

Supplementary Information (SI)

for

Refractometric and Conductivity Based Water Cut Measurement Techniques for Stable Emulsions

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Supplementary Information (SI)

This Supplementary Information (SI) file presents tables containing both raw and calculated data corresponding to the figures included in the main manuscript. The supporting tables provide data for calibration samples and for known and unknown emulsion samples. Additional details about the prepared emulsions are provided beneath each corresponding table.

Accuracy of Boyle's law for liquid volume measurements

The accuracies of Boyle's law, the volumetric method, and the fill-to-full method were evaluated using three different bottle sizes, as shown in **Table A-1**. This table presents the AARD% compared to the actual water volumes.

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Table A-1- Volumes of water measured using three methods and the AARD% relative to the actual volume of water.

| Bottle size | V_{water} measured by | | | Actual V_{water} mL | AARD relative to actual volumes | | |
|--------------|-------------------------|-------------------|---------------------|--------------------------|---------------------------------|-------------------|---------------------|
| | Boyle's law | Volumetric method | Fill to full method | | Boyle's law | Volumetric method | Fill to full method |
| | mL | | | | % | | |
| 100 mL | 80.275 | 81.0 | 80.022 | 80.232 | 0.018 | 0.319 | 0.087 |
| 500 mL | 400.862 | 404.1 | 399.783 | 400.862 | 0.000 | 0.269 | 0.090 |
| 1000 mL | 801.199 | 807.5 | 799.444 | 801.443 | 0.010 | 0.252 | 0.083 |
| \sum AARD% | | | | | 0.028 | 0.840 | 0.260 |

Volume measurement for known emulsion samples

Boyle's law parameters obtained during the total volume measurements of emulsion samples were reported in **Table A-2** for known emulsion samples. The experimentally measured emulsion volumes were compared with the corresponding ideal volumes, and the deviations were expressed as the AARD%.

Table A-2-Arithmetic average of volumes measured using Boyle’s law method and ideal volumes of known emulsion samples, along with the AARD%.

| Sample name | S# | Emulsion | WC | $P_{charging}$ | $P_{equilibrium}$ | Measured $V_{emulsion}$ | Avg. $V_{emulsion}$ | Ideal $V_{emulsion}$ | AARD | |
|----------------|-----------------------|------------------------|---------------------|----------------|-------------------|-------------------------|---------------------|----------------------|---------------|--------|
| | | | w/w | psia | | mL | | | % | |
| WCS | 1 | RO- 40/60 ^a | 0.99 | 18.133 | 15.048 | 401.80 | 401.34 | 400.92 | 0.0071 | |
| | | | | 18.130 | 15.044 | 401.33 | | | | |
| | | | | 18.080 | 15.021 | 400.91 | | | | |
| | 2 | | 0.95 | 18.100 | 15.030 | 401.04 | 401.90 | 401.80 | 0.0016 | |
| | | | | 18.104 | 15.038 | 402.12 | | | | |
| | | | | 17.991 | 14.994 | 402.53 | | | | |
| | 3 | | 0.75 | 18.139 | 15.082 | 406.99 | 407.20 | 405.87 | 0.0218 | |
| | | | | 18.097 | 15.066 | 407.23 | | | | |
| | | | | 18.167 | 15.096 | 407.37 | | | | |
| | 4 | | 0.50 | 18.105 | 15.091 | 410.73 | 411.51 | 410.90 | 0.0099 | |
| | | | | 18.102 | 15.098 | 412.05 | | | | |
| | | | | 18.019 | 15.061 | 411.74 | | | | |
| | 5 | | 0.25 | 18.032 | 15.101 | 417.22 | 416.81 | 416.02 | 0.0127 | |
| | | | | 17.946 | 15.064 | 417.20 | | | | |
| | | | | 17.954 | 15.060 | 416.02 | | | | |
| | 6 ^d | | 0.05 | 23.289 | 17.406 | 421.06 | 421.78 | 420.12 | 0.0263 | |
| | | | | 23.235 | 17.391 | 421.70 | | | | |
| | | | | 22.993 | 17.297 | 422.56 | | | | |
| | 7 ^d | | 0.01 | 17.986 | 15.114 | 422.30 | 421.97 | 421.01 | 0.0153 | |
| | | | | 18.059 | 15.135 | 420.67 | | | | |
| | | | | 17.990 | 15.120 | 422.95 | | | | |
| | 8 ^e | | RO-100 ^b | 0.75 | 24.506 | 17.649 | 400.66 | 400.50 | 398.73 | 0.0297 |
| | | | | | 23.961 | 17.424 | 400.51 | | | |
| | | | | | 23.697 | 17.314 | 400.34 | | | |
| 9 ^e | RO-10/90 ^c | 0.75 | 23.779 | 17.370 | 402.15 | 402.34 | 401.57 | 0.0127 | | |
| | | | 23.894 | 17.417 | 402.13 | | | | | |
| | | | 23.684 | 17.338 | 402.72 | | | | | |
| | | | 23.858 | 18.141 | 452.74 | | | | | |
| | | | 23.004 | 17.695 | 450.33 | | | | | |
| | | | 23.894 | 17.417 | 402.13 | | | | | |
| | | | 23.684 | 17.338 | 402.72 | | | | | |
| Σ AARD% | | | | | | | | | 0.1371 | |

Notes:

- ^a oleic phase is 40/60 wt% toluene/bitumen.
- ^b oleic phase is 100 wt% bitumen.
- ^c oleic phase is 90/10 wt% toluene/bitumen.
- ^d for samples WCS#6 and WCS#7, 100 g of RO water was added to the emulsion sample after measuring its volume to facilitate representative aqueous sampling.
- ^e for samples WCS#8 and WCS#9, 100 g of toluene was added to the emulsion sample after measuring its volume to reduce the viscosity of the oleic phase and enable salt to reach all water droplets in the water-in-oil emulsion.

Brine salinity measurement for known emulsion samples

Brine salinities for known emulsion samples were determined using three analytical techniques:

RI, EC, and gravimetry. The volume of water corresponding to these salinity values was calculated

and reported in **Table A-3**. The accuracy of the measured water volumes was evaluated by comparing them with the actual water volumes in the known emulsion samples, with deviations expressed as the AARD%.

Table A-3-The volume of water obtained using the RI, EC, and gravimetry methods, along with their corresponding AARD% for known emulsion samples prepared for water cut measurements.

| Sample name | S# | Emulsion | WC | V_{water} (mL) | | | | AARD (%) | | |
|--------------|----------------|------------------------|------|------------------|--------|--------|------------|--------------|--------------|--------------|
| | | | w/w | Actual | RI | EC | Gravimetry | RI | EC | Gravimetry |
| WCS | 1 | RO- 40/60 ^a | 0.99 | 396.78 | 399.33 | 393.47 | 406.08 | 0.043 | 0.056 | 0.156 |
| | 2 | | 0.95 | 380.7 | 381.20 | 376.55 | 384.83 | 0.009 | 0.073 | 0.072 |
| | 3 | | 0.75 | 300.55 | 300.88 | 294.28 | 302.26 | 0.007 | 0.139 | 0.038 |
| | 4 | | 0.50 | 200.36 | 197.42 | 195.12 | 201.72 | 0.098 | 0.174 | 0.045 |
| | 5 | | 0.25 | 100.18 | 100.66 | 97.97 | 101.59 | 0.032 | 0.147 | 0.094 |
| | 6 ^d | | 0.05 | 20.05 | 21.14 | 19.18 | 21.33 | 0.362 | 0.289 | 0.426 |
| | 7 ^d | | 0.01 | 4.03 | 4.72 | 3.01 | 5.21 | 1.141 | 1.687 | 1.952 |
| | 8 ^e | RO-100 ^b | 0.75 | 300.57 | 300.31 | 294.45 | 303.29 | 0.006 | 0.136 | 0.060 |
| | 9 ^e | RO-10/90 ^c | 0.75 | 300.52 | 300.35 | 295.19 | 299.28 | 0.004 | 0.118 | 0.028 |
| \sum AARD% | | | | | | | | 1.702 | 2.819 | 2.871 |

Notes:

- ^a oleic phase is 40/60 wt% toluene/bitumen.
- ^b oleic phase is 100 wt% bitumen.
- ^c oleic phase is 90/10 wt% toluene/bitumen.
- ^d for samples WCS#6 and WCS#7, 100 g of RO water was added to the emulsion sample after measuring its volume to facilitate representative aqueous sampling.
- ^e for samples WCS#8 and WCS#9, 100 g of toluene was added to the emulsion sample after measuring its volume to reduce the viscosity of the oleic phase and enable the salt to reach all water droplets in the water-in-oil emulsion.

Water cuts measurement for known emulsion samples

Following the determination of the total emulsion volume and the quantification of the aqueous phase, both volumetric (v/v) and mass-based (w/w) water cuts were calculated for the known emulsion samples. The measured volumetric water cuts (v/v) and mass water cuts (w/w) were then compared with the actual (reference) water cut values. The results, including the deviations from the true values, are presented in **Tables A-4** and **A-5**, respectively. The accuracy of the

measurements was assessed by calculating the AARD% to evaluate the performance of the methods used in measuring water cut under the tested conditions.

Table A-4- Volumetric water cuts (v/v) and corresponding AARD% for known emulsion samples measured using RI, EC, and gravimetry techniques compared to actual volumetric water cuts (v/v).

| Sample name | S# | Emulsion | WC | WC (v/v) | | | | AARD% relative to actual WC | | |
|--------------|----------------|------------------------|------|----------|-------|-------|------------|-----------------------------|--------------|--------------|
| | | | w/w | Actual | RI | EC | Gravimetry | RI | EC | Gravimetry |
| WCS | 1 | RO- 40/60 ^a | 0.99 | 0.990 | 0.995 | 0.980 | 1.012 | 0.036 | 0.063 | 0.149 |
| | 2 | | 0.95 | 0.947 | 0.949 | 0.937 | 0.958 | 0.007 | 0.074 | 0.071 |
| | 3 | | 0.75 | 0.741 | 0.739 | 0.723 | 0.742 | 0.014 | 0.160 | 0.016 |
| | 4 | | 0.50 | 0.488 | 0.480 | 0.474 | 0.490 | 0.107 | 0.184 | 0.035 |
| | 5 | | 0.25 | 0.241 | 0.242 | 0.235 | 0.244 | 0.020 | 0.160 | 0.081 |
| | 6 ^d | | 0.05 | 0.048 | 0.050 | 0.045 | 0.051 | 0.333 | 0.314 | 0.398 |
| | 7 ^d | | 0.01 | 0.010 | 0.011 | 0.007 | 0.012 | 1.126 | 1.694 | 1.927 |
| | 8 ^e | RO-100 ^b | 0.75 | 0.754 | 0.750 | 0.735 | 0.757 | 0.035 | 0.165 | 0.030 |
| | 9 ^e | RO-10/90 ^c | 0.75 | 0.748 | 0.747 | 0.734 | 0.744 | 0.017 | 0.131 | 0.040 |
| \sum AARD% | | | | | | | | 1.695 | 2.945 | 2.747 |

Notes:

- ^a oleic phase is 40/60 wt% toluene/bitumen.
- ^b oleic phase is 100 wt% bitumen.
- ^c oleic phase is 90/10 wt% toluene/bitumen.
- ^d for samples WCS#6 and WCS#7, 100 g of RO water was added to the emulsion sample after measuring its volume to facilitate representative aqueous sampling.
- ^e for samples WCS#8 and WCS#9, 100 g of toluene was added to the emulsion sample after measuring its volume to reduce the viscosity of the oleic phase and enable the salt to reach all water droplets in the water-in-oil emulsion.

Table A-5-Mass water cuts (w/w) and corresponding AARD% for known emulsion samples measured using RI, EC, and gravimetry techniques compared to actual mass water cuts (w/w).

| Sample name | S# | Emulsion | WC | WC (w/w) obtained from | | | | AARD% relative to actual WC | | |
|--------------|----------------|------------------------|------|------------------------|-------|-------|------------|-----------------------------|--------------|--------------|
| | | | w/w | Actual | RI | EC | Gravimetry | RI | EC | Gravimetry |
| WCS | 1 | RO- 40/60 ^a | 0.99 | 0.990 | 0.997 | 0.982 | 1.013 | 0.043 | 0.056 | 0.156 |
| | 2 | | 0.95 | 0.950 | 0.951 | 0.940 | 0.960 | 0.009 | 0.073 | 0.072 |
| | 3 | | 0.75 | 0.750 | 0.751 | 0.734 | 0.754 | 0.007 | 0.139 | 0.038 |
| | 4 | | 0.50 | 0.500 | 0.493 | 0.487 | 0.503 | 0.098 | 0.174 | 0.046 |
| | 5 | | 0.25 | 0.250 | 0.251 | 0.244 | 0.254 | 0.032 | 0.147 | 0.094 |
| | 6 ^d | | 0.05 | 0.050 | 0.053 | 0.048 | 0.053 | 0.363 | 0.288 | 0.428 |
| | 7 ^d | | 0.01 | 0.010 | 0.012 | 0.008 | 0.013 | 1.150 | 1.679 | 1.953 |
| | 8 ^e | RO-100 ^b | 0.75 | 0.750 | 0.749 | 0.735 | 0.757 | 0.006 | 0.136 | 0.060 |
| | 9 ^e | RO-10/90 ^c | 0.75 | 0.749 | 0.749 | 0.736 | 0.746 | 0.003 | 0.117 | 0.027 |
| \sum AARD% | | | | | | | | 1.711 | 2.809 | 2.874 |

Notes:

- ^a oleic phase is 40/60 wt% toluene/bitumen.
- ^b oleic phase is 100 wt% bitumen.
- ^c oleic phase is 90/10 wt% toluene/bitumen.
- ^d for samples WCS#6 and WCS#7, 100 g of RO water was added to the emulsion sample after measuring its volume to facilitate representative aqueous sampling.
- ^e for samples WCS#8 and WCS#9, 100 g of toluene was added to the emulsion sample after measuring its volume to reduce the viscosity of the oleic phase and enable the salt to reach all water droplets in the water-in-oil emulsion.

Salinity-RI calibration curve for unknown emulsion samples

The salinity–RI calibration curve was established using 10 mL of the aqueous phase collected from each of the first four unknown emulsion samples (UES#1–#4). Sodium chloride was added to the calibration samples: 0.3 g was added to the first group (RICS#1, #3, #5, #7), and 0.6 g was added to the second group (RICS#2, #4, #6, #8). The weight of salt added, and the corresponding volume of brine used to prepare each calibration solution are reported in **Table A-6**. Brine salinities were calculated for these prepared concentrations, and subsequently, RI values were measured for each solution. A correlation between measured salinity and RI was then developed, yielding the calibration curve used to estimate the aqueous-phase salinity in unknown emulsion samples. This calibration relationship ensures accurate determination of salinity from RI measurements during the analysis of emulsions with unknown composition.

Table A-6-Weights of NaCl, source of aqueous phase, and volumes of brine used for generating salinity-RI calibration curve for unknown emulsion samples.

| Sample Name | S# | Source aqueous phase | W_{NaCl} | V_{brine} | Avg. RI | C_{NaCl} |
|-------------|----|----------------------|------------|-------------|---------|----------------------|
| | | | g | mL | nD | g_{NaCl}/L_{brine} |
| RICS | 1 | UES#1 | 0.3209 | 10.25 | 1.33863 | 31.307 |
| | 2 | UES#1 | 0.6138 | 10.35 | 1.34324 | 59.304 |
| | 3 | UES#2 | 0.3056 | 10.25 | 1.33841 | 29.815 |
| | 4 | UES#2 | 0.6184 | 11.5 | 1.34231 | 53.774 |
| | 5 | UES#3 | 0.3187 | 10.3 | 1.33857 | 30.942 |
| | 6 | UES#3 | 0.6075 | 10.75 | 1.34279 | 56.512 |
| | 7 | UES#4 | 0.3021 | 10.25 | 1.33831 | 29.473 |
| | 8 | UES#4 | 0.6017 | 10.4 | 1.34210 | 57.856 |

Salinity-EC calibration curve for unknown emulsion samples

The salinity–EC calibration curve was developed using four calibration samples (EC calibration samples, ECCS#1–#4). Each calibration sample consisted of a 35 mL aqueous phase taken from the final collected unknown emulsion sample (UES#24). Sodium chloride was added to three of the samples: 1 g of NaCl to the second sample (ECCS#2), 2 g to the third sample (ECCS#3), and 3 g to the fourth sample (ECCS#4), while the first sample (ECCS#1) remained free of NaCl. The weight of salt added, source of aqueous phase, and the volume of brine used to prepare each solution are reported in **Table A-7**. Brine salinities of these samples were calculated, and the corresponding EC values were measured using conductivity meter. The obtained salinity values were then correlated with the measured EC to establish a calibration relationship. This curve is used to determine the salinity of the aqueous phase in unknown emulsion samples by measuring their EC, enabling accurate and reliable phase characterization.

Table A-7-Weights of NaCl and volumes of brine used for generating salinity-EC calibration for unknown emulsion samples.

| Sample name | S# | Source aqueous phase | W_{NaCl} | V_{brine} | Avg. EC | C_{NaCl} |
|-------------|----|----------------------|------------|-------------|------------------|----------------------|
| | | | g | mL | $\mu\text{S/cm}$ | g_{NaCl}/L_{brine} |
| ECCS | 1 | UES#24 | 0.0000 | 35.055 | 216 | 0.0000 |
| | 2 | UES#24 | 1.0853 | 35.912 | 47543 | 30.221 |
| | 3 | UES#24 | 2.0038 | 36.001 | 81473 | 55.659 |
| | 4 | UES#24 | 3.1069 | 36.549 | 117349 | 85.006 |

Water cut measurement for unknown actual emulsion samples

For unknown actual emulsion samples, the salinity and volume of the aqueous phase were determined using two indirect methods—RI and EC—based on the previously established calibration curves. The measured aqueous-phase volumes obtained from these methods are reported in **Table A-8**, alongside the aqueous-phase volumes determined by the centrifuge method.

Table A-8- Volumes of emulsions (achieved from Boyle’s law) and volumes of aqueous phase for each unknown emulsion sample obtained using RI, EC, and centrifuge techniques collected during the SAGD experiment.

| Sample name | S# | $V_{emulsion}$ | W_{NaCl} | RI method | | | EC method | | | Centrifuge method |
|-------------|----|----------------|------------|-----------|------------------------------|-------------|------------|------------------------------|-------------|-------------------|
| | | | | RI | C_{NaCl} | V_{water} | EC | C_{NaCl} | V_{water} | V_{water} |
| | | | | nD | $\frac{g_{salt}}{L_{brine}}$ | mL | $\mu S/cm$ | $\frac{g_{salt}}{L_{brine}}$ | mL | mL |
| UES | 1 | 747.250 | 34.9934 | 1.34289 | 57.177 | 595.90 | 84086 | 58.984 | 577.14 | 611.87 |
| | 2 | 772.862 | 35.0198 | 1.34330 | 59.673 | 570.72 | 85713 | 60.164 | 565.93 | 582.86 |
| | 3 | 736.969 | 34.9700 | 1.34420 | 65.133 | 520.79 | 91765 | 64.550 | 525.64 | 550.38 |
| | 4 | 763.044 | 35.0029 | 1.34357 | 61.297 | 554.91 | 88581 | 62.242 | 546.24 | 491.87 |
| | 5 | 773.525 | 35.1145 | 1.34308 | 58.313 | 585.99 | 83880 | 58.835 | 580.64 | 529.82 |
| | 6 | 773.421 | 35.0204 | 1.34300 | 57.806 | 589.69 | 83873 | 58.830 | 579.14 | 546.86 |
| | 7 | 773.765 | 35.2744 | 1.34289 | 57.156 | 600.90 | 83654 | 58.672 | 584.96 | 591.74 |
| | 8 | 773.447 | 35.0759 | 1.34530 | 71.810 | 472.29 | 102691 | 72.468 | 467.86 | 462.84 |
| | 9 | 727.514 | 35.2066 | 1.34389 | 63.225 | 540.62 | 92999 | 65.444 | 521.74 | 590.28 |
| | 10 | 729.438 | 35.1881 | 1.34399 | 63.854 | 534.85 | 89278 | 62.747 | 544.57 | 552.78 |
| | 11 | 710.155 | 35.0028 | 1.34679 | 80.882 | 416.63 | 114243 | 80.840 | 416.86 | 466.87 |
| | 12 | 826.761 | 35.1997 | 1.34506 | 70.369 | 483.99 | 101620 | 71.692 | 474.77 | 484.78 |
| | 13 | 798.724 | 35.0011 | 1.34704 | 82.425 | 408.51 | 118341 | 83.810 | 401.49 | 419.87 |
| | 14 | 823.706 | 35.0886 | 1.34461 | 67.609 | 502.82 | 98158 | 69.183 | 491.02 | 494.83 |
| | 15 | 780.227 | 35.0638 | 1.34545 | 72.744 | 465.86 | 104597 | 73.850 | 458.64 | 476.84 |
| | 16 | 751.983 | 35.0159 | 1.34487 | 69.232 | 489.64 | 100448 | 70.842 | 478.14 | 494.86 |
| | 17 | 887.418 | 35.1332 | 1.34425 | 65.437 | 520.71 | 96015 | 67.630 | 503.30 | 543.81 |
| | 18 | 770.647 | 35.1593 | 1.34634 | 78.142 | 433.74 | 111052 | 78.527 | 431.53 | 484.80 |
| | 19 | 795.744 | 35.3067 | 1.34404 | 64.159 | 534.03 | 91712 | 64.512 | 531.02 | 546.73 |
| | 20 | 838.337 | 35.2099 | 1.34364 | 61.723 | 554.22 | 90248 | 63.451 | 538.69 | 582.77 |
| | 21 | 816.541 | 35.3544 | 1.34251 | 54.843 | 628.36 | 79564 | 55.707 | 618.35 | 642.71 |
| | 22 | 774.492 | 35.5500 | 1.34191 | 51.189 | 678.10 | 74253 | 51.858 | 669.14 | 642.62 |
| | 23 | 1039.63 1 | 35.2974 | 1.34005 | 39.864 | 869.17 | 58028 | 40.100 | 863.97 | 840.73 |
| | 24 | 740.993 | 35.2974 | 1.34250 | 54.782 | 628.06 | 78691 | 55.075 | 624.63 | 612.73 |

Using the measured aqueous phase volumes and the total emulsion volume, the volumetric water cuts (v/v) were calculated for each sample. The resulting volumetric water cuts (v/v) derived from the three methods—RI, EC, and centrifuge—are summarized in **Table A-9**. These results allow for a comparative assessment of the accuracy and reliability of the RI and EC techniques.

Table A-9-Volume of water and volumetric water cut (v/v) obtained using RI, EC, and centrifuge methods, for unknown emulsion samples.

| Sample name | S# | $V_{emulsion}$ | Calculation obtained from RI | | Calculation obtained from EC | | Calculation obtained from centrifuge | |
|-------------|----|----------------|------------------------------|------|------------------------------|------|--------------------------------------|------|
| | | | V_{water} | WC | V_{water} | WC | V_{water} | WC |
| | | mL | mL | v/v | mL | v/v | mL | v/v |
| UES | 1 | 747.25 | 595.90 | 0.80 | 577.14 | 0.77 | 611.87 | 0.82 |
| | 2 | 772.86 | 570.72 | 0.74 | 565.93 | 0.73 | 582.86 | 0.75 |
| | 3 | 736.97 | 520.79 | 0.71 | 525.64 | 0.71 | 550.38 | 0.75 |
| | 4 | 763.05 | 554.91 | 0.73 | 546.24 | 0.72 | 491.87 | 0.64 |
| | 5 | 773.52 | 585.99 | 0.76 | 580.64 | 0.75 | 529.82 | 0.68 |
| | 6 | 773.42 | 589.69 | 0.76 | 579.14 | 0.75 | 546.86 | 0.71 |
| | 7 | 773.77 | 600.90 | 0.78 | 584.96 | 0.76 | 591.74 | 0.76 |
| | 8 | 773.44 | 472.29 | 0.61 | 467.86 | 0.60 | 462.84 | 0.60 |
| | 9 | 727.52 | 540.62 | 0.74 | 521.74 | 0.72 | 590.28 | 0.81 |
| | 10 | 729.43 | 534.85 | 0.73 | 544.57 | 0.75 | 552.78 | 0.76 |
| | 11 | 710.16 | 416.63 | 0.59 | 416.86 | 0.59 | 466.87 | 0.66 |
| | 12 | 826.76 | 483.99 | 0.59 | 474.77 | 0.57 | 484.78 | 0.59 |
| | 13 | 798.72 | 408.51 | 0.51 | 401.49 | 0.50 | 419.87 | 0.53 |
| | 14 | 823.63 | 502.82 | 0.61 | 491.02 | 0.60 | 494.83 | 0.60 |
| | 15 | 780.3 | 465.86 | 0.60 | 458.64 | 0.59 | 476.84 | 0.61 |
| | 16 | 751.9 | 489.64 | 0.65 | 478.14 | 0.64 | 494.86 | 0.66 |
| | 17 | 887.5 | 520.71 | 0.59 | 503.30 | 0.57 | 543.81 | 0.61 |
| | 18 | 770.6 | 433.74 | 0.56 | 431.53 | 0.56 | 484.80 | 0.63 |
| | 19 | 795.8 | 534.03 | 0.67 | 531.02 | 0.67 | 546.73 | 0.69 |
| | 20 | 838.3 | 554.22 | 0.66 | 538.69 | 0.64 | 582.77 | 0.70 |
| | 21 | 816.5 | 628.36 | 0.77 | 618.35 | 0.76 | 642.71 | 0.79 |
| | 22 | 774.5 | 678.10 | 0.88 | 669.14 | 0.86 | 642.62 | 0.83 |
| | 23 | 1039.7 | 869.17 | 0.84 | 863.97 | 0.83 | 840.73 | 0.81 |
| | 24 | 740.9 | 628.06 | 0.85 | 624.63 | 0.84 | 612.73 | 0.83 |