

## Supporting Information

### **Boosting the Thermoelectric Performance of SnTe through Localized van der Waals Gaps construction and Configurational-Entropy Engineering**

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## Experimental section

### 1. Synthesis

This work uses conventional melting methods to synthesize high quality polycrystalline ingots of  $(\text{SnTe})_{0.85}(\text{Ag}_{1-\delta}\text{Sb}_{1+\delta}\text{Te}_{2+\delta})_{0.15}$  ( $\delta = 0, 0.1, 0.2, 0.3$ ) and  $(\text{Sn}_{1-x-y-z-w}\text{Pb}_x\text{Ge}_y\text{Nd}_z\text{In}_w\text{Te})_{0.85}(\text{Ag}_{0.8}\text{Sb}_{1.2}\text{Te}_{2.2})_{0.15}$  ( $x = 0.15, y = z = w = 0$ ;  $x = 0.15, y = 0.05, z = w = 0$ ;  $x = 0.15, y = 0.05, z = 0.005, w = 0$ ;  $x = 0.15, y = 0.05, z = w = 0.005$ ). Stoichiometric amounts of highly pure Sn (99.99%, Aladdin), Ag (99.99%, Alfa Aesar), Sb (99.99%, Aladdin), Te (99.99%, Aex), Ge (99.99%, Alfa Aesar), Pb (99.99%, Aladdin), In (99.99%, Aladdin), Nd (99%, Aex) elements were mixed and sealed in carbon-coated quartz tubes under a vacuum of  $\sim 10^{-4}$  Pa. The raw materials were heated up to 673 K firstly and held at this temperature for 2 hours, then heated to 1273 K and held for another 18 hours, then quenched in cold water and further annealed at 873 K for 48 h and furnace cooled to room temperature. Afterwards, the as-obtained ingots were hand milled to fine powders by a mortar and pestle. The obtained powders were subsequently pressed into pellets with a spark plasma sintering (SPS, LABOX-212) method; the sintering temperature, holding time, and uniaxial pressure were 773 K, 5 minutes and 50 MPa, respectively. The obtained pellets were cut into  $2 \times 2 \times 12$  mm<sup>3</sup> cuboids for electrical transport measurements and  $6 \times 6 \times 2$  mm<sup>3</sup> cubic pellets for thermal expansion coefficient measurements.

### 2. Characterization

The crystal structure of the sample was characterised using an X-ray powder diffractometer (MiniFlex 600, Rigaku). The test parameters are set as: Cu K $\alpha$  radiation source ( $\lambda = 1.5418$  Å, 40 kV, 40 mA), with a scanning rate of  $10^\circ \text{ min}^{-1}$  from  $2\theta = 20^\circ$  to  $80^\circ$ . The scanning range of  $2\theta$  was  $20\text{-}80^\circ$  with a scanning speed of  $6^\circ/\text{min}$ . Scanning electron microscope (SEM, SUB8020, Japan) equipped with energy dispersive spectroscopy (EDS) was used to detect its microstructure and corresponding elements distribution at micron-scale level. Transmission electron microscopy (TEM), Cs-corrected STEM-HAADF and energy dispersive X-ray mapping (EDX) experiments were performed using a FEI Titan Themis 60-300 kV microscope equipped with a

Super-X detector and operating at 300 kV. Followed strain analysis of the STEM HAADF images was performed by using the commercial Geometric Phase Analysis package by HREM Research.

### 3. Measurement

The Seebeck coefficient  $S$  and electrical conductivity  $\sigma$  of the materials were measured under a micro-helium atmosphere using a commercial instrument (ADVANCE RIKO ZEM-3, Japan). The experimental error for each measurement was expected to be within 5%. Thermal conductivity is calculated using the formula  $\kappa_{\text{tot}} = D\rho C_p$ , where  $D$ ,  $\rho$ , and  $C_p$  are the thermal diffusion coefficient, mass density, and specific heat capacity, respectively. The thermal diffusion coefficient ( $D$ ) was measured using a thermal expansion instrument (NETZSCH, LFA467, Germany). The sample density  $\rho$  was measured using the Archimedes drainage method. The specific heat capacity ( $C_p$ ) of the sample is calculated using the Dulong-Petit law<sup>1</sup>, that is  $C_p = \frac{3RN}{M}$ , where  $N$  is the number of atoms in the compound;  $R$  is the gas constant;  $M$  is the relative molecular mass of the compound. The room temperature carrier concentration and carrier mobility of the material were measured using the Lake Shore 8400 Hall effect measurement system.

### 4. Two-Kane band model (TBK) simulations

In our calculations of Pisarenko curves for SnTe, two non-parabolic Kane valence bands were used in the framework of acoustic phonon scattering dominating:<sup>2</sup>

$$E \left( 1 + \frac{E}{E_g} \right) = \frac{\hbar^2 k^2}{2m_{d1}^*} \text{ or } \frac{\hbar^2 k_l^2}{2m_l^*} + \frac{\hbar^2 k_t^2}{2m_t^*}, \quad (1)$$

where  $E_g$  is the band gap,  $k$  and  $m^*$  are the wave factors and effective masses along the longitudinal ( $l$ ) and transversal ( $t$ ) directions at corresponding energy extrema, and  $m_{d1}^* = (m_l^* m_t^{*2})^{1/3}$  is the effective mass in each single valley. For each single parabolic Kane band, the carrier concentration  $n(\varepsilon_F)$  is given by:<sup>2, 3</sup>

$$n(\varepsilon_F) = \frac{(2m_d^* k_B T)^{3/2}}{3\pi^2 \hbar^3} \int_0^\infty (\varepsilon + \alpha \varepsilon^2)^{3/2} \left( -\frac{\partial f_0}{\partial \varepsilon} \right) d\varepsilon, \quad (2)$$

MERGEFORMAT (2)

where  $\varepsilon = E / k_B T$ ,  $\varepsilon_F = E_F / k_B T$  are reduced charge carrier energy and Fermi energy,  $f_0$  is the Fermi-Dirac distribution function, the value of  $\alpha = k_B T / E_g$  represents the band's non-parabolic feature,  $m_d^* = N_v^{2/3} m_{d1}^*$  is the density-of-states mass in each band, where  $N_v$  is the degeneracy of the band and  $m_{d1}^* = (m_l m_t^2)^{1/3}$  the effective mass of each single valley with  $m_l$  and  $m_t$  as effective masses along the longitudinal and transversal directions respectively.

For light L band,

$$m_l = 0.176 \cdot (T / 300)^{1/2} \cdot m_0,$$

$$m_t = 0.0405 \cdot (T / 300)^{1/2} \cdot m_0,$$

For heavy  $\Sigma$  band,

$$m_l = m_t = 0.366 \cdot (T / 300)^{1/2} \cdot m_0,$$

where  $m_0$  is the mass for an electron unit. The temperature-dependent relation ( $\sim T^{1/2}$ ) was adopted following literatures.<sup>4-6</sup>

Correspondingly, in the frame of energy dependent relaxation time approximation,<sup>2</sup> the electrical conductivity  $\sigma$ , Seebeck coefficient  $S$  can be expressed as:

$$\sigma = \frac{e^2}{m_l^*} \frac{(2m_d^* k_B T)^{3/2}}{3\pi^2 \hbar^3} \langle \tau(\varepsilon) \rangle, \quad \text{\* MERGEFORMAT (3)}$$

$$S = \frac{k_B}{e} \frac{\langle \tau(\varepsilon)(\varepsilon - \varepsilon_F) \rangle}{\langle \tau(\varepsilon) \rangle}, \quad \text{\* MERGEFORMAT (4)}$$

where  $m_l = 3(1/m_l^* + 2/m_t^*)^{-1}$  is known as the inertial or conducting effective mass,

$\langle x(\varepsilon) \rangle$  is an average of an arbitrary function over energy  $\varepsilon$  and defined as:

$$\langle x(\varepsilon) \rangle = \int_0^{\infty} (\varepsilon + \alpha \varepsilon^2)^{3/2} (1 + 2\alpha \varepsilon)^{-1} \left( -\frac{\partial f_0}{\partial \varepsilon} \right) x(\varepsilon) d\varepsilon, \text{\*}$$

MERGEFORMAT (5)

In the case that acoustic phonons dominates, the corresponding relaxation time is expressed as:<sup>2</sup>

$$\tau_{ac}(\varepsilon) = (\varepsilon + \alpha\varepsilon^2)^r (1 + 2\alpha\varepsilon)^{-1} \frac{2\pi\hbar^4 C_l}{E_{ac}^2 (2m_{d1}^* k_B T)^{3/2} [(1-A)^2 - B]}, \quad \backslash^*$$

MERGEFORMAT (6)

where  $\varepsilon = E / k_B T$  is the reduced energy,  $r = -1/2$  for acoustic scattering,  $\alpha = k_B T / E_g$  represents the band's non-parabolic feature,  $C_l$  is the combined elastic modulus ( $C_l = 58.2$  GPa for SnTe<sup>6</sup>),  $E_{ac}$  is the deformation potential of acoustic phonons of each single band ( $E_{ac\_L} = 15$  eV and  $E_{ac\_S} = 18$  eV), and  $A = \alpha\varepsilon(1-K) / (1+2\alpha\varepsilon)$ ,  $B = 8\alpha\varepsilon(1+\alpha\varepsilon)K / [3(1+2\alpha\varepsilon)^2]$ ,  $K = (E_{ac})_v / (E_{ac})_c$  the ratio of deformation potential between valence and conduction band ( $K=1.0$  is used here).

In the TKB model, the overall Seebeck coefficient, electrical conductivity and Lorenz number are evaluated as follows:

$$S = (S_L \sigma_L + S_S \sigma_S) / (\sigma_L + \sigma_S), \quad \backslash^* \text{MERGEFORMAT (7)}$$

$$\sigma = \sigma_L + \sigma_S, \quad \backslash^* \text{MERGEFORMAT (8)}$$

## 5. Details of the configurational entropy:

$$\Delta S = -R \sum_{i=1}^n x_i \ln x_i \quad \backslash^* \text{MERGEFORMAT (9)}$$

where  $k_B$  and  $N_A$  are the Boltzmann constant and Avogadro's number, respectively,  $R$  is the gas constant,  $n$  is the number of substituted components, and  $x_i$  is the mole content of the component.<sup>7</sup>

## 6. Details of the weighted mobility $\mu_w$ and Quality factor $B$ :

The temperature-dependent weighted mobility ( $\mu_w$ ) was derived from the experimental electrical conductivity  $\sigma$  and Seebeck coefficient  $S$  proposed by G. J. Snyder et al.<sup>8</sup>

$$\mu_w = 331 \left(\frac{1}{\rho}\right) \left(\frac{T}{300}\right)^{-\frac{3}{2}} \left[ \frac{\exp\left[\frac{|S|}{k_B/e} - 2\right]}{1 + \exp\left[-5\left(\frac{|S|}{k_B/e} - 1\right)\right]} + \frac{\frac{3}{\pi^2} \frac{|S|}{k_B/e}}{1 + \exp\left[5\left(\frac{|S|}{k_B/e} - 1\right)\right]} \right] \backslash^*$$

MERGEFORMAT (10)

where  $\mu_w$  is the weighted mobility,  $\rho$  is the electrical resistivity measured in  $m\Omega\text{ cm}$ ,  $T$  is the absolute temperature in K,  $S$  is the Seebeck coefficient, and  $k_B/e = 86.3\ \mu\text{V K}^{-1}$ .

The formula for calculating the quality factor ( $B$ ) is as follows:<sup>9, 10</sup>

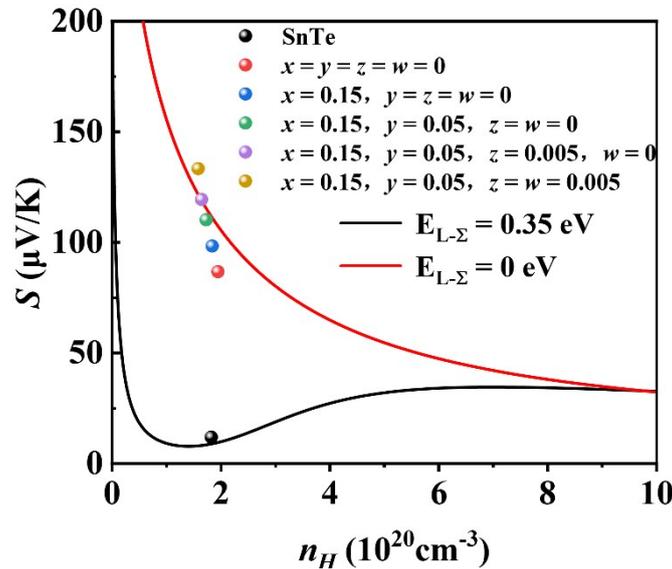
$$B = 9 \frac{\mu_w}{\kappa_{\text{lat}}} \left( \frac{T}{300} \right)^{5/2} \quad \backslash * \text{MERGEFORMAT (11)}$$

## 7. Supplemental Tables

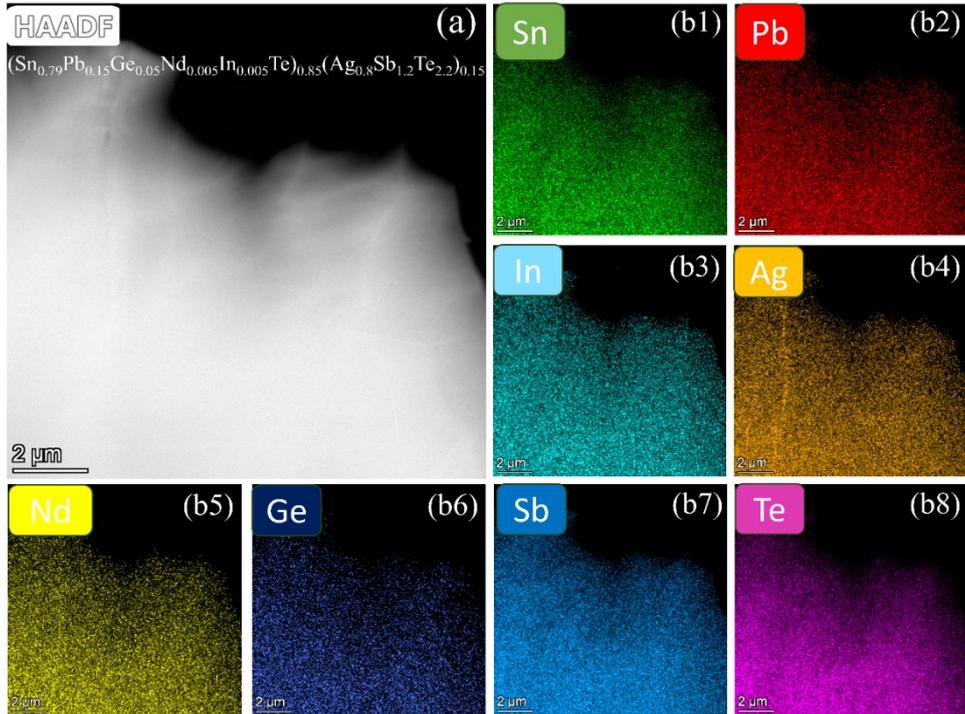
**Table. S1** The configurational entropy,  $\Delta S$ , and the room temperature carrier mobility,  $\mu$ , carrier concentrations,  $n$ , weighted mobility,  $\mu_w$ , lattice thermal conductivity,  $\kappa_l$ , quality factor,  $B$ , of this work involves multi-element co-doping materials.

Samples	$\Delta S$	$\mu$	$n$	$\mu_w$	$\kappa_l$	$B$
$(\text{SnTe})_{0.85}(\text{Ag}_{0.8}\text{Sb}_{1.2}\text{Te}_{2.2})_{0.15}$	0.75	57.65	1.95	92.3	0.89	0.94
$(\text{Sn}_{0.85}\text{Pb}_{0.15}\text{Te})_{0.85}$ $-(\text{Ag}_{0.8}\text{Sb}_{1.2}\text{Te}_{2.2})_{0.15}$	1.06	43.48	1.84	77.58	0.83	0.86
$(\text{Sn}_{0.8}\text{Pb}_{0.15}\text{Ge}_{0.05}\text{Te})_{0.85}$ $-(\text{Ag}_{0.8}\text{Sb}_{1.2}\text{Te}_{2.2})_{0.15}$	1.20	37.84	1.73	75.34	0.85	0.81
$(\text{Sn}_{0.795}\text{Pb}_{0.15}\text{Ge}_{0.05}\text{Nd}_{0.005}\text{Te})_{0.85}$ $-(\text{Ag}_{0.8}\text{Sb}_{1.2}\text{Te}_{2.2})_{0.15}$	1.22	37.72	1.65	78.97	0.88	0.82
$(\text{Sn}_{0.79}\text{Pb}_{0.15}\text{Ge}_{0.05}\text{Nd}_{0.005}\text{In}_{0.005}\text{Te})_{0.85}$ $-(\text{Ag}_{0.8}\text{Sb}_{1.2}\text{Te}_{2.2})_{0.15}$	1.25	32.45	1.59	74.73	0.76	0.9

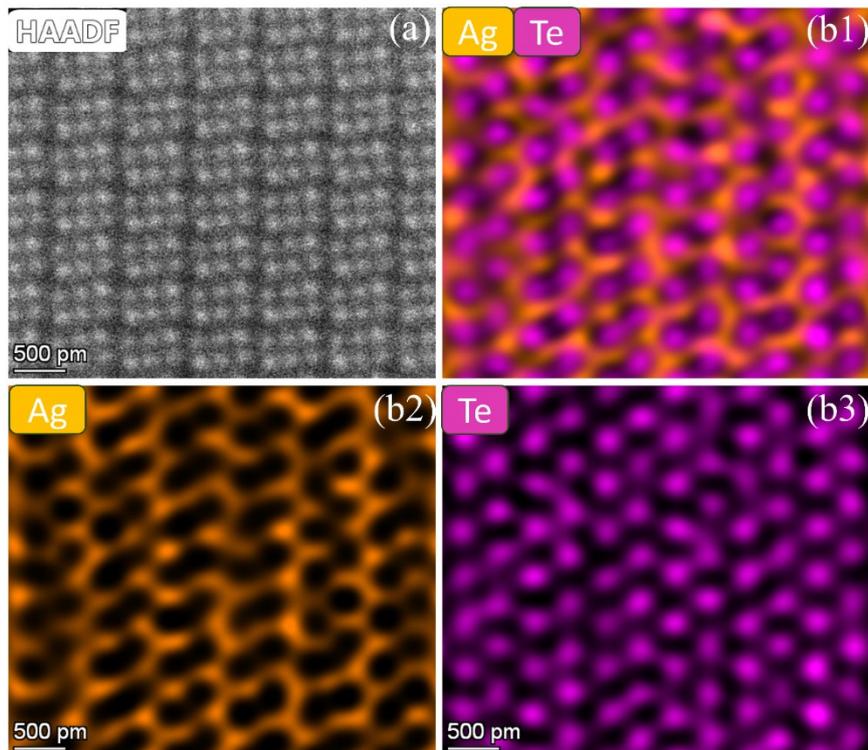
## 8. Supplemental Figures



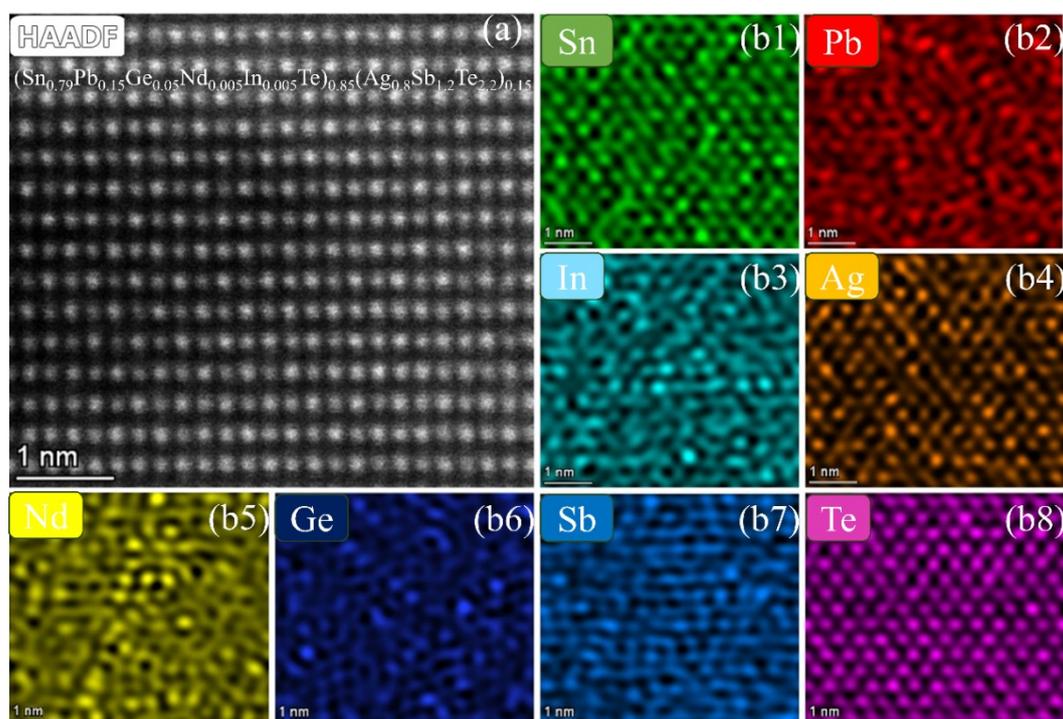
**Figure. S1** Experimental Seebeck coefficient ( $S$ ) as a function of carrier concentration ( $n_H$ ) versus calculated Pisarenko plots via a TBK model with band offsets of 0.35 and 0 eV for  $\text{SnTe}^{11}$  and  $(\text{Sn}_{1-x-y-z-w}\text{Pb}_x\text{Ge}_y\text{Nd}_z\text{In}_w\text{Te})_{0.85}(\text{Ag}_{0.8}\text{Sb}_{1.2}\text{Te}_{2.2})_{0.15}$  ( $x = y = z = w = 0$ ;  $x = 0.15, y = z = w = 0$ ;  $x = 0.15, y = 0.05, z = w = 0$ ;  $x = 0.15, y = 0.05, z = 0.005, w = 0$ ;  $x = 0.15, y = 0.05, z = w = 0.005$ ).



**Figure. S2** (a) A HAADF-STEM image and (b) corresponding energy dispersive X-ray spectroscopy (EDS) elemental mappings for  $(\text{Sn}_{1-x-y-z-w}\text{Pb}_x\text{Ge}_y\text{Nd}_z\text{In}_w\text{Te})_{0.85}(\text{Ag}_{0.8}\text{Sb}_{1.2}\text{Te}_{2.2})_{0.15}$  ( $x = 0.15$ ,  $y = 0.05$ ,  $z = w = 0.005$ ).



**Figure. S3** A atomic-scale HAADF-STEM image and (b) corresponding EDS in the upper left corner of fig 5(b).



**Figure. S4** (a) A atomic-scale HAADF-STEM image and (b1-b8) corresponding EDS elemental mappings for  $(\text{Sn}_{1-x-y-z-w}\text{Pb}_x\text{Ge}_y\text{Nd}_z\text{In}_w\text{Te})_{0.85}(\text{Ag}_{0.8}\text{Sb}_{1.2}\text{Te}_{2.2})_{0.15}$  ( $x = 0.15$ ,  $y = 0.05$ ,  $z = w = 0.005$ ).

#### References

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