

## Supplementary Information

Table 1SI: Crystallographic Data for the Two Complexes [Pd( $\eta^3$ -C<sub>3</sub>H<sub>5</sub>)(IMes)(DIC)](ClO<sub>4</sub>) (left) and [Pd( $\eta^3$ -1,1-Me<sub>2</sub>C<sub>3</sub>H<sub>3</sub>)(IMes)(PPh<sub>3</sub>)] (ClO<sub>4</sub>) (right)

Empirical formula	C <sub>33</sub> H <sub>38</sub> N <sub>3</sub> O <sub>4</sub> ClPd	C <sub>44</sub> H <sub>48</sub> N <sub>2</sub> O <sub>4</sub> PClPd
Formula weight	682.51	841.66
Wavelength (Å) / Temperature (K)	0.71073 / 150.0	0.71073 / 150.0
Crystal system	monoclinic	monoclinic
Crystal size	0.50 × 0.22 × 0.11	0.30 × 0.08 × 0.08
Space group	<i>P</i> 2 <sub>1</sub> / <i>c</i> (No. 14)	<i>P</i> 2 <sub>1</sub> / <i>n</i> (No. 14)
<i>a</i> (Å)	12.8436(1)	10.5270(2)
<i>b</i> (Å)	13.2013(1)	19.8437(4)
<i>c</i> (Å)	19.8990(2)	19.0977(4)
$\beta$ (deg)	107.063(1)	89.893(2)
Volume (Å <sup>3</sup> )	3225.4(1)	3989.4(1)
<i>Z</i> (molecules/unit cell)	4	4
Calculated density (Mg m <sup>-3</sup> )	1.406	1.401
Absorption coefficient, $\mu$ (cm <sup>-1</sup> )	6.98	6.17
<i>F</i> (000)	1408	1744
Total reflections	48218	52550
Independent (unique) reflections / <i>R</i> <sub>int</sub>	7959 / 0.027	8271 / 0.080
Observed reflections [ <i>I</i> > 2 $\sigma$ ( <i>I</i> )]	6699	4843
Data / parameters / restraints	7959 / 395 / 0	8271 / 475 / 0
Goodness-of-fit <sup>a</sup> on <i>F</i> <sup>2</sup>	1.080	0.802
Final <i>R</i> indices [ <i>I</i> > 2 $\sigma$ ( <i>I</i> )]	<i>R</i> <sub>1</sub> <sup>b</sup> = 0.0264; <i>wR</i> <sub>2</sub> <sup>c</sup> = 0.0750	<i>R</i> <sub>1</sub> <sup>b</sup> = 0.0338; <i>wR</i> <sub>2</sub> <sup>c</sup> = 0.0586
Largest difference peak and hole (eÅ <sup>-3</sup> )	0.442 and -0.592	0.364 and -0.430

<sup>a</sup> Goodness-of-fit =  $[\sum (w (F_o^2 - F_c^2)^2) / (N_{\text{obs}} - N_{\text{params}})]^{1/2}$ , based on all data;

<sup>b</sup>  $R_1 = \sum (|F_o| - |F_c|) / \sum |F_o|$ ;

<sup>c</sup>  $wR_2 = [\sum [w (F_o^2 - F_c^2)^2] / \sum [w (F_o^2)^2]]^{1/2}$ .

data\_exp\_63

\_audit\_creation\_method SHELXL-97

\_chemical\_name\_systematic

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?

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\_chemical\_name\_common ?  
\_chemical\_melting\_point ?  
\_chemical\_formula\_moiety ?  
\_chemical\_formula\_sum  
'C44 H48 Cl N2 O4 P Pd'  
\_chemical\_formula\_weight 841.66

loop\_

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\_atom\_type\_scatter\_source  
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'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'  
'H' 'H' 0.0000 0.0000  
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'  
'N' 'N' 0.0061 0.0033  
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'  
'O' 'O' 0.0106 0.0060  
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'  
'P' 'P' 0.1023 0.0942  
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'  
'Cl' 'Cl' 0.1484 0.1585  
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'  
'Pd' 'Pd' -0.9988 1.0072  
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'

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\_symmetry\_space\_group\_name\_H-M 'P 1 21/n 1 (No.14)'

loop\_

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'-x, -y, -z'  
'x-1/2, -y-1/2, z-1/2'

\_cell\_length\_a 10.5270(2)  
\_cell\_length\_b 19.8437(4)  
\_cell\_length\_c 19.0977(4)  
\_cell\_angle\_alpha 90.0  
\_cell\_angle\_beta 89.893(2)  
\_cell\_angle\_gamma 90.0  
\_cell\_volume 3989.4(1)  
\_cell\_formula\_units\_Z 4  
\_cell\_measurement\_temperature 150.0(1)  
\_cell\_measurement\_reflns\_used 11402  
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_exptl_crystal_F_000         1744
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_exptl_absorpt_process_details
;
CrysAlisPro, Oxford Diffraction Ltd.,
Version 1.171.33.52 (release 06-11-2009 CrysAlis171 .NET)
(compiled Nov 6 2009,16:24:50)
Empirical absorption correction using spherical harmonics,
implemented in SCALE3 ABSPACK scaling algorithm.
;

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;
?
;

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_diffn_radiation_source        'Enhance (Mo) X-ray Source'
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_diffn_measurement_device_type 'Xcalibur, Eos, Gemini'
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omega_theta_kappa_phi_frames
- 17.4679 -38.0000 0.0000 47

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2 omega -33.00 -3.00 1.0000 37.8300
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- 17.4679 -92.0000 -18.0000 30

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3 omega 18.00 53.00 1.0000 37.8300
omega_theta_kappa_phi_frames
- 17.4679 -92.0000 -18.0000 35

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4 omega -33.00 -1.00 1.0000 37.8300  
omega\_\_\_\_\_theta\_\_\_\_\_kappa\_\_\_\_\_phi\_\_\_\_\_ frames  
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6 omega -55.00 -23.00 1.0000 37.8300  
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omega\_\_\_\_\_theta\_\_\_\_\_kappa\_\_\_\_\_phi\_\_\_\_\_ frames  
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omega\_\_\_\_\_theta\_\_\_\_\_kappa\_\_\_\_\_phi\_\_\_\_\_ frames  
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9 omega -55.00 51.00 1.0000 37.8300  
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10 omega -55.00 6.00 1.0000 37.8300  
omega\_\_\_\_\_theta\_\_\_\_\_kappa\_\_\_\_\_phi\_\_\_\_\_ frames  
- 17.4679 -77.0000 30.0000 61

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11 omega 26.00 51.00 1.0000 37.8300  
omega\_\_\_\_\_theta\_\_\_\_\_kappa\_\_\_\_\_phi\_\_\_\_\_ frames  
- 17.4679 -77.0000 30.0000 25

#\_ type\_ start\_ end\_ width\_ exp.time\_  
12 omega -52.00 43.00 1.0000 37.8300  
omega\_\_\_\_\_theta\_\_\_\_\_kappa\_\_\_\_\_phi\_\_\_\_\_ frames  
- 17.4679 -38.0000 -150.0000 95

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13 omega -16.00 89.00 1.0000 37.8300  
omega\_\_\_\_\_theta\_\_\_\_\_kappa\_\_\_\_\_phi\_\_\_\_\_ frames  
- 17.4679 77.0000 0.0000 105

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\_computing\_data\_collection

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CrysAlisPro, Oxford Diffraction Ltd.,  
Version 1.171.33.52 (release 06-11-2009 CrysAlis171 .NET)  
(compiled Nov 6 2009,16:24:50)

\_computing\_cell\_refinement

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CrysAlisPro, Oxford Diffraction Ltd.,  
Version 1.171.33.52 (release 06-11-2009 CrysAlis171 .NET)  
(compiled Nov 6 2009,16:24:50)

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CrysAlisPro, Oxford Diffraction Ltd.,  
Version 1.171.33.52 (release 06-11-2009 CrysAlis171 .NET)  
(compiled Nov 6 2009,16:24:50)

\_computing\_structure\_solution 'SHELXTL NT vers.5.10 (Sheldrick, 1999)'  
\_computing\_structure\_refinement 'SHELXL-97 (Sheldrick, 1997)'  
\_computing\_molecular\_graphics 'SHELXTL NT vers.5.10 (Sheldrick, 1999)'  
\_computing\_publication\_material 'SHELXTL NT vers.5.10 (Sheldrick, 1999)'

\_refine\_special\_details

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Refinement of  $F^2$  against ALL reflections. The weighted R-factor  $wR$  and goodness of fit  $S$  are based on  $F^2$ , conventional R-factors  $R$  are based on  $F$ , with  $F$  set to zero for negative  $F^2$ . The threshold expression of  $F^2 > 2\sigma(F^2)$  is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on  $F^2$  are statistically about twice as large as those based on  $F$ , and R-factors based on ALL data will be even larger.

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\_refine\_ls\_structure\_factor\_coef Fsqd

\_refine\_ls\_matrix\_type full

\_refine\_ls\_weighting\_scheme calc

\_refine\_ls\_weighting\_details

'calc w=1/[\sigma^2(Fo^2)+(0.0244P)^2+0.0000P] where P=(Fo^2+2Fc^2)/3'

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\_atom\_sites\_solution\_secondary difmap

\_atom\_sites\_solution\_hydrogens geom

\_refine\_ls\_hydrogen\_treatment 'riding model'

\_refine\_ls\_extinction\_method none

\_refine\_ls\_extinction\_coef ?

\_refine\_ls\_number\_reflns 8271

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loop\_

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\_atom\_site\_type\_symbol

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\_atom\_site\_fract\_y

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\_atom\_site\_disorder\_group

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Cl Cl 0.84154(7) 0.05757(4) 0.77939(4) 0.02940(19) Uani 1 1 d . . .

P P 0.36090(7) 0.31674(4) 0.89370(4) 0.01993(18) Uani 1 1 d . B .  
O1 O 0.87083(19) 0.12657(10) 0.76292(11) 0.0356(5) Uani 1 1 d . . . .  
O2 O 0.82936(19) 0.05023(11) 0.85385(11) 0.0419(6) Uani 1 1 d . . . .  
O3 O 0.9428(2) 0.01541(11) 0.75484(12) 0.0480(6) Uani 1 1 d . . . .  
O4 O 0.7250(2) 0.03922(12) 0.74607(12) 0.0525(7) Uani 1 1 d . . . .  
N1 N 0.1299(2) 0.19314(11) 1.02035(11) 0.0204(6) Uani 1 1 d . . . .  
N2 N 0.2477(2) 0.10933(11) 0.99115(12) 0.0215(6) Uani 1 1 d . . . .  
C1 C 0.2096(2) 0.17178(14) 0.96887(14) 0.0199(7) Uani 1 1 d . B .  
C2 C 0.1200(3) 0.14538(15) 1.07319(15) 0.0273(7) Uani 1 1 d . B .  
H2A H 0.0715 0.1489 1.1137 0.033 Uiso 1 1 calc R . .  
C3 C 0.1931(3) 0.09368(15) 1.05487(15) 0.0263(7) Uani 1 1 d . B .  
H3A H 0.2053 0.0542 1.0803 0.032 Uiso 1 1 calc R . .  
C4 C 0.0549(3) 0.25396(14) 1.01999(14) 0.0194(7) Uani 1 1 d . B .  
C5 C -0.0548(3) 0.25582(14) 0.97888(15) 0.0211(7) Uani 1 1 d . . . .  
C6 C -0.1264(3) 0.31488(15) 0.98023(15) 0.0247(7) Uani 1 1 d . B .  
H6A H -0.2000 0.3172 0.9534 0.030 Uiso 1 1 calc R . .  
C7 C -0.0916(3) 0.37030(15) 1.02023(16) 0.0275(8) Uani 1 1 d . . . .  
C8 C 0.0153(3) 0.36426(15) 1.06271(15) 0.0279(8) Uani 1 1 d . B .  
H8A H 0.0380 0.4003 1.0912 0.034 Uiso 1 1 calc R . .  
C9 C 0.0890(3) 0.30676(15) 1.06410(14) 0.0239(7) Uani 1 1 d . . . .  
C10 C -0.0993(3) 0.19630(14) 0.93698(16) 0.0329(8) Uani 1 1 d . B .  
H10A H -0.1761 0.2078 0.9126 0.049 Uiso 1 1 calc R . .  
H10B H -0.1152 0.1590 0.9678 0.049 Uiso 1 1 calc R . .  
H10C H -0.0350 0.1840 0.9038 0.049 Uiso 1 1 calc R . .  
C11 C -0.1690(3) 0.43419(15) 1.01828(17) 0.0386(9) Uani 1 1 d . B .  
H11A H -0.2388 0.4287 0.9864 0.058 Uiso 1 1 calc R . .  
H11B H -0.1165 0.4708 1.0029 0.058 Uiso 1 1 calc R . .  
H11C H -0.2010 0.4437 1.0643 0.058 Uiso 1 1 calc R . .  
C12 C 0.1994(3) 0.30049(15) 1.11383(14) 0.0331(8) Uani 1 1 d . B .  
H12A H 0.2088 0.3416 1.1398 0.050 Uiso 1 1 calc R . .  
H12B H 0.2756 0.2919 1.0878 0.050 Uiso 1 1 calc R . .  
H12C H 0.1843 0.2639 1.1457 0.050 Uiso 1 1 calc R . .  
C13 C 0.3249(3) 0.06242(14) 0.95248(14) 0.0205(7) Uani 1 1 d . B .  
C14 C 0.2668(3) 0.00424(15) 0.92692(15) 0.0243(7) Uani 1 1 d . . . .  
C15 C 0.3412(3) -0.04065(15) 0.89010(15) 0.0271(7) Uani 1 1 d . B .  
H15A H 0.3038 -0.0798 0.8729 0.033 Uiso 1 1 calc R . .  
C16 C 0.4695(3) -0.02991(15) 0.87760(15) 0.0262(8) Uani 1 1 d . . . .  
C17 C 0.5221(3) 0.02866(15) 0.90294(15) 0.0259(7) Uani 1 1 d . B .  
H17A H 0.6072 0.0374 0.8938 0.031 Uiso 1 1 calc R . .  
C18 C 0.4532(3) 0.07516(14) 0.94155(14) 0.0228(7) Uani 1 1 d . . . .  
C19 C 0.1269(3) -0.00994(16) 0.93678(17) 0.0375(9) Uani 1 1 d . B .  
H19A H 0.0892 0.0257 0.9636 0.056 Uiso 1 1 calc R . .  
H19B H 0.1166 -0.0519 0.9612 0.056 Uiso 1 1 calc R . .  
H19C H 0.0862 -0.0127 0.8919 0.056 Uiso 1 1 calc R . .  
C20 C 0.5470(3) -0.08076(16) 0.83672(16) 0.0351(8) Uani 1 1 d . B .  
H20A H 0.6334 -0.0655 0.8336 0.053 Uiso 1 1 calc R . .  
H20B H 0.5122 -0.0855 0.7905 0.053 Uiso 1 1 calc R . .  
H20C H 0.5447 -0.1235 0.8602 0.053 Uiso 1 1 calc R . .  
C21 C 0.5176(3) 0.13662(14) 0.97062(16) 0.0296(8) Uani 1 1 d . B .  
H21A H 0.6054 0.1365 0.9572 0.044 Uiso 1 1 calc R . .  
H21B H 0.5113 0.1364 1.0208 0.044 Uiso 1 1 calc R . .

H21C H 0.4771 0.1763 0.9525 0.044 Uiso 1 1 calc R . .  
C24 C 0.1658(3) 0.13296(15) 0.81821(15) 0.0350(8) Uani 1 1 d . B .  
H24A H 0.1894 0.0880 0.8332 0.042 Uiso 1 1 calc R A 1  
H24B H 0.0760 0.1376 0.8080 0.042 Uiso 1 1 calc R A 1  
C27 C 0.2612(3) 0.38411(14) 0.85842(14) 0.0197(7) Uani 1 1 d . . .  
C28 C 0.1355(3) 0.38474(14) 0.88129(15) 0.0254(7) Uani 1 1 d . B .  
H28A H 0.1078 0.3522 0.9128 0.031 Uiso 1 1 calc R . .  
C29 C 0.0518(3) 0.43308(16) 0.85769(15) 0.0306(8) Uani 1 1 d . . .  
H29A H -0.0316 0.4331 0.8736 0.037 Uiso 1 1 calc R B .  
C30 C 0.0910(3) 0.48139(16) 0.81071(16) 0.0330(8) Uani 1 1 d . B .  
H30A H 0.0342 0.5137 0.7945 0.040 Uiso 1 1 calc R . .  
C31 C 0.2150(3) 0.48138(15) 0.78792(16) 0.0323(8) Uani 1 1 d . . .  
H31A H 0.2417 0.5142 0.7565 0.039 Uiso 1 1 calc R B .  
C32 C 0.3003(3) 0.43328(14) 0.81104(14) 0.0250(7) Uani 1 1 d . B .  
H32A H 0.3836 0.4337 0.7950 0.030 Uiso 1 1 calc R . .  
C33 C 0.4103(3) 0.35005(14) 0.97886(14) 0.0211(7) Uani 1 1 d . . .  
C34 C 0.3596(3) 0.40761(15) 1.00868(16) 0.0309(8) Uani 1 1 d . B .  
H34A H 0.2939 0.4302 0.9861 0.037 Uiso 1 1 calc R . .  
C35 C 0.4055(3) 0.43182(17) 1.07141(17) 0.0396(9) Uani 1 1 d . . .  
H35A H 0.3705 0.4707 1.0906 0.047 Uiso 1 1 calc R B .  
C36 C 0.5022(3) 0.39933(18) 1.10595(17) 0.0382(9) Uani 1 1 d . B .  
H36A H 0.5325 0.4157 1.1484 0.046 Uiso 1 1 calc R . .  
C37 C 0.5538(3) 0.34205(17) 1.07666(16) 0.0353(8) Uani 1 1 d . . .  
H37A H 0.6198 0.3199 1.0994 0.042 Uiso 1 1 calc R B .  
C38 C 0.5083(3) 0.31728(15) 1.01383(15) 0.0295(8) Uani 1 1 d . B .  
H38A H 0.5436 0.2784 0.9948 0.035 Uiso 1 1 calc R . .  
C39 C 0.5149(3) 0.31952(14) 0.84997(14) 0.0212(7) Uani 1 1 d . . .  
C40 C 0.5858(3) 0.37836(15) 0.84471(15) 0.0272(8) Uani 1 1 d . B .  
H40A H 0.5539 0.4183 0.8631 0.033 Uiso 1 1 calc R . .  
C41 C 0.7033(3) 0.37811(18) 0.81243(16) 0.0369(9) Uani 1 1 d . . .  
H41A H 0.7482 0.4181 0.8072 0.044 Uiso 1 1 calc R B .  
C42 C 0.7539(3) 0.31846(19) 0.78799(16) 0.0381(9) Uani 1 1 d . B .  
H42A H 0.8332 0.3185 0.7667 0.046 Uiso 1 1 calc R . .  
C43 C 0.6882(3) 0.25893(18) 0.79479(15) 0.0350(9) Uani 1 1 d . . .  
H43A H 0.7237 0.2186 0.7796 0.042 Uiso 1 1 calc R B .  
C44 C 0.5675(3) 0.25991(15) 0.82479(14) 0.0269(7) Uani 1 1 d . B .  
H44A H 0.5213 0.2201 0.8280 0.032 Uiso 1 1 calc R . .  
C22 C 0.2323(4) 0.2334(2) 0.7519(2) 0.0243(13) Uiso 0.769(5) 1 d P B 1  
C23 C 0.2518(4) 0.1660(2) 0.77099(19) 0.0261(12) Uiso 0.769(5) 1 d P B 1  
H23A H 0.3278 0.1423 0.7547 0.031 Uiso 0.769(5) 1 calc PR B 1  
C25 C 0.1029(4) 0.2635(2) 0.7501(2) 0.0395(13) Uiso 0.769(5) 1 d P B 1  
H25A H 0.0805 0.2742 0.7026 0.059 Uiso 0.769(5) 1 calc PR B 1  
H25B H 0.1020 0.3039 0.7778 0.059 Uiso 0.769(5) 1 calc PR B 1  
H25C H 0.0428 0.2319 0.7687 0.059 Uiso 0.769(5) 1 calc PR B 1  
C26 C 0.3309(4) 0.2673(2) 0.7061(2) 0.0363(13) Uiso 0.769(5) 1 d P B 1  
H26A H 0.3005 0.2690 0.6587 0.054 Uiso 0.769(5) 1 calc PR B 1  
H26B H 0.4086 0.2420 0.7078 0.054 Uiso 0.769(5) 1 calc PR B 1  
H26C H 0.3460 0.3122 0.7228 0.054 Uiso 0.769(5) 1 calc PR B 1  
C22A C 0.2721(13) 0.2172(8) 0.7541(6) 0.013(3) Uiso 0.231(5) 1 d P B 2  
C23A C 0.1597(14) 0.1923(7) 0.7788(7) 0.030(4) Uiso 0.231(5) 1 d P B 2  
H23B H 0.0783 0.2132 0.7666 0.036 Uiso 0.231(5) 1 calc PR B 2



C25A C 0.3752(12) 0.1682(7) 0.7360(7) 0.039(4) Uiso 0.231(5) 1 d P B 2  
H25D H 0.3871 0.1676 0.6862 0.058 Uiso 0.231(5) 1 calc PR B 2  
H25E H 0.3518 0.1240 0.7518 0.058 Uiso 0.231(5) 1 calc PR B 2  
H25F H 0.4529 0.1817 0.7584 0.058 Uiso 0.231(5) 1 calc PR B 2  
C26A C 0.2722(14) 0.2815(7) 0.7108(6) 0.026(3) Uiso 0.231(5) 1 d P B 2  
H26D H 0.2815 0.2703 0.6621 0.039 Uiso 0.231(5) 1 calc PR B 2  
H26E H 0.3416 0.3097 0.7252 0.039 Uiso 0.231(5) 1 calc PR B 2  
H26F H 0.1936 0.3050 0.7176 0.039 Uiso 0.231(5) 1 calc PR B 2

loop\_

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\_atom\_site\_aniso\_U\_12  
Pd 0.02251(12) 0.01500(11) 0.02125(12) 0.00006(12) 0.00147(8) -0.00113(13)  
Cl 0.0289(5) 0.0247(4) 0.0346(5) -0.0007(4) 0.0037(4) -0.0017(4)  
P 0.0231(4) 0.0154(4) 0.0213(4) 0.0010(3) 0.0031(3) -0.0002(3)  
O1 0.0433(14) 0.0185(12) 0.0451(14) 0.0040(10) 0.0016(11) 0.0001(11)  
O2 0.0400(14) 0.0534(16) 0.0322(13) 0.0106(11) 0.0054(11) 0.0003(12)  
O3 0.0460(15) 0.0292(13) 0.0690(17) -0.0101(12) 0.0172(12) 0.0128(12)  
O4 0.0408(16) 0.0582(17) 0.0586(16) -0.0044(13) -0.0163(13) -0.0140(13)  
N1 0.0205(13) 0.0198(14) 0.0209(13) -0.0003(11) 0.0001(11) -0.0002(11)  
N2 0.0188(14) 0.0189(14) 0.0268(14) 0.0039(11) 0.0029(11) 0.0031(11)  
C1 0.0144(16) 0.0168(17) 0.0284(18) 0.0001(14) -0.0019(13) -0.0026(14)  
C2 0.0305(19) 0.0318(19) 0.0195(17) 0.0040(15) 0.0043(14) -0.0030(16)  
C3 0.0264(18) 0.0266(18) 0.0258(18) 0.0095(15) 0.0034(14) 0.0011(15)  
C4 0.0195(17) 0.0183(16) 0.0204(16) 0.0019(13) 0.0071(13) 0.0017(14)  
C5 0.0187(17) 0.0206(17) 0.0240(17) -0.0028(14) 0.0033(13) -0.0028(15)  
C6 0.0179(17) 0.0287(18) 0.0276(18) 0.0003(15) 0.0021(13) 0.0005(15)  
C7 0.0232(18) 0.0267(19) 0.0327(19) -0.0006(15) 0.0102(15) 0.0027(15)  
C8 0.0313(19) 0.0259(18) 0.0266(18) -0.0061(15) 0.0052(15) -0.0022(16)  
C9 0.0209(17) 0.031(2) 0.0197(16) -0.0019(14) 0.0067(13) -0.0048(14)  
C10 0.0261(18) 0.030(2) 0.042(2) -0.0087(15) -0.0059(15) -0.0010(15)  
C11 0.036(2) 0.029(2) 0.051(2) -0.0046(17) 0.0080(17) 0.0048(17)  
C12 0.0379(19) 0.037(2) 0.0248(17) -0.0034(15) 0.0002(15) -0.0073(16)  
C13 0.0201(17) 0.0171(16) 0.0242(17) 0.0056(14) 0.0025(13) 0.0038(14)  
C14 0.0186(17) 0.0204(17) 0.0339(19) 0.0039(14) 0.0017(14) -0.0020(14)  
C15 0.0293(19) 0.0193(17) 0.0328(19) 0.0027(14) -0.0022(15) -0.0015(15)  
C16 0.0255(19) 0.028(2) 0.0252(18) 0.0087(15) 0.0012(14) 0.0085(16)  
C17 0.0179(17) 0.033(2) 0.0264(18) 0.0091(15) 0.0041(14) 0.0044(15)  
C18 0.0228(18) 0.0190(17) 0.0266(18) 0.0100(14) -0.0014(14) -0.0016(14)  
C19 0.0270(19) 0.033(2) 0.053(2) -0.0054(17) 0.0070(16) -0.0116(16)  
C20 0.0304(19) 0.041(2) 0.034(2) -0.0006(16) 0.0045(15) 0.0103(17)  
C21 0.0213(18) 0.0275(19) 0.040(2) 0.0112(16) -0.0017(15) -0.0007(15)  
C24 0.046(2) 0.0237(19) 0.035(2) -0.0001(15) -0.0184(16) -0.0127(17)  
C27 0.0215(17) 0.0174(16) 0.0202(18) -0.0033(13) 0.0007(14) -0.0011(14)  
C28 0.0294(19) 0.0241(18) 0.0228(17) 0.0003(14) 0.0020(14) -0.0005(15)  
C29 0.0217(18) 0.040(2) 0.0304(19) -0.0063(16) -0.0037(15) 0.0035(16)

C30 0.040(2) 0.0261(19) 0.033(2) 0.0019(16) -0.0091(16) 0.0077(17)  
C31 0.044(2) 0.0204(18) 0.033(2) 0.0079(15) -0.0020(16) 0.0004(17)  
C32 0.0233(17) 0.0240(18) 0.0276(18) 0.0023(14) 0.0009(14) -0.0015(15)  
C33 0.0222(17) 0.0198(17) 0.0212(17) 0.0003(14) 0.0051(13) -0.0031(14)  
C34 0.034(2) 0.0280(19) 0.0304(19) -0.0058(16) -0.0017(15) 0.0024(16)  
C35 0.047(2) 0.035(2) 0.037(2) -0.0163(17) 0.0028(18) -0.0008(18)  
C36 0.038(2) 0.050(2) 0.027(2) -0.0105(18) -0.0004(17) -0.0157(19)  
C37 0.0282(19) 0.050(2) 0.0279(19) 0.0014(17) -0.0051(15) -0.0042(18)  
C38 0.0316(19) 0.0244(18) 0.0326(19) -0.0009(15) 0.0017(15) -0.0001(15)  
C39 0.0261(17) 0.0198(17) 0.0176(16) -0.0003(13) 0.0001(13) 0.0008(14)  
C40 0.0230(18) 0.0264(19) 0.0323(19) 0.0041(15) 0.0017(15) -0.0002(15)  
C41 0.0237(19) 0.043(2) 0.044(2) 0.0180(18) -0.0011(16) -0.0051(17)  
C42 0.0243(19) 0.058(3) 0.032(2) 0.0123(19) 0.0080(15) 0.0063(19)  
C43 0.038(2) 0.045(2) 0.0224(18) 0.0020(16) 0.0058(16) 0.0207(19)  
C44 0.0358(19) 0.0251(18) 0.0198(17) 0.0015(14) -0.0015(14) 0.0023(15)

\_geom\_special\_details

;

All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

;

loop\_

\_geom\_bond\_atom\_site\_label\_1

\_geom\_bond\_atom\_site\_label\_2

\_geom\_bond\_distance

\_geom\_bond\_site\_symmetry\_2

\_geom\_bond\_publ\_flag

Pd C1 2.070(3) . ?

Pd C23A 2.093(13) . ?

Pd C24 2.133(3) . ?

Pd C23 2.173(4) . ?

Pd C22A 2.279(12) . ?

Pd C22 2.353(4) . ?

Pd P 2.3578(9) . ?

Cl O4 1.428(2) . ?

Cl O3 1.434(2) . ?

Cl O2 1.435(2) . ?

Cl O1 1.438(2) . ?

P C39 1.826(3) . ?

P C27 1.828(3) . ?

P C33 1.830(3) . ?

N1 C1 1.361(3) . ?

N1 C2 1.388(3) . ?

N1 C4 1.443(3) . ?

N2 C1 1.370(3) . ?

N2 C3 1.382(3) . ?

N2 C13 1.441(3) . ?  
C2 C3 1.330(4) . ?  
C4 C9 1.391(4) . ?  
C4 C5 1.395(4) . ?  
C5 C6 1.394(4) . ?  
C5 C10 1.501(4) . ?  
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C7 C8 1.392(4) . ?  
C7 C11 1.507(4) . ?  
C8 C9 1.380(4) . ?  
C9 C12 1.505(4) . ?  
C13 C18 1.390(4) . ?  
C13 C14 1.395(4) . ?  
C14 C15 1.380(4) . ?  
C14 C19 1.511(4) . ?  
C15 C16 1.389(4) . ?  
C16 C17 1.375(4) . ?  
C16 C20 1.515(4) . ?  
C17 C18 1.386(4) . ?  
C18 C21 1.501(4) . ?  
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C24 C23 1.437(5) . ?  
C27 C32 1.393(4) . ?  
C27 C28 1.395(4) . ?  
C28 C29 1.377(4) . ?  
C29 C30 1.377(4) . ?  
C30 C31 1.377(4) . ?  
C31 C32 1.382(4) . ?  
C33 C34 1.384(4) . ?  
C33 C38 1.390(4) . ?  
C34 C35 1.377(4) . ?  
C35 C36 1.373(4) . ?  
C36 C37 1.379(4) . ?  
C37 C38 1.381(4) . ?  
C39 C40 1.389(4) . ?  
C39 C44 1.392(4) . ?  
C40 C41 1.383(4) . ?  
C41 C42 1.380(4) . ?  
C42 C43 1.375(4) . ?  
C43 C44 1.395(4) . ?  
C22 C23 1.401(6) . ?  
C22 C26 1.515(6) . ?  
C22 C25 1.487(6) . ?  
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C22A C26A 1.52(2) . ?

loop\_

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C1 Pd C24 91.56(11) . . ?  
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C23A Pd C23 30.1(4) . . ?  
C24 Pd C23 38.98(13) . . ?  
C1 Pd C22A 155.6(4) . . ?  
C23A Pd C22A 36.1(5) . . ?  
C24 Pd C22A 64.4(4) . . ?  
C23 Pd C22A 28.1(4) . . ?  
C1 Pd C22 156.19(13) . . ?  
C23A Pd C22 31.5(4) . . ?  
C24 Pd C22 66.43(14) . . ?  
C23 Pd C22 35.80(16) . . ?  
C22A Pd C22 13.0(4) . . ?  
C1 Pd P 108.12(8) . . ?  
C23A Pd P 123.4(4) . . ?  
C24 Pd P 160.32(8) . . ?  
C23 Pd P 122.25(11) . . ?  
C22A Pd P 96.0(4) . . ?  
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O4 Cl O3 110.10(14) . . ?  
O4 Cl O2 109.72(14) . . ?  
O3 Cl O2 109.41(14) . . ?  
O4 Cl O1 109.25(14) . . ?  
O3 Cl O1 108.91(13) . . ?  
O2 Cl O1 109.43(13) . . ?  
C39 P C27 108.59(13) . . ?  
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N2 C1 Pd 125.5(2) . . ?  
C3 C2 N1 106.9(3) . . ?  
C2 C3 N2 107.5(3) . . ?  
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C9 C4 N1 119.1(2) . . ?  
C5 C4 N1 118.5(3) . . ?

C6 C5 C4 117.3(3) . . ?  
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C8 C9 C4 117.8(3) . . ?  
C8 C9 C12 120.9(3) . . ?  
C4 C9 C12 121.2(3) . . ?  
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C18 C13 N2 120.6(3) . . ?  
C14 C13 N2 117.8(2) . . ?  
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C17 C16 C20 121.8(3) . . ?  
C15 C16 C20 120.8(3) . . ?  
C16 C17 C18 122.7(3) . . ?  
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C17 C18 C21 120.1(3) . . ?  
C13 C18 C21 122.0(3) . . ?  
C23A C24 C23 46.1(6) . . ?  
C23A C24 Pd 69.1(5) . . ?  
C23 C24 Pd 71.98(19) . . ?  
C32 C27 C28 118.6(3) . . ?  
C32 C27 P 125.6(2) . . ?  
C28 C27 P 115.8(2) . . ?  
C29 C28 C27 120.7(3) . . ?  
C30 C29 C28 120.4(3) . . ?  
C29 C30 C31 119.4(3) . . ?  
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C41 C40 C39 120.7(3) . . ?  
C42 C41 C40 120.0(3) . . ?  
C43 C42 C41 120.7(3) . . ?  
C42 C43 C44 119.0(3) . . ?

C39 C44 C43 121.1(3) . . ?  
C23 C22 C26 118.3(4) . . ?  
C23 C22 C25 121.5(4) . . ?  
C26 C22 C25 115.9(4) . . ?  
C23 C22 Pd 65.1(2) . . ?  
C26 C22 Pd 125.2(3) . . ?  
C25 C22 Pd 99.7(3) . . ?  
C22 C23 C24 120.5(4) . . ?  
C22 C23 Pd 79.1(2) . . ?  
C24 C23 Pd 69.04(19) . . ?  
C23A C22A C25A 118.3(13) . . ?  
C23A C22A C26A 119.5(14) . . ?  
C25A C22A C26A 114.7(12) . . ?  
C23A C22A Pd 64.5(7) . . ?  
C25A C22A Pd 106.3(9) . . ?  
C26A C22A Pd 124.2(9) . . ?  
C22A C23A C24 116.8(13) . . ?  
C22A C23A Pd 79.4(8) . . ?  
C24 C23A Pd 72.2(6) . . ?

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data\_exp\_50

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loop\_

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'H' 'H' 0.0000 0.0000

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loop\_

\_symmetry\_equiv\_pos\_as\_xyz

'x, y, z'

'-x, y+1/2, -z+1/2'

'-x, -y, -z'

'x, -y-1/2, z-1/2'

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\_cell\_angle\_beta 107.063(1)  
\_cell\_angle\_gamma 90.00  
\_cell\_volume 3225.4(1)  
\_cell\_formula\_units\_Z 4  
\_cell\_measurement\_temperature 150.0(1)  
\_cell\_measurement\_reflns\_used 30639  
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;

CrysAlisPro, Oxford Diffraction Ltd.,  
Version 1.171.33.52 (release 06-11-2009 CrysAlis171 .NET)  
(compiled Nov 6 2009,16:24:50)

Empirical absorption correction using spherical harmonics,  
implemented in SCALE3 ABSPACK scaling algorithm.

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\_exptl\_special\_details

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?

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\_diffn\_ambient\_temperature 150.0(1)

\_diffn\_radiation\_wavelength 0.71073

\_diffn\_radiation\_type 'Mo K\alpha'

\_diffn\_radiation\_source 'Enhance (Mo) X-ray Source'

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\_diffn\_measurement\_device\_type 'Xcalibur, Eos, Gemini'

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1 omega -97.00 -55.00 1.0000 11.4300

omega\_theta\_kappa\_phi\_frames

- -21.3113 157.0000 -27.0000 42

#\_type\_start\_end\_width\_exp.time\_

2 omega 44.00 90.00 1.0000 11.4300

omega\_theta\_kappa\_phi\_frames

- 21.3895 179.0000 30.0000 46

#\_type\_start\_end\_width\_exp.time\_

3 omega -52.00 47.00 1.0000 11.4300

omega\_theta\_kappa\_phi\_frames

- 21.3895 -38.0000 120.0000 99

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4 omega -47.00 15.00 1.0000 11.4300

omega\_theta\_kappa\_phi\_frames

- 21.3895 -77.0000 60.0000 62

#\_type\_start\_end\_width\_exp.time\_

5 omega -5.00 80.00 1.0000 11.4300

omega\_theta\_kappa\_phi\_frames

- 21.3895 66.0000 117.0000 85

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6 omega 2.00 82.00 1.0000 11.4300

omega\_theta\_kappa\_phi\_frames

- 21.3895 77.0000 0.0000 80

#\_type\_start\_end\_width\_exp.time\_

7 omega -43.00 51.00 1.0000 11.4300

omega\_theta\_kappa\_phi\_frames

- 21.3895 -77.0000 -30.0000 94



```
#_type_start_end_width_exp.time_  
8 omega 2.00 93.00 1.0000 11.4300  
omega_theta_kappa_phi_frames  
- 21.3895 77.0000 -90.0000 91
```

```
#_type_start_end_width_exp.time_  
9 omega -47.00 42.00 1.0000 11.4300  
omega_theta_kappa_phi_frames  
- 21.3895 -38.0000 -150.0000 89
```

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#_type_start_end_width_exp.time_  
10 omega -6.00 88.00 1.0000 11.4300  
omega_theta_kappa_phi_frames  
- 21.3895 77.0000 -180.0000 94
```

```
#_type_start_end_width_exp.time_  
11 omega 42.00 85.00 1.0000 11.4300  
omega_theta_kappa_phi_frames  
- 21.3895 -132.0000 -119.0000 43
```

;

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_diffraction_measurement_method '\w scans'  
_diffraction_detector_area_resol_mean 16.1274  
_diffraction_standards_number 2  
_diffraction_standards_interval_count 50  
_diffraction_standards_interval_time ?  
_diffraction_standards_decay_percent 'negligible'  
_diffraction_reflections_number 48218  
_diffraction_reflections_av_R_equivalents 0.0266  
_diffraction_reflections_av_sigma_netI 0.0204  
_diffraction_reflections_limit_h_min -17  
_diffraction_reflections_limit_h_max 17  
_diffraction_reflections_limit_k_min -17  
_diffraction_reflections_limit_k_max 16  
_diffraction_reflections_limit_l_min -26  
_diffraction_reflections_limit_l_max 27  
_diffraction_reflections_theta_min 3.27  
_diffraction_reflections_theta_max 29.01  
_diffraction_orient_matrix_UB_11 -0.0375801528  
_diffraction_orient_matrix_UB_12 -0.0374271123  
_diffraction_orient_matrix_UB_13 -0.0178257397  
_diffraction_orient_matrix_UB_21 0.0318099455  
_diffraction_orient_matrix_UB_22 -0.0379273995  
_diffraction_orient_matrix_UB_23 0.0219019870  
_diffraction_orient_matrix_UB_31 -0.0301793108  
_diffraction_orient_matrix_UB_32 0.0066913581  
_diffraction_orient_matrix_UB_33 0.0243618730  
_reflections_number_total 7959  
_reflections_number_gt 6669  
_reflections_threshold_expression >2sigma(I)
```

```
_computing_data_collection
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CrysAlisPro, Oxford Diffraction Ltd.,
Version 1.171.33.52 (release 06-11-2009 CrysAlis171 .NET)
(compiled Nov 6 2009,16:24:50)
;
_computing_cell_refinement
;
CrysAlisPro, Oxford Diffraction Ltd.,
Version 1.171.33.52 (release 06-11-2009 CrysAlis171 .NET)
(compiled Nov 6 2009,16:24:50)
;
_computing_data_reduction
;
CrysAlisPro, Oxford Diffraction Ltd.,
Version 1.171.33.52 (release 06-11-2009 CrysAlis171 .NET)
(compiled Nov 6 2009,16:24:50)
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_computing_structure_solution 'SHELXTL NT vers.5.10 (Sheldrick, 1999)'
_computing_structure_refinement 'SHELXL-97 (Sheldrick, 1997)'
_computing_molecular_graphics 'SHELXTL NT vers.5.10 (Sheldrick, 1999)'
_computing_publication_material 'SHELXTL NT vers.5.10 (Sheldrick, 1999)'

_refine_special_details
;
Refinement of F2 against ALL reflections. The weighted R-factor wR and
goodness of fit S are based on F2, conventional R-factors R are based
on F, with F set to zero for negative F2. The threshold expression of
F2 > 2sigma(F2) is used only for calculating R-factors(gt) etc. and is
not relevant to the choice of reflections for refinement. R-factors based
on F2 are statistically about twice as large as those based on F, and R-
factors based on ALL data will be even larger.
;

_refine_ls_structure_factor_coef Fsqd
_refine_ls_matrix_type full
_refine_ls_weighting_scheme calc
_refine_ls_weighting_details
'calc w=1/[s2(Fo2)+(0.0457P)2+0.7242P] where P=(Fo2+2Fc2)/3'
_atom_sites_solution_primary 'heavy-atom methods'
_atom_sites_solution_secondary difmap
_atom_sites_solution_hydrogens geom
_refine_ls_hydrogen_treatment mixed
_refine_ls_extinction_method riding model
_refine_ls_extinction_coef ?
_refine_ls_number_reflns 7959
_refine_ls_number_parameters 395
_refine_ls_number_restraints 0
_refine_ls_R_factor_all 0.0337
_refine_ls_R_factor_gt 0.0264
```

\_refine\_ls\_wR\_factor\_ref 0.0769  
\_refine\_ls\_wR\_factor\_gt 0.0750  
\_refine\_ls\_goodness\_of\_fit\_ref 1.080  
\_refine\_ls\_restrained\_S\_all 1.080  
\_refine\_ls\_shift/su\_max 0.002  
\_refine\_ls\_shift/su\_mean 0.000

loop\_

\_atom\_site\_label

\_atom\_site\_type\_symbol

\_atom\_site\_fract\_x

\_atom\_site\_fract\_y

\_atom\_site\_fract\_z

\_atom\_site\_U\_iso\_or\_equiv

\_atom\_site\_adp\_type

\_atom\_site\_occupancy

\_atom\_site\_symmetry\_multiplicity

\_atom\_site\_calc\_flag

\_atom\_site\_refinement\_flags

\_atom\_site\_disorder\_assembly

\_atom\_site\_disorder\_group

Pd Pd 0.210095(10) 0.760826(10) 0.402882(7) 0.02017(5) Uani 1 1 d . . .

N1 N 0.45326(12) 0.71515(11) 0.47314(8) 0.0226(3) Uani 1 1 d . . .

N2 N 0.38940(12) 0.81342(11) 0.53735(7) 0.0222(3) Uani 1 1 d . . .

N3 N 0.10118(13) 0.66293(12) 0.50970(8) 0.0268(3) Uani 1 1 d . . .

C1 C 0.36059(14) 0.76272(12) 0.47554(9) 0.0208(3) Uani 1 1 d . . .

C2 C 0.49867(14) 0.79850(15) 0.57332(10) 0.0268(4) Uani 1 1 d . . .

H2A H 0.5366 0.8258 0.6167 0.032 Uiso 1 1 calc R . .

C3 C 0.53862(15) 0.73713(14) 0.53328(10) 0.0267(4) Uani 1 1 d . . .

H3A H 0.6098 0.7136 0.5436 0.032 Uiso 1 1 calc R . .

C4 C 0.46167(14) 0.65112(13) 0.41620(9) 0.0233(3) Uani 1 1 d . . .

C5 C 0.52799(15) 0.68195(14) 0.37533(10) 0.0267(4) Uani 1 1 d . . .

C6 C 0.53073(16) 0.62114(15) 0.31883(10) 0.0317(4) Uani 1 1 d . . .

H6A H 0.5742 0.6402 0.2909 0.038 Uiso 1 1 calc R . .

C7 C 0.46994(16) 0.53229(16) 0.30301(10) 0.0335(4) Uani 1 1 d . . .

C8 C 0.40806(16) 0.50297(15) 0.34599(11) 0.0331(4) Uani 1 1 d . . .

H8A H 0.3684 0.4430 0.3360 0.040 Uiso 1 1 calc R . .

C9 C 0.40308(14) 0.56031(14) 0.40386(10) 0.0269(4) Uani 1 1 d . . .

C10 C 0.59543(18) 0.77697(16) 0.39111(12) 0.0357(5) Uani 1 1 d . . .

H10A H 0.6345 0.7850 0.3571 0.054 Uiso 1 1 calc R . .

H10B H 0.6462 0.7722 0.4373 0.054 Uiso 1 1 calc R . .

H10C H 0.5486 0.8343 0.3891 0.054 Uiso 1 1 calc R . .

C11 C 0.4713(2) 0.46970(19) 0.23999(12) 0.0467(6) Uani 1 1 d . . .

H11A H 0.5181 0.5011 0.2163 0.070 Uiso 1 1 calc R . .

H11B H 0.3988 0.4651 0.2084 0.070 Uiso 1 1 calc R . .

H11C H 0.4978 0.4030 0.2550 0.070 Uiso 1 1 calc R . .

C12 C 0.33990(17) 0.52292(15) 0.45162(12) 0.0348(4) Uani 1 1 d . . .

H12A H 0.3058 0.4596 0.4343 0.052 Uiso 1 1 calc R . .

H12B H 0.2851 0.5717 0.4529 0.052 Uiso 1 1 calc R . .

H12C H 0.3884 0.5136 0.4981 0.052 Uiso 1 1 calc R . .

C13 C 0.31388(14) 0.86792(13) 0.56542(9) 0.0228(3) Uani 1 1 d . . .

C14 C 0.28281(15) 0.82340(14) 0.62011(9) 0.0266(4) Uani 1 1 d . . .  
C15 C 0.20854(17) 0.87580(17) 0.64581(10) 0.0350(5) Uani 1 1 d . . .  
H15A H 0.1863 0.8475 0.6821 0.042 Uiso 1 1 calc R . .  
C16 C 0.16682(18) 0.96895(16) 0.61888(11) 0.0377(5) Uani 1 1 d . . .  
C17 C 0.20059(17) 1.01003(15) 0.56467(11) 0.0351(4) Uani 1 1 d . . .  
H17A H 0.1727 1.0725 0.5463 0.042 Uiso 1 1 calc R . .  
C18 C 0.27458(15) 0.96147(14) 0.53661(10) 0.0270(4) Uani 1 1 d . . .  
C19 C 0.32728(19) 0.72262(16) 0.65133(11) 0.0363(5) Uani 1 1 d . . .  
H19A H 0.2961 0.7052 0.6881 0.054 Uiso 1 1 calc R . .  
H19B H 0.4050 0.7270 0.6703 0.054 Uiso 1 1 calc R . .  
H19C H 0.3091 0.6715 0.6154 0.054 Uiso 1 1 calc R . .  
C20 C 0.0868(2) 1.0254(2) 0.64804(16) 0.0623(8) Uani 1 1 d . . .  
H20A H 0.0674 1.0883 0.6234 0.093 Uiso 1 1 calc R . .  
H20B H 0.1197 1.0386 0.6971 0.093 Uiso 1 1 calc R . .  
H20C H 0.0226 0.9849 0.6421 0.093 Uiso 1 1 calc R . .  
C21 C 0.30934(19) 1.00895(15) 0.47786(11) 0.0360(5) Uani 1 1 d . . .  
H21A H 0.3604 0.9653 0.4653 0.054 Uiso 1 1 calc R . .  
H21B H 0.3431 1.0732 0.4930 0.054 Uiso 1 1 calc R . .  
H21C H 0.2467 1.0187 0.4378 0.054 Uiso 1 1 calc R . .  
C22 C 0.07799(18) 0.76211(17) 0.30389(11) 0.0337(4) Uani 1 1 d . . .  
H22A H 0.0866(19) 0.694(2) 0.2867(12) 0.042(6) Uiso 1 1 d . . .  
H22B H 0.001(2) 0.7801(19) 0.3002(13) 0.043(7) Uiso 1 1 d . . .  
C23 C 0.15265(16) 0.83762(16) 0.30261(9) 0.0325(4) Uani 1 1 d . . .  
H23A H 0.1305 0.9088 0.3012 0.039 Uiso 1 1 calc R . .  
C24 C 0.26293(17) 0.81357(18) 0.31693(10) 0.0325(4) Uani 1 1 d . . .  
H24A H 0.286(2) 0.7505(19) 0.3050(16) 0.049(8) Uiso 1 1 d . . .  
H24B H 0.3147(19) 0.8684(18) 0.3222(12) 0.041(6) Uiso 1 1 d . . .  
C25 C 0.13570(14) 0.70013(14) 0.46862(10) 0.0260(4) Uani 1 1 d . . .  
C26 C 0.05765(14) 0.61992(14) 0.56013(9) 0.0248(4) Uani 1 1 d . . .  
C27 C 0.09623(15) 0.52565(14) 0.58845(9) 0.0270(4) Uani 1 1 d . . .  
C28 C 0.04900(17) 0.48468(16) 0.63692(10) 0.0330(4) Uani 1 1 d . . .  
H28A H 0.0717 0.4215 0.6565 0.040 Uiso 1 1 calc R . .  
C29 C -0.03067(18) 0.53610(17) 0.65632(10) 0.0368(5) Uani 1 1 d . . .  
H29A H -0.0611 0.5072 0.6888 0.044 Uiso 1 1 calc R . .  
C30 C -0.06624(17) 0.63029(16) 0.62820(11) 0.0351(4) Uani 1 1 d . . .  
H30A H -0.1192 0.6645 0.6427 0.042 Uiso 1 1 calc R . .  
C31 C -0.02338(16) 0.67400(15) 0.57853(10) 0.0292(4) Uani 1 1 d . . .  
C32 C 0.18524(17) 0.47087(16) 0.56868(12) 0.0365(5) Uani 1 1 d . . .  
H32A H 0.1998 0.4076 0.5935 0.055 Uiso 1 1 calc R . .  
H32B H 0.2500 0.5116 0.5809 0.055 Uiso 1 1 calc R . .  
H32C H 0.1629 0.4583 0.5190 0.055 Uiso 1 1 calc R . .  
C33 C -0.06430(19) 0.77344(17) 0.54485(13) 0.0406(5) Uani 1 1 d . . .  
H33A H -0.1196 0.7989 0.5640 0.061 Uiso 1 1 calc R . .  
H33B H -0.0943 0.7643 0.4950 0.061 Uiso 1 1 calc R . .  
H33C H -0.0052 0.8209 0.5540 0.061 Uiso 1 1 calc R . .  
Cl Cl 0.22756(4) 0.33560(4) 0.78973(3) 0.03656(12) Uani 1 1 d . . .  
O1 O 0.20528(15) 0.28997(15) 0.72150(9) 0.0554(4) Uani 1 1 d . . .  
O2 O 0.12898(13) 0.37775(15) 0.79747(9) 0.0498(4) Uani 1 1 d . . .  
O4 O 0.26850(15) 0.26025(15) 0.84275(11) 0.0696(7) Uani 1 1 d . . .  
O3 O 0.30814(13) 0.41321(14) 0.79694(9) 0.0528(4) Uani 1 1 d . . .

loop\_

\_atom\_site\_aniso\_label

\_atom\_site\_aniso\_U\_11

\_atom\_site\_aniso\_U\_22

\_atom\_site\_aniso\_U\_33

\_atom\_site\_aniso\_U\_23

\_atom\_site\_aniso\_U\_13

\_atom\_site\_aniso\_U\_12

Pd 0.02015(8) 0.02163(8) 0.01777(8) 0.00108(5) 0.00409(5) 0.00142(5)

N1 0.0224(7) 0.0235(7) 0.0210(7) -0.0012(6) 0.0048(6) 0.0031(6)

N2 0.0226(7) 0.0232(7) 0.0194(7) -0.0010(6) 0.0041(6) 0.0026(6)

N3 0.0273(8) 0.0280(8) 0.0246(8) 0.0029(6) 0.0069(6) -0.0001(6)

C1 0.0220(8) 0.0201(8) 0.0199(8) 0.0021(6) 0.0053(7) 0.0021(6)

C2 0.0242(9) 0.0292(9) 0.0229(9) -0.0021(7) 0.0004(7) 0.0015(7)

C3 0.0208(8) 0.0303(10) 0.0251(9) -0.0002(7) 0.0007(7) 0.0032(7)

C4 0.0227(8) 0.0230(9) 0.0220(8) -0.0007(7) 0.0034(7) 0.0049(7)

C5 0.0259(9) 0.0271(9) 0.0261(9) 0.0019(7) 0.0062(7) 0.0050(7)

C6 0.0317(10) 0.0384(11) 0.0263(9) -0.0004(8) 0.0104(8) 0.0065(8)

C7 0.0322(10) 0.0361(11) 0.0291(10) -0.0064(8) 0.0039(8) 0.0109(8)

C8 0.0309(10) 0.0258(10) 0.0385(11) -0.0083(8) 0.0036(8) 0.0018(8)

C9 0.0226(9) 0.0250(9) 0.0313(10) -0.0010(7) 0.0049(7) 0.0054(7)

C10 0.0385(11) 0.0348(11) 0.0359(11) 0.0008(9) 0.0143(9) -0.0060(9)

C11 0.0520(14) 0.0475(13) 0.0384(12) -0.0147(10) 0.0097(10) 0.0095(11)

C12 0.0330(10) 0.0240(10) 0.0497(13) 0.0008(9) 0.0159(9) 0.0013(8)

C13 0.0245(8) 0.0234(8) 0.0194(8) -0.0028(7) 0.0047(7) 0.0023(7)

C14 0.0325(10) 0.0271(9) 0.0199(8) -0.0009(7) 0.0070(7) 0.0018(7)

C15 0.0431(12) 0.0390(11) 0.0281(10) 0.0000(8) 0.0185(9) 0.0021(9)

C16 0.0428(12) 0.0361(11) 0.0389(11) -0.0049(9) 0.0193(10) 0.0075(9)

C17 0.0430(11) 0.0260(10) 0.0376(11) 0.0014(8) 0.0140(9) 0.0101(8)

C18 0.0317(10) 0.0235(9) 0.0253(9) -0.0010(7) 0.0076(7) 0.0016(7)

C19 0.0495(13) 0.0316(11) 0.0282(10) 0.0060(8) 0.0122(9) 0.0060(9)

C20 0.0714(19) 0.0588(17) 0.0719(19) -0.0024(14) 0.0446(16) 0.0199(14)

C21 0.0511(13) 0.0248(10) 0.0359(11) 0.0051(8) 0.0187(10) 0.0038(9)

C22 0.0274(10) 0.0434(12) 0.0242(10) 0.0005(8) -0.0021(8) 0.0016(8)

C23 0.0381(11) 0.0371(11) 0.0185(9) 0.0069(8) 0.0025(8) 0.0028(8)

C24 0.0359(11) 0.0409(12) 0.0214(9) 0.0044(8) 0.0094(8) -0.0012(9)

C25 0.0235(8) 0.0256(9) 0.0267(9) 0.0024(7) 0.0040(7) 0.0028(7)

C26 0.0251(9) 0.0285(9) 0.0206(8) 0.0034(7) 0.0063(7) -0.0024(7)

C27 0.0273(9) 0.0287(9) 0.0228(9) 0.0000(7) 0.0041(7) -0.0001(7)

C28 0.0424(11) 0.0300(10) 0.0238(9) 0.0047(8) 0.0053(8) -0.0034(8)

C29 0.0433(12) 0.0445(12) 0.0253(10) 0.0012(9) 0.0143(9) -0.0087(9)

C30 0.0344(10) 0.0420(12) 0.0321(10) -0.0060(9) 0.0150(9) -0.0021(9)

C31 0.0283(9) 0.0302(10) 0.0280(9) -0.0002(8) 0.0066(8) 0.0011(7)

C32 0.0352(11) 0.0320(11) 0.0424(12) 0.0025(9) 0.0113(9) 0.0055(8)

C33 0.0375(12) 0.0368(12) 0.0469(13) 0.0061(10) 0.0113(10) 0.0108(9)

Cl 0.0259(2) 0.0456(3) 0.0338(3) 0.0113(2) 0.00171(19) -0.00385(19)

O1 0.0515(10) 0.0581(11) 0.0516(11) -0.0102(9) 0.0073(8) 0.0087(9)

O2 0.0359(8) 0.0737(12) 0.0406(9) 0.0029(8) 0.0123(7) 0.0023(8)

O4 0.0336(9) 0.0838(15) 0.0735(15) 0.0513(11) -0.0121(9) -0.0139(9)

O3 0.0457(9) 0.0547(10) 0.0570(11) 0.0102(9) 0.0136(8) -0.0172(8)

\_geom\_special\_details

;

All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

;

loop\_

\_geom\_bond\_atom\_site\_label\_1

\_geom\_bond\_atom\_site\_label\_2

\_geom\_bond\_distance

\_geom\_bond\_site\_symmetry\_2

\_geom\_bond\_publ\_flag

Pd C25 1.9999(19) . ?

Pd C1 2.0463(19) . ?

Pd C24 2.133(2) . ?

Pd C23 2.1655(19) . ?

Pd C22 2.190(2) . ?

N1 C1 1.359(2) . ?

N1 C3 1.396(2) . ?

N1 C4 1.443(2) . ?

N2 C1 1.353(2) . ?

N2 C2 1.390(2) . ?

N2 C13 1.445(2) . ?

N3 C25 1.148(2) . ?

N3 C26 1.404(2) . ?

C2 C3 1.340(3) . ?

C4 C9 1.398(3) . ?

C4 C5 1.400(3) . ?

C5 C6 1.390(3) . ?

C5 C10 1.504(3) . ?

C6 C7 1.393(3) . ?

C7 C8 1.383(3) . ?

C7 C11 1.506(3) . ?

C8 C9 1.395(3) . ?

C9 C12 1.502(3) . ?

C13 C18 1.392(2) . ?

C13 C14 1.394(3) . ?

C14 C15 1.392(3) . ?

C14 C19 1.508(3) . ?

C15 C16 1.385(3) . ?

C16 C17 1.386(3) . ?

C16 C20 1.516(3) . ?

C17 C18 1.392(3) . ?

C18 C21 1.505(3) . ?

C22 C23 1.389(3) . ?

C23 C24 1.397(3) . ?

C26 C27 1.396(3) . ?

C26 C31 1.397(3) . ?  
C27 C28 1.391(3) . ?  
C27 C32 1.500(3) . ?  
C28 C29 1.374(3) . ?  
C29 C30 1.385(3) . ?  
C30 C31 1.390(3) . ?  
C31 C33 1.497(3) . ?  
C1 O2 1.4320(17) . ?  
C1 O4 1.4329(17) . ?  
C1 O3 1.4333(16) . ?  
C1 O1 1.4354(18) . ?

loop\_

\_geom\_angle\_atom\_site\_label\_1  
\_geom\_angle\_atom\_site\_label\_2  
\_geom\_angle\_atom\_site\_label\_3  
\_geom\_angle  
\_geom\_angle\_site\_symmetry\_1  
\_geom\_angle\_site\_symmetry\_3  
\_geom\_angle\_publ\_flag  
C25 Pd C1 94.37(7) . . ?  
C25 Pd C24 168.67(8) . . ?  
C1 Pd C24 96.07(8) . . ?  
C25 Pd C23 133.73(8) . . ?  
C1 Pd C23 129.88(8) . . ?  
C24 Pd C23 37.92(8) . . ?  
C25 Pd C22 101.46(8) . . ?  
C1 Pd C22 163.17(8) . . ?  
C24 Pd C22 67.74(8) . . ?  
C23 Pd C22 37.17(8) . . ?  
C1 N1 C3 110.45(15) . . ?  
C1 N1 C4 124.51(15) . . ?  
C3 N1 C4 125.04(15) . . ?  
C1 N2 C2 111.32(15) . . ?  
C1 N2 C13 124.20(15) . . ?  
C2 N2 C13 124.22(14) . . ?  
C25 N3 C26 178.46(19) . . ?  
N2 C1 N1 104.59(15) . . ?  
N2 C1 Pd 126.73(13) . . ?  
N1 C1 Pd 128.68(13) . . ?  
C3 C2 N2 106.53(16) . . ?  
C2 C3 N1 107.11(16) . . ?  
C9 C4 C5 122.36(17) . . ?  
C9 C4 N1 118.67(16) . . ?  
C5 C4 N1 118.97(16) . . ?  
C6 C5 C4 117.78(18) . . ?  
C6 C5 C10 120.04(18) . . ?  
C4 C5 C10 122.18(17) . . ?  
C5 C6 C7 121.56(19) . . ?  
C8 C7 C6 118.80(18) . . ?  
C8 C7 C11 120.7(2) . . ?

C6 C7 C11 120.5(2) . . ?  
C7 C8 C9 122.18(19) . . ?  
C8 C9 C4 117.22(18) . . ?  
C8 C9 C12 120.52(18) . . ?  
C4 C9 C12 122.23(17) . . ?  
C18 C13 C14 122.89(16) . . ?  
C18 C13 N2 119.07(15) . . ?  
C14 C13 N2 118.04(16) . . ?  
C15 C14 C13 117.48(17) . . ?  
C15 C14 C19 120.31(17) . . ?  
C13 C14 C19 122.20(17) . . ?  
C16 C15 C14 121.89(18) . . ?  
C15 C16 C17 118.35(18) . . ?  
C15 C16 C20 121.1(2) . . ?  
C17 C16 C20 120.5(2) . . ?  
C16 C17 C18 122.57(19) . . ?  
C17 C18 C13 116.82(17) . . ?  
C17 C18 C21 120.85(17) . . ?  
C13 C18 C21 122.33(16) . . ?  
C23 C22 Pd 70.44(11) . . ?  
C22 C23 C24 119.8(2) . . ?  
C22 C23 Pd 72.39(12) . . ?  
C24 C23 Pd 69.80(11) . . ?  
C23 C24 Pd 72.28(11) . . ?  
N3 C25 Pd 174.45(16) . . ?  
C27 C26 C31 123.61(17) . . ?  
C27 C26 N3 118.72(16) . . ?  
C31 C26 N3 117.67(16) . . ?  
C28 C27 C26 116.83(17) . . ?  
C28 C27 C32 121.04(18) . . ?  
C26 C27 C32 122.12(17) . . ?  
C29 C28 C27 121.00(19) . . ?  
C28 C29 C30 120.97(18) . . ?  
C29 C30 C31 120.50(19) . . ?  
C30 C31 C26 117.08(18) . . ?  
C30 C31 C33 121.47(18) . . ?  
C26 C31 C33 121.43(18) . . ?  
O2 Cl O4 109.61(12) . . ?  
O2 Cl O3 110.29(11) . . ?  
O4 Cl O3 108.92(11) . . ?  
O2 Cl O1 109.12(11) . . ?  
O4 Cl O1 109.47(13) . . ?  
O3 Cl O1 109.40(12) . . ?

\_diffn\_measured\_fraction\_theta\_max 0.927  
\_diffn\_reflns\_theta\_full 29.01  
\_diffn\_measured\_fraction\_theta\_full 0.927  
\_refine\_diff\_density\_max 0.442  
\_refine\_diff\_density\_min -0.592  
\_refine\_diff\_density\_rms 0.065



Table 1 SI Close (< 2.500 Å) Nonbonding Contacts for the Complexes

[Pd( $\eta^3$ -C<sub>3</sub>H<sub>5</sub>)(IMes)(DIC)](ClO<sub>4</sub>) (top) and [Pd( $\eta^3$ -C<sub>3</sub>H<sub>3</sub>Me<sub>2</sub>)(IMes)(PPh<sub>3</sub>)] (ClO<sub>4</sub>) (bottom)

Donor Atom	Acceptor Atom	Parent Atom <sup>a</sup>	Symmetry	D–A Distance (Å)	D–A–P Angle (°) <sup>b</sup>
O(4)	H(30A)	C(30)	$-x, -1/2+y, 3/2-z$	2.384	169.4
O(4)	H(3A)	C(3)	$1-x, -1/2+y, 3/2-z$	2.421	116.4
O(3)	H(2A)	C(2)	$1-x, -1/2+y, 3/2-z$	2.500	155.7
O(1)	H(24B)	C(24)	$1+x, y, z$	2.335	165.0
O(2)	H(3A)	C(3)	$1-x, -y, 2-z$	2.451	163.6
O(1)	H(43A)	C(43)	$x, y, z$	2.417	161.8
O(2)	H(17A)	C(17)	$x, y, z$	2.473	171.5

<sup>a</sup> Parent atom of close contact acceptor.

<sup>b</sup> Donor–acceptor–parent angle.