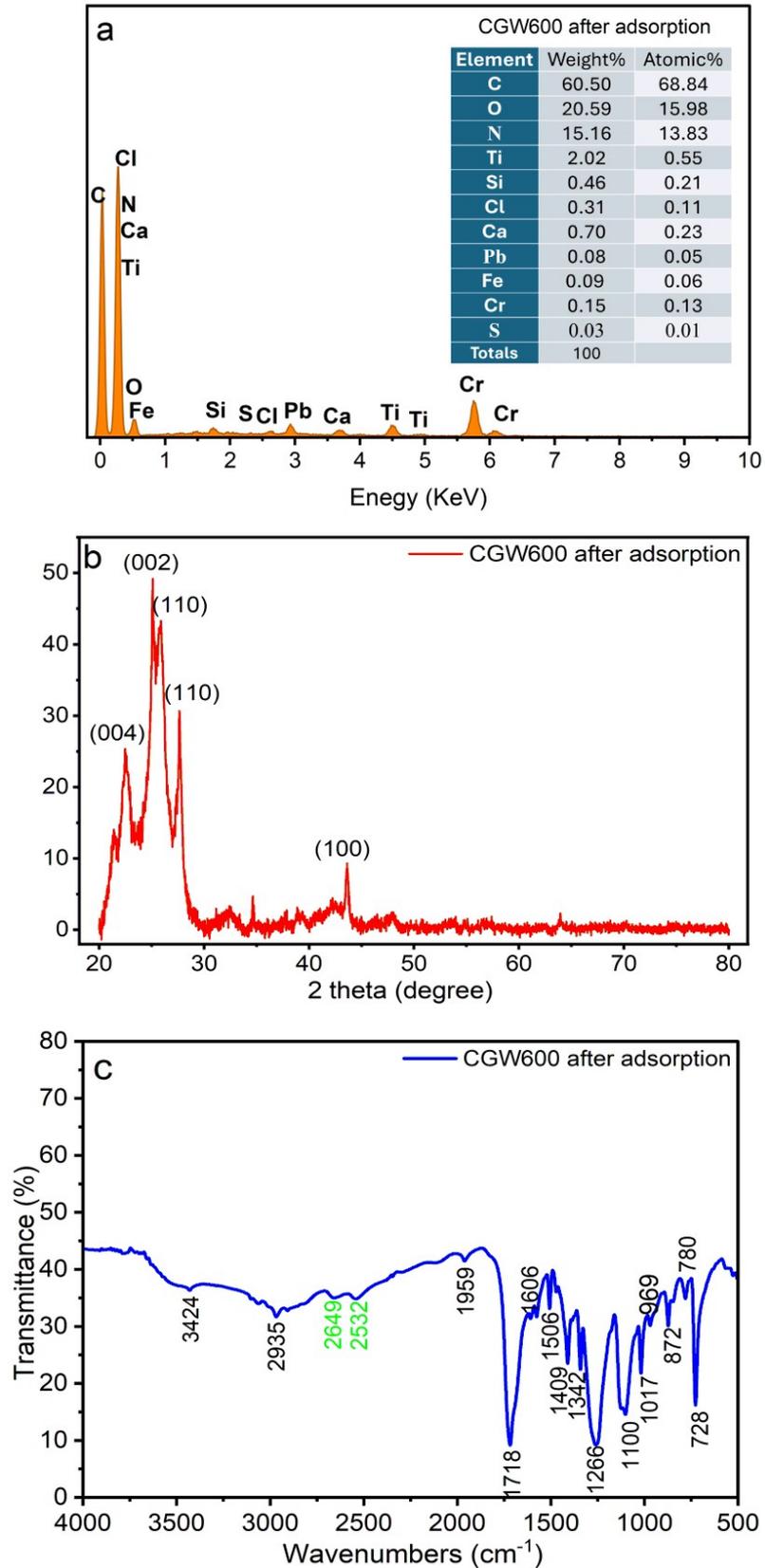


Fig. S3. EDX spectra (a), XRD (b) and FTIR (c) of CWG600 after Pb and Cr adsorption

References

- 1 R. T. Schossler, S. Ojo, Z. Jiang, J. Hu and X. Yu, *Sci. Rep.*, 2024, **14**, 1–15.

- 2 E. Vakarelska, M. Nedyalkova, M. Vasighi and V. Simeonov, *Chemosphere*, 2022, **287**, 132189.