

## 1 Appendix

2 This Appendix presents tables containing both raw and calculated data corresponding to the figures  
3 included in the main manuscript. The supporting tables provide data for calibration samples and  
4 for known and unknown emulsion samples. Additional details about the prepared emulsions are  
5 provided beneath each corresponding table.

### 6 7 Accuracy of Boyle's law for liquid volume measurements

8  
9 The accuracies of Boyle's law, the volumetric method, and the fill-to-full method were evaluated  
10 using three different bottle sizes, as shown in **Table A-1**. This table presents the AARD%  
11 compared to the actual water volumes.

12 **Table A-1**-Volumes of water measured using three methods and the AARD% relative to the actual  
13 volume of water.

| Bottle size  | $V_{water}$ measured by |                   |                     | Actual $V_{water}$ | AARD relative to actual volumes |                   |                     |
|--------------|-------------------------|-------------------|---------------------|--------------------|---------------------------------|-------------------|---------------------|
|              | Boyle's law             | Volumetric method | Fill to full method |                    | Boyle's law                     | Volumetric method | Fill to full method |
|              | mL                      |                   |                     |                    | mL                              | %                 |                     |
| 100 mL       | 80.275                  | 81.0              | 80.022              | 80.232             | 0.018                           | 0.319             | 0.087               |
| 500 mL       | 400.862                 | 404.1             | 399.783             | 400.862            | 0.000                           | 0.269             | 0.090               |
| 1000 mL      | 801.199                 | 807.5             | 799.444             | 801.443            | 0.010                           | 0.252             | 0.083               |
| $\sum$ AARD% |                         |                   |                     |                    | <b>0.028</b>                    | <b>0.840</b>      | <b>0.260</b>        |

### 14 Volume measurement for known emulsion samples

15 Boyle's law parameters obtained during the total volume measurements of emulsion samples were  
16 reported in **Table A-2** for known emulsion samples. The experimentally measured emulsion  
17 volumes were compared with the corresponding ideal volumes, and the deviations were expressed  
18 as the AARD%.

19 **Table A-2**-Arithmetic average of volumes measured using Boyle’s law method and ideal volumes  
 20 of known emulsion samples, along with the AARD%.

| Sample name | S# | Emulsion               | WC           | $P_{charging}$ | $P_{equilibrium}$ | Measured $V_{emulsion}$ | Avg. $V_{emulsion}$ | Ideal $V_{emulsion}$ | AARD   |
|-------------|----|------------------------|--------------|----------------|-------------------|-------------------------|---------------------|----------------------|--------|
|             |    |                        | w/w          | psia           |                   | mL                      |                     | %                    |        |
| WCS         | 1  | RO- 40/60 <sup>1</sup> | 0.99         | 18.133         | 15.048            | 401.80                  | 401.34              | 400.92               | 0.0071 |
|             |    |                        |              | 18.130         | 15.044            | 401.33                  |                     |                      |        |
|             |    |                        |              | 18.080         | 15.021            | 400.91                  |                     |                      |        |
|             | 2  |                        | 0.95         | 18.100         | 15.030            | 401.04                  | 401.90              | 401.80               | 0.0016 |
|             |    |                        |              | 18.104         | 15.038            | 402.12                  |                     |                      |        |
|             |    |                        |              | 17.991         | 14.994            | 402.53                  |                     |                      |        |
|             | 3  |                        | 0.75         | 18.139         | 15.082            | 406.99                  | 407.20              | 405.87               | 0.0218 |
|             |    |                        |              | 18.097         | 15.066            | 407.23                  |                     |                      |        |
|             |    |                        |              | 18.167         | 15.096            | 407.37                  |                     |                      |        |
|             | 4  | 0.50                   | 18.105       | 15.091         | 410.73            | 411.51                  | 410.90              | 0.0099               |        |
|             |    |                        | 18.102       | 15.098         | 412.05            |                         |                     |                      |        |
|             |    |                        | 18.019       | 15.061         | 411.74            |                         |                     |                      |        |
|             | 5  | 0.25                   | 18.032       | 15.101         | 417.22            | 416.81                  | 416.02              | 0.0127               |        |
|             |    |                        | 17.946       | 15.064         | 417.20            |                         |                     |                      |        |
|             |    |                        | 17.954       | 15.060         | 416.02            |                         |                     |                      |        |
|             | 6  | 0.05                   | 23.289       | 17.406         | 421.06            | 421.78                  | 420.12              | 0.0263               |        |
|             |    |                        | 23.235       | 17.391         | 421.70            |                         |                     |                      |        |
|             |    |                        | 22.993       | 17.297         | 422.56            |                         |                     |                      |        |
|             | 7  | 0.01                   | 17.986       | 15.114         | 422.30            | 421.97                  | 421.01              | 0.0153               |        |
|             |    |                        | 18.059       | 15.135         | 420.67            |                         |                     |                      |        |
|             |    |                        | 17.990       | 15.120         | 422.95            |                         |                     |                      |        |
|             | 8  | RO-100 <sup>2</sup>    | 0.75         | 24.506         | 17.649            | 400.66                  | 400.50              | 398.73               | 0.0297 |
|             |    |                        |              | 23.961         | 17.424            | 400.51                  |                     |                      |        |
|             |    |                        |              | 23.697         | 17.314            | 400.34                  |                     |                      |        |
|             | 9  | RO-10/90 <sup>3</sup>  | 0.75         | 23.779         | 17.370            | 402.15                  | 402.34              | 401.57               | 0.0127 |
|             |    |                        |              | 23.894         | 17.417            | 402.13                  |                     |                      |        |
|             |    |                        |              | 23.684         | 17.338            | 402.72                  |                     |                      |        |
| 23.858      |    |                        |              | 18.141         | 452.74            |                         |                     |                      |        |
| 23.004      |    |                        |              | 17.695         | 450.33            |                         |                     |                      |        |
| 23.894      |    |                        |              | 17.417         | 402.13            |                         |                     |                      |        |
|             |    |                        | 23.684       | 17.338         | 402.72            |                         |                     |                      |        |
|             |    |                        | $\sum$ AARD% |                |                   |                         |                     | <b>0.1371</b>        |        |

21 **Notes:**

- 22 • <sup>1</sup> oleic phase is 40/60 wt% toluene/bitumen.
- 23 • <sup>2</sup> oleic phase is 100 wt% bitumen.
- 24 • <sup>3</sup> oleic phase is 90/10 wt% toluene/bitumen.
- 25 • For samples WCS#6 and WCS#7, 100 g of RO water was added to the emulsion sample after measuring its volume to facilitate representative aqueous sampling.
- 26 • For samples WCS#8 and WCS#9, 100 g of toluene was added to the emulsion sample after measuring its volume to reduce the viscosity of the oleic phase and enable salt to reach all water droplets in the water-in-oil emulsion.

34 **Brine salinity measurement for known emulsion samples**

35 Brine salinities for known emulsion samples were determined using three analytical techniques:

36 RI, EC, and gravimetry. The volume of water corresponding to these salinity values was calculated

37 and reported in **Table A-3**. The accuracy of the measured water volumes was evaluated by  
 38 comparing them with the actual water volumes in the known emulsion samples, with deviations  
 39 expressed as the AARD%.

40 **Table A-3**-The volume of water obtained using the RI, EC, and gravimetry methods, along with  
 41 their corresponding AARD% for known emulsion samples prepared for water cut measurements.

| Sample name  | S# | Emulsion               | WC   | $V_{water}$ (mL) |        |        |            | AARD (%)     |              |              |
|--------------|----|------------------------|------|------------------|--------|--------|------------|--------------|--------------|--------------|
|              |    |                        | w/w  | Actual           | RI     | EC     | Gravimetry | RI           | EC           | Gravimetry   |
| WCS          | 1  | RO- 40/60 <sup>1</sup> | 0.99 | 396.78           | 399.33 | 393.47 | 406.08     | 0.043        | 0.056        | 0.156        |
|              | 2  |                        | 0.95 | 380.7            | 381.20 | 376.55 | 384.83     | 0.009        | 0.073        | 0.072        |
|              | 3  |                        | 0.75 | 300.55           | 300.88 | 294.28 | 302.26     | 0.007        | 0.139        | 0.038        |
|              | 4  |                        | 0.50 | 200.36           | 197.42 | 195.12 | 201.72     | 0.098        | 0.174        | 0.045        |
|              | 5  |                        | 0.25 | 100.18           | 100.66 | 97.97  | 101.59     | 0.032        | 0.147        | 0.094        |
|              | 6  |                        | 0.05 | 20.05            | 21.14  | 19.18  | 21.33      | 0.362        | 0.289        | 0.426        |
|              | 7  |                        | 0.01 | 4.03             | 4.72   | 3.01   | 5.21       | 1.141        | 1.687        | 1.952        |
|              | 8  | RO-100 <sup>2</sup>    | 0.75 | 300.57           | 300.31 | 294.45 | 303.29     | 0.006        | 0.136        | 0.060        |
|              | 9  | RO-10/90 <sup>3</sup>  | 0.75 | 300.52           | 300.35 | 295.19 | 299.28     | 0.004        | 0.118        | 0.028        |
| $\sum$ AARD% |    |                        |      |                  |        |        |            | <b>1.702</b> | <b>2.819</b> | <b>2.871</b> |

42 **Notes:**

- 43 • <sup>1</sup> oleic phase is 40/60 wt% toluene/bitumen.
- 44 • <sup>2</sup> oleic phase is 100 wt% bitumen.
- 45 • <sup>3</sup> oleic phase is 90/10 wt% toluene/bitumen.
- 46 • For samples WCS#6 and WCS#7, 100 g of RO water was added to the emulsion sample after measuring its volume to facilitate representative aqueous sampling.
- 47 • For samples WCS#8 and WCS#9, 100 g of toluene was added to the emulsion sample after measuring its volume to reduce the viscosity of the oleic phase and enable the salt to reach all water droplets in the water-in-oil emulsion.

49  
50

### 51 **Water cuts measurement for known emulsion samples**

52 Following the determination of the total emulsion volume and the quantification of the aqueous  
 53 phase, both volumetric (v/v) and mass-based (w/w) water cuts were calculated for the known  
 54 emulsion samples. The measured volumetric water cuts (v/v) and mass water cuts (w/w) were then  
 55 compared with the actual (reference) water cut values. The results, including the deviations from  
 56 the true values, are presented in **Tables A-4** and **A-5**, respectively. The accuracy of the

57 measurements was assessed by calculating the AARD% to evaluate the performance of the  
 58 methods used in predicting water cut under the tested conditions.

59 **Table A-4-Volumetric water cuts (v/v) and corresponding AARD% for known emulsion samples**  
 60 measured using RI, EC, and gravimetry techniques compared to actual volumetric water cuts (v/v).

| Sample name  | S# | Emulsion               | WC   | WC (v/v) |       |       |            | AARD% relative to actual WC |              |              |
|--------------|----|------------------------|------|----------|-------|-------|------------|-----------------------------|--------------|--------------|
|              |    |                        | w/w  | Actual   | RI    | EC    | Gravimetry | RI                          | EC           | Gravimetry   |
| WCS          | 1  | RO- 40/60 <sup>1</sup> | 0.99 | 0.990    | 0.995 | 0.980 | 1.012      | 0.036                       | 0.063        | 0.149        |
|              | 2  |                        | 0.95 | 0.947    | 0.949 | 0.937 | 0.958      | 0.007                       | 0.074        | 0.071        |
|              | 3  |                        | 0.75 | 0.741    | 0.739 | 0.723 | 0.742      | 0.014                       | 0.160        | 0.016        |
|              | 4  |                        | 0.50 | 0.488    | 0.480 | 0.474 | 0.490      | 0.107                       | 0.184        | 0.035        |
|              | 5  |                        | 0.25 | 0.241    | 0.242 | 0.235 | 0.244      | 0.020                       | 0.160        | 0.081        |
|              | 6  |                        | 0.05 | 0.048    | 0.050 | 0.045 | 0.051      | 0.333                       | 0.314        | 0.398        |
|              | 7  |                        | 0.01 | 0.010    | 0.011 | 0.007 | 0.012      | 1.126                       | 1.694        | 1.927        |
|              | 8  | RO-100 <sup>2</sup>    | 0.75 | 0.754    | 0.750 | 0.735 | 0.757      | 0.035                       | 0.165        | 0.030        |
|              | 9  | RO-10/90 <sup>3</sup>  | 0.75 | 0.748    | 0.747 | 0.734 | 0.744      | 0.017                       | 0.131        | 0.040        |
| $\sum$ AARD% |    |                        |      |          |       |       |            | <b>1.695</b>                | <b>2.945</b> | <b>2.747</b> |

61 Notes:

- 62 • <sup>1</sup> oleic phase is 40/60 wt% toluene/bitumen.
- 63 • <sup>2</sup> oleic phase is 100 wt% bitumen.
- 64 • <sup>3</sup> oleic phase is 90/10 wt% toluene/bitumen.
- 65 • For samples WCS#6 and WCS#7, 100 g of RO water was added to the emulsion sample after measuring its volume to facilitate representative aqueous sampling.
- 66 • For samples WCS#8 and WCS#9, 100 g of toluene was added to the emulsion sample after measuring its volume to reduce the viscosity of the oleic phase and enable the salt to reach all water droplets in the water-in-oil emulsion.

70 **Table A-5-Mass water cuts (w/w) and corresponding AARD% for known emulsion samples**  
 71 measured using RI, EC, and gravimetry techniques compared to actual mass water cuts (w/w).

| Sample name | S# | Emulsion               | WC   | WC (w/w) obtained from |       |       |            | AARD% relative to actual WC |       |            |
|-------------|----|------------------------|------|------------------------|-------|-------|------------|-----------------------------|-------|------------|
|             |    |                        | w/w  | Actual                 | RI    | EC    | Gravimetry | RI                          | EC    | Gravimetry |
| WCS         | 1  | RO- 40/60 <sup>1</sup> | 0.99 | 0.990                  | 0.997 | 0.982 | 1.013      | 0.043                       | 0.056 | 0.156      |
|             | 2  |                        | 0.95 | 0.950                  | 0.951 | 0.940 | 0.960      | 0.009                       | 0.073 | 0.072      |
|             | 3  |                        | 0.75 | 0.750                  | 0.751 | 0.734 | 0.754      | 0.007                       | 0.139 | 0.038      |
|             | 4  |                        | 0.50 | 0.500                  | 0.493 | 0.487 | 0.503      | 0.098                       | 0.174 | 0.046      |
|             | 5  |                        | 0.25 | 0.250                  | 0.251 | 0.244 | 0.254      | 0.032                       | 0.147 | 0.094      |
|             | 6  |                        | 0.05 | 0.050                  | 0.053 | 0.048 | 0.053      | 0.363                       | 0.288 | 0.428      |
|             | 7  |                        | 0.01 | 0.010                  | 0.012 | 0.008 | 0.013      | 1.150                       | 1.679 | 1.953      |

|               |   |                       |      |       |       |       |       |              |              |              |
|---------------|---|-----------------------|------|-------|-------|-------|-------|--------------|--------------|--------------|
|               | 8 | RO-100 <sup>2</sup>   | 0.75 | 0.750 | 0.749 | 0.735 | 0.757 | 0.006        | 0.136        | 0.060        |
|               | 9 | RO-10/90 <sup>3</sup> | 0.75 | 0.749 | 0.749 | 0.736 | 0.746 | 0.003        | 0.117        | 0.027        |
| $\sum AARD\%$ |   |                       |      |       |       |       |       | <b>1.711</b> | <b>2.809</b> | <b>2.874</b> |

72  
73  
74  
75  
76  
77  
78  
79

**Notes:**

- <sup>1</sup> oleic phase is 40/60 wt% toluene/bitumen.
- <sup>2</sup> oleic phase is 100 wt% bitumen.
- <sup>3</sup> oleic phase is 90/10 wt% toluene/bitumen.
- For samples WCS#6 and WCS#7, 100 g of RO water was added to the emulsion sample after measuring its volume to facilitate representative aqueous sampling.
- For samples WCS#8 and WCS#9, 100 g of toluene was added to the emulsion sample after measuring its volume to reduce the viscosity of the oleic phase and enable the salt to reach all water droplets in the water-in-oil emulsion.

**80 Salinity-RI calibration curve for unknown emulsion samples**

81 The salinity–RI calibration curve was established using synthetic brine samples prepared with  
82 known quantities of salt and brine volume. The weight of salt added, and the corresponding volume  
83 of brine used to prepare each calibration solution are reported in **Table A-6**. Brine salinities were  
84 calculated from these prepared concentrations, and subsequently, RI values were measured for  
85 each solution. A correlation between measured salinity and RI was then developed, yielding the  
86 calibration curve used to estimate the aqueous-phase salinity in unknown emulsion samples. This  
87 calibration relationship ensures accurate determination of salinity from RI measurements during  
88 the analysis of emulsions with unknown composition.

89 **Table A-6**-Weights of NaCl and volumes of brine used for generating salinity-RI calibration curve  
90 for unknown emulsion samples.

| Sample Name | S# | Source aqueous phase | $W_{NaCl}$ | $V_{brine}$ | Avg. RI | $C_{NaCl}$           |
|-------------|----|----------------------|------------|-------------|---------|----------------------|
|             |    |                      | g          | mL          | nD      | $g_{NaCl}/L_{brine}$ |
| RICS        | 1  | UES#1                | 0.3209     | 10.25       | 1.33863 | 31.307               |
|             | 2  | UES#1                | 0.6138     | 10.35       | 1.34324 | 59.304               |
|             | 3  | UES#2                | 0.3056     | 10.25       | 1.33841 | 29.815               |
|             | 4  | UES#2                | 0.6184     | 11.5        | 1.34231 | 53.774               |
|             | 5  | UES#3                | 0.3187     | 10.3        | 1.33857 | 30.942               |
|             | 6  | UES#3                | 0.6075     | 10.75       | 1.34279 | 56.512               |
|             | 7  | UES#4                | 0.3021     | 10.25       | 1.33831 | 29.473               |

|  |   |       |        |      |         |        |
|--|---|-------|--------|------|---------|--------|
|  | 8 | UES#4 | 0.6017 | 10.4 | 1.34210 | 57.856 |
|--|---|-------|--------|------|---------|--------|

91

92 **Salinity-EC calibration curve for unknown emulsion samples**

93 The salinity–EC calibration curve was developed using synthetic brine solutions prepared with  
 94 precisely measured amounts of salt and RO water. The weight of salt added, and the volume of  
 95 brine used to prepare each solution are reported in **Table A-7**. Brine salinities were calculated  
 96 based on the known concentrations of these solutions, and the corresponding EC values were  
 97 measured using conductivity meter. The obtained salinity values were then correlated with the  
 98 measured EC to establish a calibration relationship. This curve is used to determine the salinity of  
 99 the aqueous phase in unknown emulsion samples by measuring their EC, enabling accurate and  
 100 reliable phase characterization.

101 **Table A-7**-Weights of NaCl and volumes of brine used for generating salinity-EC calibration for  
 102 unknown emulsion samples.

| Sample name | S# | Source aqueous phase | $W_{NaCl}$ | $V_{brine}$ | Avg. EC          | $C_{NaCl}$           |
|-------------|----|----------------------|------------|-------------|------------------|----------------------|
|             |    |                      | g          | mL          | $\mu\text{S/cm}$ | $g_{NaCl}/L_{brine}$ |
| ECCS        | 1  | UES#24               | 0.0000     | 35.055      | 216              | 0.0000               |
|             | 2  | UES#24               | 1.0853     | 35.912      | 47543            | 30.221               |
|             | 3  | UES#24               | 2.0038     | 36.001      | 81473            | 55.659               |
|             | 4  | UES#24               | 3.1069     | 36.549      | 117349           | 85.006               |

103 **Water cut measurement for unknown actual emulsion samples**

104 For unknown actual emulsion samples, the salinity and volume of the aqueous phase were  
 105 determined using two indirect methods—RI and EC—based on the previously established  
 106 calibration curves. The measured aqueous-phase volumes obtained from these methods are  
 107 reported in **Table A-8**, alongside the aqueous-phase volumes determined by the centrifuge method.

108 **Table A-8**-Volumes of emulsions (achieved from Boyle’s law) and volumes of aqueous phase for  
 109 each unknown emulsion sample obtained using RI, EC, and centrifuge techniques collected during  
 110 the SAGD experiment.

| Sample name | S# | $V_{emulsion}$<br>mL | $W_{NaCl}$<br>g | RI method |                                       |             | EC method |                                       |             | Centrifuge method |
|-------------|----|----------------------|-----------------|-----------|---------------------------------------|-------------|-----------|---------------------------------------|-------------|-------------------|
|             |    |                      |                 | RI        | $C_{NaCl}$                            | $V_{water}$ | EC        | $C_{NaCl}$                            | $V_{water}$ | $V_{water}$       |
|             |    |                      |                 | nD        | g <sub>salt</sub> /L <sub>brine</sub> | mL          | μS/cm     | g <sub>salt</sub> /L <sub>brine</sub> | mL          | mL                |
| UES         | 1  | 747.250              | 34.9934         | 1.34289   | 57.177                                | 595.90      | 84086     | 58.984                                | 577.14      | 611.87            |
|             | 2  | 772.862              | 35.0198         | 1.34330   | 59.673                                | 570.72      | 85713     | 60.164                                | 565.93      | 582.86            |
|             | 3  | 736.969              | 34.9700         | 1.34420   | 65.133                                | 520.79      | 91765     | 64.550                                | 525.64      | 550.38            |
|             | 4  | 763.044              | 35.0029         | 1.34357   | 61.297                                | 554.91      | 88581     | 62.242                                | 546.24      | 491.87            |
|             | 5  | 773.525              | 35.1145         | 1.34308   | 58.313                                | 585.99      | 83880     | 58.835                                | 580.64      | 529.82            |
|             | 6  | 773.421              | 35.0204         | 1.34300   | 57.806                                | 589.69      | 83873     | 58.830                                | 579.14      | 546.86            |
|             | 7  | 773.765              | 35.2744         | 1.34289   | 57.156                                | 600.90      | 83654     | 58.672                                | 584.96      | 591.74            |
|             | 8  | 773.447              | 35.0759         | 1.34530   | 71.810                                | 472.29      | 102691    | 72.468                                | 467.86      | 462.84            |
|             | 9  | 727.514              | 35.2066         | 1.34389   | 63.225                                | 540.62      | 92999     | 65.444                                | 521.74      | 590.28            |
|             | 10 | 729.438              | 35.1881         | 1.34399   | 63.854                                | 534.85      | 89278     | 62.747                                | 544.57      | 552.78            |
|             | 11 | 710.155              | 35.0028         | 1.34679   | 80.882                                | 416.63      | 114243    | 80.840                                | 416.86      | 466.87            |
|             | 12 | 826.761              | 35.1997         | 1.34506   | 70.369                                | 483.99      | 101620    | 71.692                                | 474.77      | 484.78            |
|             | 13 | 798.724              | 35.0011         | 1.34704   | 82.425                                | 408.51      | 118341    | 83.810                                | 401.49      | 419.87            |
|             | 14 | 823.706              | 35.0886         | 1.34461   | 67.609                                | 502.82      | 98158     | 69.183                                | 491.02      | 494.83            |
|             | 15 | 780.227              | 35.0638         | 1.34545   | 72.744                                | 465.86      | 104597    | 73.850                                | 458.64      | 476.84            |
|             | 16 | 751.983              | 35.0159         | 1.34487   | 69.232                                | 489.64      | 100448    | 70.842                                | 478.14      | 494.86            |
|             | 17 | 887.418              | 35.1332         | 1.34425   | 65.437                                | 520.71      | 96015     | 67.630                                | 503.30      | 543.81            |
|             | 18 | 770.647              | 35.1593         | 1.34634   | 78.142                                | 433.74      | 111052    | 78.527                                | 431.53      | 484.80            |
|             | 19 | 795.744              | 35.3067         | 1.34404   | 64.159                                | 534.03      | 91712     | 64.512                                | 531.02      | 546.73            |
|             | 20 | 838.337              | 35.2099         | 1.34364   | 61.723                                | 554.22      | 90248     | 63.451                                | 538.69      | 582.77            |
|             | 21 | 816.541              | 35.3544         | 1.34251   | 54.843                                | 628.36      | 79564     | 55.707                                | 618.35      | 642.71            |
|             | 22 | 774.492              | 35.5500         | 1.34191   | 51.189                                | 678.10      | 74253     | 51.858                                | 669.14      | 642.62            |
|             | 23 | 1039.63<br>1         | 35.2974         | 1.34005   | 39.864                                | 869.17      | 58028     | 40.100                                | 863.97      | 840.73            |
|             | 24 | 740.993              | 35.2974         | 1.34250   | 54.782                                | 628.06      | 78691     | 55.075                                | 624.63      | 612.73            |

111 Using the measured aqueous phase volumes and the total emulsion volume, the volumetric water  
 112 cuts (v/v) were calculated for each sample. The resulting volumetric water cuts (v/v) derived from  
 113 the three methods—RI, EC, and centrifuge—are summarized in **Table A-9**. These results allow  
 114 for a comparative assessment of the accuracy and reliability of the RI and EC techniques.

115 **Table A-9**-Volume of water and volumetric water cut (v/v) obtained using RI, EC, and  
 116 centrifuge methods, for unknown emulsion samples.

| Sample name | S# | $V_{emulsion}$ | Calculation obtained from RI |      | Calculation obtained from EC |      | Calculation obtained from centrifuge |      |
|-------------|----|----------------|------------------------------|------|------------------------------|------|--------------------------------------|------|
|             |    |                | $V_{water}$                  | WC   | $V_{water}$                  | WC   | $V_{water}$                          | WC   |
|             |    | mL             | mL                           | v/v  | mL                           | v/v  | mL                                   | v/v  |
| UES         | 1  | 747.25         | 595.90                       | 0.80 | 577.14                       | 0.77 | 611.87                               | 0.82 |
|             | 2  | 772.86         | 570.72                       | 0.74 | 565.93                       | 0.73 | 582.86                               | 0.75 |
|             | 3  | 736.97         | 520.79                       | 0.71 | 525.64                       | 0.71 | 550.38                               | 0.75 |
|             | 4  | 763.05         | 554.91                       | 0.73 | 546.24                       | 0.72 | 491.87                               | 0.64 |
|             | 5  | 773.52         | 585.99                       | 0.76 | 580.64                       | 0.75 | 529.82                               | 0.68 |
|             | 6  | 773.42         | 589.69                       | 0.76 | 579.14                       | 0.75 | 546.86                               | 0.71 |
|             | 7  | 773.77         | 600.90                       | 0.78 | 584.96                       | 0.76 | 591.74                               | 0.76 |
|             | 8  | 773.44         | 472.29                       | 0.61 | 467.86                       | 0.60 | 462.84                               | 0.60 |
|             | 9  | 727.52         | 540.62                       | 0.74 | 521.74                       | 0.72 | 590.28                               | 0.81 |
|             | 10 | 729.43         | 534.85                       | 0.73 | 544.57                       | 0.75 | 552.78                               | 0.76 |
|             | 11 | 710.16         | 416.63                       | 0.59 | 416.86                       | 0.59 | 466.87                               | 0.66 |
|             | 12 | 826.76         | 483.99                       | 0.59 | 474.77                       | 0.57 | 484.78                               | 0.59 |
|             | 13 | 798.72         | 408.51                       | 0.51 | 401.49                       | 0.50 | 419.87                               | 0.53 |
|             | 14 | 823.63         | 502.82                       | 0.61 | 491.02                       | 0.60 | 494.83                               | 0.60 |
|             | 15 | 780.3          | 465.86                       | 0.60 | 458.64                       | 0.59 | 476.84                               | 0.61 |
|             | 16 | 751.9          | 489.64                       | 0.65 | 478.14                       | 0.64 | 494.86                               | 0.66 |
|             | 17 | 887.5          | 520.71                       | 0.59 | 503.30                       | 0.57 | 543.81                               | 0.61 |
|             | 18 | 770.6          | 433.74                       | 0.56 | 431.53                       | 0.56 | 484.80                               | 0.63 |
|             | 19 | 795.8          | 534.03                       | 0.67 | 531.02                       | 0.67 | 546.73                               | 0.69 |
|             | 20 | 838.3          | 554.22                       | 0.66 | 538.69                       | 0.64 | 582.77                               | 0.70 |
|             | 21 | 816.5          | 628.36                       | 0.77 | 618.35                       | 0.76 | 642.71                               | 0.79 |
|             | 22 | 774.5          | 678.10                       | 0.88 | 669.14                       | 0.86 | 642.62                               | 0.83 |
|             | 23 | 1039.7         | 869.17                       | 0.84 | 863.97                       | 0.83 | 840.73                               | 0.81 |
|             | 24 | 740.9          | 628.06                       | 0.85 | 624.63                       | 0.84 | 612.73                               | 0.83 |

117

118