

Controlled translocation of palladium(II) within a 22 ring atom macrocyclic ligand.

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SUPPLEMENTARY INFORMATION

S2 Crystallographic data for **H₄L**, [PdCl(H₃L)] (**3a**), [Pd(*N*-(3-aminopropyl)caprolactam)(H₂L)] (**5**) and [Pd(OH₂)(H₂L)] (**6**) in CIF format.

Crystallographic data for **H₄L**, [PdCl(H₃L)] (**3a**), [Pd(*N*-(3-aminopropyl)caprolactam)(H₂L)] (**5**) and [Pd(OH₂)(H₂L)] (**6**) in CIF format.

1. Compound **H₄L**.

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_audit_creation_method SHELXL-97

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_publ_section_abstract ' Abstract '

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_publ_requested_journal 'Journal'

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Please consider this CIF for publication. I certify that this contribution is the original work of those listed as authors; that it has not been published before (in any language or medium) and is not being considered for publication elsewhere; that all authors concur with and are aware of the submission; that all workers involved in the study are listed as authors or given proper credit in the acknowledgements; that I have obtained permission for and acknowledged the source of any excerpts from other copyright works; and that to the best of my knowledge the paper contains no statements which are libellous, unlawful or in any way actionable. All coauthors have made significant scientific contributions to the work reported, including the ideas and their execution, and share responsibility and accountability for the results.

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_publ_section_exptl_refinement
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The X-ray data was "squeezed" by the method of Sluis and Spek (1990) to allow for the presence of disordered solvent of crystallization which could not be satisfactorily modelled. The SQUEEZE results showed that the total potential accessible void volume was 1553.4 Å³ (24.4% of the crystal unit cell volume). The estimated missing electron count per cell of 538 corresponds to 134 electrons per asymmetric unit. The two possible molecules of crystallization are n-hexane and dioxane, both of which happen to have an identical electron count of 48. Hence it is not possible to make a definitive determination of the solvent of crystallization, other than to note that both the void volume and electron count are consistent with the unit cell containing 12 solvent molecules (either n-hexane or dioxane or both) in addition to the 8 molecules of H4L.

The hydrogens were placed in calculated positions and refined using the riding model under the conditions: C~aryl~-H~aryl~=0.93, C~methyl~-H~methyl~=0.96, C~methylene~-H~methylene~ = 0.97, N-H = 0.86\%A, <i>U</i>~iso~(H) = 1.2<i>U</i>~eq~(C) except for the methyl hydrogens where <i>U</i>~iso~(H) = 1.5 <i>x</i> <i>U</i>~eq~(C).

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Fig. 1: Structure showing 50 % probability displacement ellipsoids for non-hydrogen atoms of Molecule A (Burnett & Johnson, 1996).

Fig. 1: Structure showing 50 % probability displacement ellipsoids for non-hydrogen atoms of Molecule B (Burnett & Johnson, 1996).

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_publ_section_acknowledgements

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No acknowledgements

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Sheldrick, G.M. (1997). *SADABS*. Univ. of G\ottingen, Germany.

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Sluis, P. v.d. and Spek, A.L., *Acta Crystallographica*, (1990), A46, 194-201.

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F2 > 2sigma(F2) is used only for calculating R-factors(gt) etc.
and is

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not relevant to the choice of reflections for refinement. R-factors based on F^2 are statistically about twice as large as those based on F , and R-factors based on ALL data will be even larger.

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O3A O 0.01968(7) 0.60881(8) 1.0792(2) 0.0256(5) Uani 1 1 d . . .
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N8A N 0.14278(8) 0.51502(10) 0.9766(3) 0.0243(6) Uani 1 1 d . . .
C1A C -0.05665(11) 0.39138(12) 0.5189(3) 0.0294(7) Uani 1 1 d . . .
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C3A C -0.06756(12) 0.29447(12) 0.4653(4) 0.0324(8) Uani 1 1 d . . .
H3A1 H -0.0911 0.3035 0.3964 0.039 Uiso 1 1 calc R . .
C4A C -0.05573(12) 0.24158(13) 0.4898(4) 0.0366(8) Uani 1 1 d . . .
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C5A C -0.02030(12) 0.22945(13) 0.5905(4) 0.0372(8) Uani 1 1 d . . .
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C7A C 0.04336(11) 0.25902(12) 0.7704(4) 0.0298(7) Uani 1 1 d . . .
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C12A C -0.03609(10) 0.55845(11) 0.7536(3) 0.0223(7) Uani 1 1 d . . .
C13A C 0.10015(11) 0.30333(12) 0.9419(3) 0.0287(7) Uani 1 1 d . . .
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H19B H 0.0484 0.5070 0.9527 0.029 Uiso 1 1 calc R . .
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H20B H 0.1019 0.5638 1.0961 0.030 Uiso 1 1 calc R . .
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H22B H 0.1470 0.5083 1.2554 0.036 Uiso 1 1 calc R . .
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H25B H 0.1350 0.4318 0.7950 0.035 Uiso 1 1 calc R . .
C26A C 0.18801(12) 0.43915(13) 0.6451(4) 0.0329(8) Uani 1 1 d . . .

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H27A H 0.2123 0.3628 0.6882 0.068 Uiso 1 1 calc R . . .
H27B H 0.2062 0.3737 0.5241 0.068 Uiso 1 1 calc R . . .
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N7B N 0.52882(8) 0.42101(9) 0.6256(3) 0.0248(6) Uani 1 1 d . . .
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C22B C 0.44500(10) 0.45587(11) 0.5812(3) 0.0250(7) Uani 1 1 d . . .
H22C H 0.4527 0.4931 0.5625 0.030 Uiso 1 1 calc R . . .
H22D H 0.4394 0.4521 0.6826 0.030 Uiso 1 1 calc R . . .
C23B C 0.39848(10) 0.44046(12) 0.4982(3) 0.0241(7) Uani 1 1 d . . .
H23C H 0.4057 0.4388 0.3973 0.029 Uiso 1 1 calc R . . .
H23D H 0.3881 0.4051 0.5280 0.029 Uiso 1 1 calc R . . .
C24B C 0.34284(11) 0.48266(13) 0.6709(3) 0.0293(7) Uani 1 1 d . . .
H24C H 0.3152 0.5071 0.6750 0.035 Uiso 1 1 calc R . . .
H24D H 0.3696 0.4986 0.7260 0.035 Uiso 1 1 calc R . . .
C25B C 0.32837(11) 0.43044(13) 0.7425(3) 0.0348(8) Uani 1 1 d . . .
H25C H 0.3571 0.4077 0.7531 0.042 Uiso 1 1 calc R . . .
H25D H 0.3046 0.4118 0.6824 0.042 Uiso 1 1 calc R . . .
C26B C 0.30641(13) 0.44030(15) 0.8888(4) 0.0421(9) Uani 1 1 d . . .
H26C H 0.2766 0.4613 0.8772 0.050 Uiso 1 1 calc R . . .
H26D H 0.3295 0.4610 0.9465 0.050 Uiso 1 1 calc R . . .
C27B C 0.29432(15) 0.38812(16) 0.9669(4) 0.0544(11) Uani 1 1 d . . .
H27D H 0.2716 0.3674 0.9100 0.082 Uiso 1 1 calc R . . .
H27E H 0.2799 0.3964 1.0570 0.082 Uiso 1 1 calc R . . .
H27F H 0.3239 0.3679 0.9827 0.082 Uiso 1 1 calc R . . .

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0.0011(11)
O2A 0.0518(15) 0.0191(12) 0.0522(17) -0.0017(11) 0.0011(12)
0.0055(10)
O3A 0.0294(12) 0.0239(11) 0.0235(12) -0.0005(10) -0.0011(9)
0.0010(9)
O4A 0.0341(13) 0.0446(14) 0.0370(14) 0.0081(12) -0.0101(11)
0.0041(11)
N1A 0.0314(14) 0.0215(13) 0.0190(14) -0.0012(11) -0.0016(11) -
0.0010(10)
N2A 0.0295(14) 0.0253(14) 0.0235(15) -0.0018(12) 0.0027(11)
0.0004(11)
N3A 0.0304(15) 0.0163(13) 0.0366(16) -0.0002(12) 0.0016(12)
0.0020(10)
N4A 0.0224(13) 0.0270(14) 0.0211(14) -0.0023(12) 0.0016(11) -
0.0013(10)
N5A 0.0235(14) 0.0252(14) 0.0319(16) 0.0027(12) 0.0039(12)
0.0043(11)
N6A 0.0218(13) 0.0232(13) 0.0240(14) -0.0053(11) 0.0006(11)
0.0049(10)
N7A 0.0204(13) 0.0293(15) 0.0329(16) 0.0030(12) -0.0031(11)
0.0047(10)
N8A 0.0198(13) 0.0309(14) 0.0221(14) -0.0025(12) 0.0000(11)
0.0017(10)

C1A 0.0307(18) 0.0331(18) 0.0244(18) -0.0057(15) 0.0018(14) -
0.0024(14)
C2A 0.0284(17) 0.0247(16) 0.0289(19) -0.0064(14) 0.0075(14) -
0.0028(13)
C3A 0.0368(19) 0.0323(19) 0.0282(19) -0.0115(15) 0.0032(15) -
0.0046(14)
C4A 0.042(2) 0.0332(19) 0.034(2) -0.0114(16) 0.0091(16) -0.0096(15)
C5A 0.046(2) 0.0243(17) 0.042(2) -0.0050(16) 0.0075(17) -0.0030(15)
C6A 0.0362(19) 0.0221(17) 0.0325(19) -0.0049(15) 0.0124(15) -
0.0044(13)
C7A 0.0333(18) 0.0220(17) 0.034(2) -0.0012(15) 0.0096(15) -
0.0003(14)
C8A 0.0225(16) 0.0259(16) 0.0200(16) -0.0055(14) 0.0035(13)
0.0023(12)
C9A 0.0274(17) 0.0323(18) 0.0160(16) -0.0013(14) -0.0067(13)
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0.0026(13)
C12A 0.0203(15) 0.0258(17) 0.0208(16) -0.0051(13) -0.0016(12) -
0.0006(12)
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C15A 0.032(2) 0.039(2) 0.065(3) 0.014(2) -0.0088(18) 0.0087(16)
C16A 0.0349(19) 0.0311(19) 0.044(2) 0.0057(17) -0.0087(16)
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0.0015(13)
C18A 0.0217(15) 0.0144(14) 0.0234(17) 0.0033(13) 0.0045(13) -
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C20A 0.0289(17) 0.0219(16) 0.0246(17) 0.0013(13) -0.0012(13)
0.0004(12)
C21A 0.0203(16) 0.0361(18) 0.0199(17) 0.0020(15) 0.0019(13)
0.0002(13)
C22A 0.0237(17) 0.044(2) 0.0230(18) 0.0010(16) -0.0003(13) -
0.0031(14)
C23A 0.0195(16) 0.0318(17) 0.0298(18) 0.0009(15) 0.0016(13) -
0.0004(12)
C24A 0.0217(16) 0.0376(18) 0.0261(18) 0.0047(15) 0.0015(13)
0.0008(13)
C25A 0.0287(17) 0.0382(19) 0.0217(17) -0.0047(15) 0.0041(14) -
0.0009(14)
C26A 0.0292(18) 0.0385(19) 0.0312(19) 0.0010(16) 0.0026(14)
0.0038(14)
C27A 0.053(2) 0.048(2) 0.035(2) -0.0015(18) 0.0002(18) 0.0095(18)
O1B 0.0482(15) 0.0242(12) 0.0411(15) -0.0014(11) -0.0041(11)
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O2B 0.0466(14) 0.0324(12) 0.0224(12) -0.0033(10) -0.0070(10) -
0.0026(10)

O3B 0.0378(14) 0.0502(15) 0.0541(17) 0.0128(14) -0.0232(12) -
0.0084(11)
O4B 0.0308(12) 0.0247(11) 0.0172(11) -0.0043(10) -0.0006(9)
0.0012(9)
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0.0074(11)
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0.0001(11)
N3B 0.0275(14) 0.0219(13) 0.0203(14) -0.0014(11) -0.0011(11) -
0.0002(10)
N4B 0.0225(14) 0.0302(15) 0.0325(16) -0.0005(13) -0.0009(12)
0.0020(11)
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0.0008(10)
N6B 0.0295(15) 0.0329(15) 0.0306(16) 0.0015(13) -0.0078(12)
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N7B 0.0233(13) 0.0233(13) 0.0277(15) -0.0033(12) -0.0022(11)
0.0029(10)
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0.0047(13)
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0.0047(13)
C3B 0.042(2) 0.0218(16) 0.034(2) -0.0046(15) 0.0017(16) 0.0019(14)
C4B 0.046(2) 0.0262(18) 0.030(2) -0.0091(15) -0.0016(16) -0.0046(15)
C5B 0.043(2) 0.0276(18) 0.029(2) -0.0057(15) 0.0002(16) 0.0003(14)
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0.0039(13)
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0.0008(13)
C8B 0.0241(17) 0.0340(19) 0.0297(19) -0.0014(15) -0.0012(14)
0.0045(13)
C9B 0.038(2) 0.0290(19) 0.057(2) 0.0037(18) -0.0067(18) 0.0052(15)
C10B 0.042(2) 0.038(2) 0.060(3) 0.0105(19) -0.0140(19) 0.0060(16)
C11B 0.034(2) 0.044(2) 0.054(2) 0.0115(19) -0.0169(17) -0.0051(16)
C12B 0.0247(17) 0.0334(19) 0.039(2) 0.0037(16) -0.0005(15)
0.0026(14)
C13B 0.0193(15) 0.0204(15) 0.0213(16) 0.0025(13) -0.0004(12) -
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C14B 0.0263(16) 0.0290(17) 0.0149(16) -0.0038(13) -0.0021(12) -
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C15B 0.0291(17) 0.0279(17) 0.0263(18) 0.0030(14) -0.0022(14) -
0.0008(13)
C16B 0.0301(17) 0.0177(15) 0.0250(17) -0.0010(13) -0.0015(13) -
0.0018(12)
C17B 0.0187(15) 0.0196(15) 0.0274(18) -0.0025(13) 0.0000(13) -
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C18B 0.0241(17) 0.039(2) 0.037(2) 0.0029(17) -0.0047(15) -0.0038(14)
C19B 0.0201(16) 0.0417(19) 0.0271(18) -0.0060(16) -0.0017(13) -
0.0049(13)
C20B 0.0231(17) 0.0385(19) 0.0298(19) -0.0010(15) -0.0042(14) -
0.0040(14)

C21B 0.0262(16) 0.0182(15) 0.0236(17) 0.0005(13) 0.0003(13)
0.0002(12)
C22B 0.0280(17) 0.0250(16) 0.0219(17) -0.0010(14) 0.0006(13) -
0.0030(12)
C23B 0.0222(16) 0.0300(17) 0.0200(16) -0.0049(14) -0.0014(13) -
0.0004(12)
C24B 0.0197(16) 0.0414(19) 0.0268(18) -0.0059(16) -0.0003(13) -
0.0017(13)
C25B 0.0266(17) 0.045(2) 0.033(2) -0.0049(17) 0.0008(15) -0.0003(15)
C26B 0.036(2) 0.065(2) 0.0254(19) -0.0106(18) 0.0079(15) -0.0130(17)
C27B 0.061(3) 0.079(3) 0.024(2) -0.004(2) 0.0145(18) -0.017(2)

_geom_special_details

;

All esds (except the esd in the dihedral angle between two l.s.
planes)

are estimated using the full covariance matrix. The cell esds are
taken

into account individually in the estimation of esds in distances,
angles

and torsion angles; correlations between esds in cell parameters
are only

used when they are defined by crystal symmetry. An approximate
(isotropic)

treatment of cell esds is used for estimating esds involving l.s.
planes.

;

loop_

_geom_bond_atom_site_label_1

_geom_bond_atom_site_label_2

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_geom_bond_site_symmetry_2

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O3A C18A 1.241(3) . ?

O4A C21A 1.219(3) . ?

N1A C1A 1.364(4) . ?

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N1A H1A 0.8600 . ?

N2A C6A 1.341(4) . ?

N2A C2A 1.347(4) . ?

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N4A C12A 1.335(4) . ?

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N5A C13A 1.341(4) . ?

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C22A H22B 0.9700 . ?
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O3B C18B 1.210(4) . ?
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N4B C12B 1.337(4) . ?
N5B C17B 1.338(3) . ?
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N6B C12B 1.396(4) . ?
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N7B C21B 1.357(4) . ?
N7B C17B 1.415(4) . ?
N7B H7B 0.8600 . ?
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N8B C24B 1.486(4) . ?
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C22B C23B 1.522(4) . ?

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C22B H22D 0.9700 . ?
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C23B H23D 0.9700 . ?
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C24B H24D 0.9700 . ?
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C25B H25D 0.9700 . ?
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C13A N3A H3A 116.4 . . ?
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C20A N8A C23A 110.8(2) . . ?
C24A N8A C23A 110.5(2) . . ?
O1A C1A N1A 124.3(3) . . ?
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N2A C2A C1A 117.9(3) . . ?
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 before (in any language or medium) and is not being considered for
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 elsewhere; that all authors concur with and are aware of the
 submission; that
 all workers involved in the study are listed as authors or given
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in the acknowledgements; that I have obtained permission for and acknowledged the source of any excerpts from other copyright works; and that to the best of my knowledge the paper contains no statements which are libellous, unlawful or in any way actionable. All coauthors have made significant scientific contributions to the work reported, including the ideas and their execution, and share responsibility and accountability for the results.
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Fig. 1: Structure showing 50 % probability displacement ellipsoids for non-hydrogen atoms and hydrogen atoms as arbitrary spheres (Burnett & Johnson, 1996). The dioxane molecule of crystallisation is not shown.

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Burnett, M.N. and Johnson, C.K. (1996). ORTEP-III: Report ORNL-6895. Oak Ridge National Laboratory, Tennessee, USA.

Sheldrick, G.M. (1996). *SADABS*. Univ. of G"ottingen, Germany.

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Siemens (1995). *SMART* (Version 4.050) and *SAINT* (Version 4.050). Siemens Analytical X-ray Instruments Inc., Madison, Wisconsin, USA.

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F2 > 2sigma(F2) is used only for calculating R-factors(gt) etc.
and is
not relevant to the choice of reflections for refinement. R-
factors based

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on F^2 are statistically about twice as large as those based on F ,
and R -

factors based on ALL data will be even larger.

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Pd Pd 0.08338(3) 0.06063(4) 0.134264(17) 0.01668(13) Uani 1 1 d . . .
.
Cl Cl 0.22471(8) 0.07387(14) 0.12427(5) 0.0199(3) Uani 1 1 d . . .
O1 O 0.1210(3) -0.3360(4) -0.05910(16) 0.0265(9) Uani 1 1 d . . .
N1 N 0.1207(3) -0.1474(5) 0.00994(19) 0.0213(10) Uani 1 1 d . . .
H1 H 0.1493 -0.0685 0.0277 0.026 Uiso 1 1 calc R . .
C1 C 0.1550(3) -0.2229(6) -0.0298(2) 0.0205(11) Uani 1 1 d . . .
O2 O 0.4354(3) 0.2503(5) -0.0089(2) 0.0363(10) Uani 1 1 d . . .
N2 N 0.2649(3) -0.0184(5) -0.01231(18) 0.0184(9) Uani 1 1 d . . .
C2 C 0.2390(3) -0.1594(6) -0.0358(2) 0.0208(11) Uani 1 1 d . . .
O3 O -0.1668(2) -0.0210(5) 0.15458(16) 0.0264(9) Uani 1 1 d . . .

```

N3 N 0.3218(3) 0.2738(5) 0.03288(19) 0.0212(10) Uani 1 1 d . . .
H3 H 0.2778 0.2253 0.0388 0.025 Uiso 1 1 calc R . .
C3 C 0.2866(4) -0.2493(7) -0.0654(3) 0.0296(13) Uani 1 1 d . . .
H3A H 0.2660 -0.3456 -0.0813 0.036 Uiso 1 1 calc R . .
O4 O 0.1060(2) 0.6809(4) 0.17040(16) 0.0237(8) Uani 1 1 d . . .
N4 N 0.0295(3) -0.0959(5) 0.06896(18) 0.0191(9) Uani 1 1 d . . .
C4 C 0.3646(4) -0.1939(8) -0.0707(3) 0.0376(15) Uani 1 1 d . . .
H4 H 0.3990 -0.2536 -0.0888 0.045 Uiso 1 1 calc R . .
N5 N 0.2739(3) 0.4759(5) 0.08045(18) 0.0183(9) Uani 1 1 d . . .
C5 C 0.3909(4) -0.0478(8) -0.0486(3) 0.0331(14) Uani 1 1 d . . .
H5 H 0.4428 -0.0062 -0.0526 0.040 Uiso 1 1 calc R . .
N6 N -0.0357(3) -0.0038(5) 0.1322(2) 0.0220(10) Uani 1 1 d . . .
C6 C 0.3393(3) 0.0362(6) -0.0205(2) 0.0235(12) Uani 1 1 d . . .
N7 N 0.2180(3) 0.6746(5) 0.12995(18) 0.0194(9) Uani 1 1 d . . .
H7 H 0.2170 0.7746 0.1325 0.023 Uiso 1 1 calc R . .
C7 C 0.3700(3) 0.1958(6) 0.0020(2) 0.0237(12) Uani 1 1 d . . .
N8 N 0.0992(3) 0.2053(5) 0.20650(18) 0.0180(9) Uani 1 1 d . . .
C8 C 0.0442(3) -0.1840(6) 0.0251(2) 0.0183(11) Uani 1 1 d . . .
C9 C -0.0149(3) -0.2980(6) -0.0006(2) 0.0231(12) Uani 1 1 d . . .
H9 H -0.0057 -0.3595 -0.0312 0.028 Uiso 1 1 calc R . .
C10 C -0.0883(4) -0.3192(6) 0.0201(2) 0.0249(12) Uani 1 1 d . . .
H10 H -0.1280 -0.3962 0.0031 0.030 Uiso 1 1 calc R . .
C11 C -0.1033(3) -0.2288(6) 0.0649(2) 0.0234(12) Uani 1 1 d . . .
H11 H -0.1520 -0.2436 0.0790 0.028 Uiso 1 1 calc R . .
C12 C -0.0430(3) -0.1157(6) 0.0880(2) 0.0201(11) Uani 1 1 d . . .
C13 C 0.3369(3) 0.4261(6) 0.0561(2) 0.0196(11) Uani 1 1 d . . .
C14 C 0.4079(3) 0.5157(7) 0.0542(2) 0.0250(12) Uani 1 1 d . . .
H14 H 0.4501 0.4775 0.0371 0.030 Uiso 1 1 calc R . .
C15 C 0.4143(4) 0.6635(6) 0.0782(2) 0.0255(12) Uani 1 1 d . . .
H15 H 0.4609 0.7269 0.0768 0.031 Uiso 1 1 calc R . .
C16 C 0.3521(3) 0.7175(6) 0.1044(2) 0.0224(12) Uani 1 1 d . . .
H16 H 0.3562 0.8160 0.1215 0.027 Uiso 1 1 calc R . .
C17 C 0.2828(3) 0.6185(6) 0.1041(2) 0.0188(11) Uani 1 1 d . . .
C18 C -0.0952(3) 0.0416(6) 0.1606(2) 0.0233(12) Uani 1 1 d . . .
C19 C -0.0650(3) 0.1804(6) 0.2004(2) 0.0216(11) Uani 1 1 d . . .
H19A H -0.1022 0.1912 0.2269 0.026 Uiso 1 1 calc R . .
H19B H -0.0721 0.2734 0.1759 0.026 Uiso 1 1 calc R . .
C20 C 0.0287(3) 0.1732(7) 0.2376(2) 0.0233(12) Uani 1 1 d . . .
H20A H 0.0354 0.2474 0.2699 0.028 Uiso 1 1 calc R . .
H20B H 0.0388 0.0702 0.2552 0.028 Uiso 1 1 calc R . .
C21 C 0.1565(3) 0.6015(6) 0.1518(2) 0.0174(11) Uani 1 1 d . . .
C22 C 0.1550(3) 0.4274(6) 0.1536(2) 0.0199(11) Uani 1 1 d . . .
H22A H 0.2126 0.3881 0.1722 0.024 Uiso 1 1 calc R . .
H22B H 0.1369 0.3861 0.1136 0.024 Uiso 1 1 calc R . .
C23 C 0.0921(4) 0.3745(6) 0.1889(2) 0.0210(11) Uani 1 1 d . . .
H23A H 0.1017 0.4374 0.2245 0.025 Uiso 1 1 calc R . .
H23B H 0.0334 0.3944 0.1654 0.025 Uiso 1 1 calc R . .
C24 C 0.1852(3) 0.1812(6) 0.2512(2) 0.0225(11) Uani 1 1 d . . .
H24A H 0.1887 0.2507 0.2845 0.027 Uiso 1 1 calc R . .
H24B H 0.2311 0.2100 0.2331 0.027 Uiso 1 1 calc R . .
C25 C 0.2010(4) 0.0145(6) 0.2745(2) 0.0257(12) Uani 1 1 d . . .
H25A H 0.1715 -0.0018 0.3054 0.031 Uiso 1 1 calc R . .
H25B H 0.1771 -0.0581 0.2426 0.031 Uiso 1 1 calc R . .
C26 C 0.2965(4) -0.0169(8) 0.2990(3) 0.0468(18) Uani 1 1 d . . .

H26A H 0.3253 -0.0017 0.2677 0.056 Uiso 1 1 calc R . . .
H26B H 0.3044 -0.1250 0.3114 0.056 Uiso 1 1 calc R . . .
C27 C 0.3394(5) 0.0867(11) 0.3512(4) 0.084(4) Uani 1 1 d . . .
H27A H 0.3388 0.1929 0.3381 0.127 Uiso 1 1 calc R . . .
H27B H 0.3982 0.0536 0.3674 0.127 Uiso 1 1 calc R . . .
H27C H 0.3083 0.0791 0.3811 0.127 Uiso 1 1 calc R . . .
O5 O 0.4796(6) 0.9915(14) 0.2091(4) 0.134(3) Uani 1 1 d . . .
O6 O 0.6493(7) 0.8892(13) 0.2578(5) 0.146(4) Uani 1 1 d . . .
C28 C 0.4990(9) 0.833(2) 0.2443(6) 0.146(7) Uani 1 1 d . . .
H28A H 0.4547 0.8102 0.2646 0.175 Uiso 1 1 calc R . . .
H28B H 0.5021 0.7472 0.2178 0.175 Uiso 1 1 calc R . . .
C29 C 0.5786(6) 0.8576(14) 0.2846(6) 0.099(4) Uani 1 1 d . . .
H29A H 0.5932 0.7662 0.3097 0.118 Uiso 1 1 calc R . . .
H29B H 0.5733 0.9449 0.3098 0.118 Uiso 1 1 calc R . . .
C30 C 0.6343(10) 1.0281(15) 0.2216(5) 0.129(6) Uani 1 1 d . . .
H30A H 0.6772 1.0358 0.1990 0.155 Uiso 1 1 calc R . . .
H30B H 0.6391 1.1198 0.2465 0.155 Uiso 1 1 calc R . . .
C31 C 0.5478(10) 1.0196(19) 0.1814(7) 0.132(5) Uiso 1 1 d . . .
H31A H 0.5360 1.1169 0.1596 0.158 Uiso 1 1 calc R . . .
H31B H 0.5472 0.9372 0.1529 0.158 Uiso 1 1 calc R . . .

loop_

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0.00052(17)
Cl 0.0243(6) 0.0156(6) 0.0224(6) -0.0012(5) 0.0107(5) -0.0007(5)
O1 0.038(2) 0.018(2) 0.026(2) -0.0045(17) 0.0118(17) -0.0020(17)
N1 0.028(2) 0.014(2) 0.021(2) -0.0010(18) 0.0054(19) 0.0011(18)
C1 0.029(3) 0.016(3) 0.017(3) 0.002(2) 0.007(2) 0.005(2)
O2 0.032(2) 0.035(2) 0.052(3) -0.009(2) 0.029(2) -0.0062(19)
N2 0.023(2) 0.018(2) 0.015(2) 0.0002(17) 0.0062(18) 0.0031(18)
C2 0.025(3) 0.018(3) 0.017(3) 0.001(2) 0.002(2) 0.002(2)
O3 0.024(2) 0.034(2) 0.023(2) 0.0042(17) 0.0104(16) -0.0019(17)
N3 0.021(2) 0.018(2) 0.028(2) -0.0002(19) 0.0126(19) -0.0010(18)
C3 0.033(3) 0.025(3) 0.030(3) -0.010(3) 0.008(3) 0.005(3)
O4 0.036(2) 0.0152(18) 0.025(2) 0.0013(16) 0.0152(17) 0.0015(17)
N4 0.023(2) 0.016(2) 0.017(2) 0.0026(17) 0.0046(18) 0.0000(18)
C4 0.038(4) 0.040(4) 0.037(4) -0.016(3) 0.015(3) 0.005(3)
N5 0.023(2) 0.015(2) 0.019(2) 0.0021(17) 0.0098(18) 0.0022(18)
C5 0.027(3) 0.041(4) 0.035(3) -0.009(3) 0.014(3) 0.004(3)
N6 0.024(2) 0.018(2) 0.026(2) -0.0002(19) 0.0096(19) -0.0032(19)
C6 0.024(3) 0.026(3) 0.022(3) 0.004(2) 0.008(2) 0.008(2)
N7 0.027(2) 0.009(2) 0.026(2) 0.0014(18) 0.0137(19) 0.0010(18)
C7 0.025(3) 0.024(3) 0.024(3) -0.002(2) 0.010(2) 0.005(2)
N8 0.025(2) 0.014(2) 0.018(2) 0.0019(17) 0.0114(18) -0.0018(18)
C8 0.028(3) 0.012(2) 0.015(2) 0.003(2) 0.006(2) 0.003(2)
C9 0.027(3) 0.015(3) 0.026(3) -0.003(2) 0.005(2) 0.003(2)
C10 0.030(3) 0.014(3) 0.027(3) 0.004(2) 0.001(2) -0.004(2)

```

C11 0.023(3) 0.021(3) 0.025(3) 0.003(2) 0.003(2) 0.001(2)
C12 0.023(3) 0.014(3) 0.022(3) 0.002(2) 0.004(2) 0.004(2)
C13 0.022(3) 0.017(3) 0.021(3) 0.003(2) 0.009(2) 0.001(2)
C14 0.023(3) 0.026(3) 0.030(3) -0.001(2) 0.015(2) 0.001(2)
C15 0.025(3) 0.018(3) 0.035(3) 0.004(2) 0.012(2) -0.004(2)
C16 0.028(3) 0.014(3) 0.025(3) 0.003(2) 0.007(2) -0.004(2)
C17 0.023(3) 0.019(3) 0.016(3) 0.003(2) 0.008(2) 0.003(2)
C18 0.028(3) 0.022(3) 0.022(3) 0.011(2) 0.012(2) 0.007(2)
C19 0.029(3) 0.021(3) 0.021(3) 0.003(2) 0.016(2) 0.002(2)
C20 0.033(3) 0.021(3) 0.022(3) 0.000(2) 0.017(2) -0.006(2)
C21 0.024(3) 0.016(3) 0.014(2) 0.002(2) 0.007(2) 0.000(2)
C22 0.029(3) 0.015(3) 0.019(3) 0.000(2) 0.012(2) 0.001(2)
C23 0.031(3) 0.011(2) 0.025(3) 0.000(2) 0.014(2) 0.000(2)
C24 0.031(3) 0.017(3) 0.020(3) 0.002(2) 0.008(2) -0.004(2)
C25 0.035(3) 0.019(3) 0.024(3) 0.001(2) 0.009(2) -0.002(2)
C26 0.035(4) 0.045(4) 0.059(5) 0.029(4) 0.009(3) 0.004(3)
C27 0.061(5) 0.078(6) 0.083(6) 0.053(5) -0.036(5) -0.036(5)
O5 0.104(7) 0.170(9) 0.122(7) 0.018(7) 0.019(6) 0.008(7)
O6 0.147(9) 0.161(10) 0.141(8) -0.006(7) 0.058(7) -0.002(8)
C28 0.095(9) 0.24(2) 0.089(9) -0.025(12) -0.009(7) 0.039(12)
C29 0.059(6) 0.099(9) 0.136(10) -0.027(8) 0.023(7) 0.009(6)
C30 0.191(15) 0.091(9) 0.080(8) 0.035(7) -0.011(9) -0.003(9)

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All esds (except the esd in the dihedral angle between two l.s. planes)

are estimated using the full covariance matrix. The cell esds are taken

into account individually in the estimation of esds in distances, angles

and torsion angles; correlations between esds in cell parameters are only

used when they are defined by crystal symmetry. An approximate (isotropic)

treatment of cell esds is used for estimating esds involving l.s. planes.

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Pd N4 2.045(4) . ?
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Pd N8 2.056(4) . ?
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Pd C1 2.3349(13) . ?
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O1 C1 1.229(6) . ?
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N1 C1 1.359(7) . ?
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N1 C8 1.397(7) . ?
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N1 H1 0.8600 . ?
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C1 C2 1.490(7) . ?
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O2 C7 1.230(7) . ?
N2 C6 1.337(7) . ?
N2 C2 1.348(7) . ?
C2 C3 1.388(8) . ?
O3 C18 1.239(6) . ?
N3 C7 1.362(7) . ?
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N3 H3 0.8600 . ?
C3 C4 1.369(9) . ?
C3 H3A 0.9300 . ?
O4 C21 1.220(6) . ?
N4 C8 1.342(6) . ?
N4 C12 1.358(7) . ?
C4 C5 1.378(9) . ?
C4 H4 0.9300 . ?
N5 C17 1.334(7) . ?
N5 C13 1.349(7) . ?
C5 C6 1.386(8) . ?
C5 H5 0.9300 . ?
N6 C18 1.353(7) . ?
N6 C12 1.392(7) . ?
C6 C7 1.502(8) . ?
N7 C21 1.372(6) . ?
N7 C17 1.412(6) . ?
N7 H7 0.8600 . ?
N8 C23 1.504(6) . ?
N8 C24 1.509(7) . ?
N8 C20 1.517(6) . ?
C8 C9 1.383(7) . ?
C9 C10 1.393(8) . ?
C9 H9 0.9300 . ?
C10 C11 1.374(8) . ?
C10 H10 0.9300 . ?
C11 C12 1.374(7) . ?
C11 H11 0.9300 . ?
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C14 C15 1.380(8) . ?
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C15 C16 1.375(8) . ?
C15 H15 0.9300 . ?
C16 C17 1.396(7) . ?
C16 H16 0.9300 . ?
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C19 H19B 0.9700 . ?
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C20 H20B 0.9700 . ?
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C22 C23 1.526(7) . ?
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C22 H22B 0.9700 . ?
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C24 C25 1.527(7) . ?
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C27 H27B 0.9600 . ?
C27 H27C 0.9600 . ?
O5 C31 1.428(16) . ?
O5 C28 1.578(18) . ?
O6 C30 1.445(14) . ?
O6 C29 1.454(13) . ?
C28 C29 1.388(15) . ?
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C28 H28B 0.9700 . ?
C29 H29A 0.9700 . ?
C29 H29B 0.9700 . ?
C30 C31 1.456(17) . ?
C30 H30A 0.9700 . ?
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C31 H31A 0.9700 . ?
C31 H31B 0.9700 . ?

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N6 Pd N8 95.73(17) . . ?
N4 Pd N8 161.01(17) . . ?
N6 Pd C1 164.88(13) . . ?
N4 Pd C1 100.78(12) . . ?
N8 Pd C1 97.95(12) . . ?
C1 N1 C8 127.1(4) . . ?
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C8 N1 H1 116.5 . . ?
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O1 C1 C2 120.9(5) . . ?
N1 C1 C2 115.1(5) . . ?
C6 N2 C2 116.5(4) . . ?
N2 C2 C3 123.4(5) . . ?
N2 C2 C1 118.6(5) . . ?
C3 C2 C1 118.0(5) . . ?
C7 N3 C13 126.5(5) . . ?
C7 N3 H3 116.7 . . ?
C13 N3 H3 116.7 . . ?

C4 C3 C2 118.9(5) . . ?
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C2 C3 H3A 120.6 . . ?
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C5 C4 H4 120.7 . . ?
C17 N5 C13 117.0(4) . . ?
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C6 C5 H5 120.4 . . ?
C18 N6 C12 129.0(5) . . ?
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N2 C6 C7 119.5(5) . . ?
C5 C6 C7 117.3(5) . . ?
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C21 N7 H7 113.6 . . ?
C17 N7 H7 113.6 . . ?
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O2 C7 C6 119.5(5) . . ?
N3 C7 C6 116.9(5) . . ?
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C24 N8 Pd 112.3(3) . . ?
C20 N8 Pd 109.6(3) . . ?
N4 C8 C9 119.6(5) . . ?
N4 C8 N1 114.0(4) . . ?
C9 C8 N1 126.4(5) . . ?
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C11 C10 C9 121.5(5) . . ?
C11 C10 H10 119.3 . . ?
C9 C10 H10 119.3 . . ?
C12 C11 C10 116.9(5) . . ?
C12 C11 H11 121.6 . . ?
C10 C11 H11 121.6 . . ?
N4 C12 C11 122.1(5) . . ?
N4 C12 N6 104.1(4) . . ?
C11 C12 N6 133.8(5) . . ?
N5 C13 C14 123.3(5) . . ?
N5 C13 N3 112.6(4) . . ?
C14 C13 N3 124.2(5) . . ?
C15 C14 C13 118.1(5) . . ?
C15 C14 H14 120.9 . . ?
C13 C14 H14 120.9 . . ?
C16 C15 C14 120.3(5) . . ?
C16 C15 H15 119.8 . . ?

C14 C15 H15 119.8 . . ?
 C15 C16 C17 117.3(5) . . ?
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 C17 C16 H16 121.3 . . ?
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 C16 C17 N7 117.5(5) . . ?
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 O3 C18 C19 123.3(5) . . ?
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 H19A C19 H19B 107.5 . . ?
 N8 C20 C19 117.5(4) . . ?
 N8 C20 H20A 107.9 . . ?
 C19 C20 H20A 107.9 . . ?
 N8 C20 H20B 107.9 . . ?
 C19 C20 H20B 107.9 . . ?
 H20A C20 H20B 107.2 . . ?
 O4 C21 N7 118.9(5) . . ?
 O4 C21 C22 122.0(5) . . ?
 N7 C21 C22 119.1(4) . . ?
 C21 C22 C23 109.3(4) . . ?
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 C23 C22 H22A 109.8 . . ?
 C21 C22 H22B 109.8 . . ?
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 H22A C22 H22B 108.3 . . ?
 N8 C23 C22 114.9(4) . . ?
 N8 C23 H23A 108.5 . . ?
 C22 C23 H23A 108.5 . . ?
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 C22 C23 H23B 108.5 . . ?
 H23A C23 H23B 107.5 . . ?
 N8 C24 C25 114.2(4) . . ?
 N8 C24 H24A 108.7 . . ?
 C25 C24 H24A 108.7 . . ?
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 H25A C25 H25B 108.0 . . ?
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 C27 C26 H26B 108.9 . . ?

H26A C26 H26B 107.7 . . ?
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 H27A C27 H27C 109.5 . . ?
 H27B C27 H27C 109.5 . . ?
 C31 O5 C28 108.2(11) . . ?
 C30 O6 C29 112.1(12) . . ?
 C29 C28 O5 104.0(14) . . ?
 C29 C28 H28A 111.0 . . ?
 O5 C28 H28A 111.0 . . ?
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 O5 C28 H28B 111.0 . . ?
 H28A C28 H28B 109.0 . . ?
 C28 C29 O6 114.6(12) . . ?
 C28 C29 H29A 108.6 . . ?
 O6 C29 H29A 108.6 . . ?
 C28 C29 H29B 108.6 . . ?
 O6 C29 H29B 108.6 . . ?
 H29A C29 H29B 107.6 . . ?
 O6 C30 C31 108.7(13) . . ?
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 C31 C30 H30A 109.9 . . ?
 O6 C30 H30B 109.9 . . ?
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 O5 C31 C30 115.2(13) . . ?
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3. Compound [Pd(*N*-(3-aminopropyl)caprolactam)(H₂L)] (5).

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data_global

_audit_creation_method SHELXL-97

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_publ_contact_author_email   'g.clark@auckland.ac.nz'
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'Clark, George R.'
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;

'Wright, L. James.'
;
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Private Bag 92019
Auckland
New Zealand
;

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;
Hydrogen atoms were placed in calculated positions and refined using the riding model [C-H 0.93-0.97 \(%A), with $U_{\text{iso}}(\text{H}) = 1.2$ or 1.5 times $U_{\text{eq}}(\text{C})$. The crystals contain a water molecule of crystallization, whose hydrogen atoms were not located. There is high thermal motion in the carbons at the end of the aliphatic chain.
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Fig. 1: Structure showing 50 % probability displacement ellipsoids for non-hydrogen atoms and hydrogen atoms as arbitrary spheres (Burnett & Johnson, 1996).
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No acknowledgements
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;

Burnett, M.N. and Johnson, C.K. (1996). ORTEP-III: Report ORNL-6895. Oak Ridge National Laboratory, Tennessee, USA.

Sheldrick, G.M. (1997). *SADABS*. Univ. of G"ottingen, Germany.

Sheldrick, G.M. (1997). *SHELXS97* and *SHELXL97*. Release 97-1, University of G"ottingen, Germany.

Siemens (1995). *SHELXTL* (Version 5), *SMART* (Version 4.050) and *SAINT* (Version 4.050). Siemens Analytical X-ray Instruments Inc., Madison, Wisconsin, USA.

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'x, -y-1/2, z-1/2'

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based
on F, with F set to zero for negative F2. The threshold
expression of
F2 > 2sigma(F2) is used only for calculating R-factors(gt) etc.
and is
not relevant to the choice of reflections for refinement. R-
factors based
on F2 are statistically about twice as large as those based on F,
and R-

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factors based on ALL data will be even larger.

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O1 O 0.2910(4) 0.2861(3) -0.0008(2) 0.0288(11) Uani 1 1 d . . .
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O4 O 0.4288(4) 0.7524(3) 0.3199(3) 0.0446(14) Uani 1 1 d . . .
O5 O 0.5792(6) 0.3755(3) 0.4184(3) 0.066(2) Uani 1 1 d . . .
O6 O 0.2777(11) 0.1642(9) -0.1036(7) 0.199(5) Uiso 1 1 d . . .
N1 N 0.3176(4) 0.4077(3) 0.0719(3) 0.0200(12) Uani 1 1 d . . .
N2 N 0.5242(4) 0.4170(3) 0.0630(3) 0.0191(12) Uani 1 1 d . . .
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N4 N 0.1601(4) 0.4874(3) 0.0819(2) 0.0191(11) Uani 1 1 d . . .
N5 N 0.5423(4) 0.6804(3) 0.1789(3) 0.0219(12) Uani 1 1 d . . .
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N7 N 0.4660(5) 0.8032(3) 0.2167(3) 0.0316(14) Uani 1 1 d . . .
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N8 N 0.1002(5) 0.8468(3) 0.1710(3) 0.0251(13) Uani 1 1 d . . .
N9 N 0.3525(4) 0.5722(3) 0.1630(3) 0.0214(12) Uani 1 1 d . . .
H9A H 0.3872 0.6229 0.1689 0.026 Uiso 1 1 calc R . . .
H9B H 0.2841 0.5804 0.1347 0.026 Uiso 1 1 calc R . . .
N10 N 0.5447(5) 0.5177(4) 0.4139(3) 0.0370(15) Uani 1 1 d . . .
C1 C 0.3496(5) 0.3435(4) 0.0322(3) 0.0207(15) Uani 1 1 d . . .
C2 C 0.4717(5) 0.3497(4) 0.0289(3) 0.0179(14) Uani 1 1 d . . .
C3 C 0.5273(5) 0.2956(4) -0.0073(3) 0.0230(16) Uani 1 1 d . . .
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C4 C 0.6373(6) 0.3135(4) -0.0090(4) 0.0261(16) Uani 1 1 d . . .
H4 H 0.6767 0.2766 -0.0322 0.031 Uiso 1 1 calc R . . .
C5 C 0.6903(5) 0.3863(4) 0.0236(3) 0.0238(15) Uani 1 1 d . . .
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C6 C 0.6304(5) 0.4363(4) 0.0612(3) 0.0188(14) Uani 1 1 d . . .
C7 C 0.6762(5) 0.5151(4) 0.1038(3) 0.0216(14) Uani 1 1 d . . .
C8 C 0.2030(5) 0.4083(4) 0.0785(3) 0.0175(14) Uani 1 1 d . . .
C9 C 0.1406(5) 0.3350(4) 0.0823(3) 0.0227(16) Uani 1 1 d . . .
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C10 C 0.0322(5) 0.3445(4) 0.0923(3) 0.0223(15) Uani 1 1 d . . .
H10 H -0.0106 0.2966 0.0960 0.027 Uiso 1 1 calc R . . .
C11 C -0.0124(6) 0.4232(4) 0.0969(3) 0.0232(15) Uani 1 1 d . . .
H11 H -0.0850 0.4298 0.1036 0.028 Uiso 1 1 calc R . . .
C12 C 0.0552(5) 0.4937(4) 0.0911(3) 0.0202(13) Uani 1 1 d . . .
C13 C 0.6286(6) 0.6293(4) 0.1752(3) 0.0247(16) Uani 1 1 d . . .
C14 C 0.7376(6) 0.6486(5) 0.2111(3) 0.0291(17) Uani 1 1 d . . .
H14 H 0.7972 0.6133 0.2079 0.035 Uiso 1 1 calc R . . .
C15 C 0.7554(6) 0.7215(5) 0.2516(4) 0.041(2) Uani 1 1 d . . .
H15 H 0.8276 0.7353 0.2761 0.050 Uiso 1 1 calc R . . .
C16 C 0.6667(6) 0.7740(5) 0.2562(4) 0.0336(18) Uani 1 1 d . . .
H16 H 0.6773 0.8230 0.2836 0.040 Uiso 1 1 calc R . . .
C17 C 0.5626(6) 0.7506(4) 0.2183(3) 0.0253(16) Uani 1 1 d . . .
C18 C 0.0564(6) 0.6533(4) 0.0910(3) 0.0240(16) Uani 1 1 d . . .
C19 C -0.0208(6) 0.7256(4) 0.1026(4) 0.0296(17) Uani 1 1 d . . .
H19A H -0.0431 0.7162 0.1472 0.035 Uiso 1 1 calc R . . .
H19B H -0.0881 0.7240 0.0649 0.035 Uiso 1 1 calc R . . .
C20 C 0.0321(6) 0.8146(4) 0.1042(3) 0.0268(16) Uani 1 1 d . . .
H20A H 0.0785 0.8151 0.0694 0.032 Uiso 1 1 calc R . . .
H20B H -0.0284 0.8547 0.0880 0.032 Uiso 1 1 calc R . . .
C21 C 0.4016(6) 0.7970(4) 0.2667(4) 0.0324(18) Uani 1 1 d . . .
C22 C 0.2937(6) 0.8489(4) 0.2487(4) 0.0316(17) Uani 1 1 d . . .
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H22B H 0.2691 0.8622 0.2918 0.038 Uiso 1 1 calc R . . .
C23 C 0.2027(6) 0.7983(4) 0.1983(4) 0.0295(17) Uani 1 1 d . . .
H23A H 0.2324 0.7786 0.1585 0.035 Uiso 1 1 calc R . . .
H23B H 0.1841 0.7488 0.2232 0.035 Uiso 1 1 calc R . . .
C24 C 0.0352(6) 0.8602(5) 0.2265(4) 0.0369(19) Uani 1 1 d . . .
H24A H 0.0865 0.8735 0.2711 0.044 Uiso 1 1 calc R . . .
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C25 C -0.0509(7) 0.9316(5) 0.2076(4) 0.046(2) Uani 1 1 d . . .
H25A H -0.1053 0.9168 0.1646 0.056 Uiso 1 1 calc R . . .
H25B H -0.0906 0.9382 0.2455 0.056 Uiso 1 1 calc R . . .

C26 C 0.0054(9) 1.0157(6) 0.1962(7) 0.087(4) Uani 1 1 d . . .
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H26B H 0.0362 1.0104 0.1542 0.104 Uiso 1 1 calc R . .
C27 C -0.0684(9) 1.0919(6) 0.1877(6) 0.083(4) Uani 1 1 d . . .
H27A H -0.1345 1.0816 0.1513 0.124 Uiso 1 1 calc R . .
H27B H -0.0287 1.1397 0.1747 0.124 Uiso 1 1 calc R . .
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C28 C 0.3375(6) 0.5423(5) 0.2338(4) 0.0350(18) Uani 1 1 d . . .
H28A H 0.2989 0.4882 0.2283 0.042 Uiso 1 1 calc R . .
H28B H 0.2917 0.5825 0.2527 0.042 Uiso 1 1 calc R . .
C29 C 0.4511(6) 0.5327(5) 0.2858(4) 0.0332(18) Uani 1 1 d . . .
H29A H 0.4941 0.4890 0.2687 0.040 Uiso 1 1 calc R . .
H29B H 0.4923 0.5855 0.2876 0.040 Uiso 1 1 calc R . .
C30 C 0.4392(6) 0.5098(5) 0.3608(4) 0.0419(19) Uani 1 1 d . . .
H30A H 0.3835 0.5466 0.3739 0.050 Uiso 1 1 calc R . .
H30B H 0.4123 0.4520 0.3607 0.050 Uiso 1 1 calc R . .
C31 C 0.6074(8) 0.4492(5) 0.4386(4) 0.043(2) Uani 1 1 d . . .
C32 C 0.7181(7) 0.4615(5) 0.4920(4) 0.049(2) Uani 1 1 d . . .
H32A H 0.7428 0.4072 0.5135 0.059 Uiso 1 1 calc R . .
H32B H 0.7061 0.4990 0.5294 0.059 Uiso 1 1 calc R . .
C33 C 0.8116(7) 0.4986(5) 0.4588(4) 0.050(2) Uani 1 1 d . . .
H33A H 0.8836 0.4864 0.4900 0.061 Uiso 1 1 calc R . .
H33B H 0.8096 0.4702 0.4140 0.061 Uiso 1 1 calc R . .
C34 C 0.8029(7) 0.5930(6) 0.4457(4) 0.053(2) Uani 1 1 d . . .
H34A H 0.8629 0.6103 0.4233 0.064 Uiso 1 1 calc R . .
H34B H 0.8142 0.6218 0.4912 0.064 Uiso 1 1 calc R . .
C35 C 0.6905(7) 0.6218(5) 0.3990(4) 0.044(2) Uani 1 1 d . . .
H35A H 0.6944 0.6824 0.3912 0.053 Uiso 1 1 calc R . .
H35B H 0.6808 0.5943 0.3532 0.053 Uiso 1 1 calc R . .
C36 C 0.5873(6) 0.6039(5) 0.4287(4) 0.0373(19) Uani 1 1 d . . .
H36A H 0.6060 0.6127 0.4797 0.045 Uiso 1 1 calc R . .
H36B H 0.5286 0.6438 0.4083 0.045 Uiso 1 1 calc R . .

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O2 0.022(3) 0.029(3) 0.033(3) -0.006(2) 0.016(2) -0.005(2)
O3 0.022(3) 0.023(2) 0.037(3) -0.006(2) 0.015(2) -0.003(2)
O4 0.045(3) 0.057(4) 0.038(3) 0.013(3) 0.021(3) 0.011(3)
O5 0.133(6) 0.034(3) 0.040(4) -0.001(3) 0.037(4) -0.022(4)
N1 0.021(3) 0.019(3) 0.023(3) 0.000(2) 0.012(2) 0.003(2)
N2 0.016(3) 0.025(3) 0.018(3) 0.007(2) 0.007(2) 0.001(2)
N3 0.023(3) 0.025(3) 0.022(3) -0.002(2) 0.009(2) 0.002(2)
N4 0.017(3) 0.025(3) 0.016(3) -0.004(2) 0.006(2) 0.001(2)
N5 0.020(3) 0.022(3) 0.024(3) -0.001(2) 0.006(2) 0.000(2)
N6 0.015(3) 0.028(3) 0.027(3) -0.004(2) 0.013(2) -0.001(2)
N7 0.042(4) 0.027(3) 0.029(3) 0.001(3) 0.014(3) 0.002(3)

N8 0.028(3) 0.028(3) 0.022(3) -0.006(2) 0.011(3) 0.004(3)
N9 0.017(3) 0.024(3) 0.025(3) 0.000(2) 0.009(2) -0.002(2)
N10 0.046(4) 0.040(4) 0.026(3) -0.002(3) 0.009(3) -0.012(3)
C1 0.022(4) 0.022(3) 0.019(4) 0.003(3) 0.005(3) 0.000(3)
C2 0.027(4) 0.017(3) 0.014(3) 0.002(3) 0.013(3) -0.004(3)
C3 0.025(4) 0.025(4) 0.021(4) 0.002(3) 0.010(3) -0.001(3)
C4 0.029(4) 0.025(4) 0.027(4) -0.001(3) 0.013(3) 0.011(3)
C5 0.020(4) 0.026(4) 0.028(4) -0.001(3) 0.012(3) 0.005(3)
C6 0.022(4) 0.019(3) 0.017(3) 0.000(3) 0.007(3) 0.003(3)
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C12 0.016(3) 0.029(4) 0.014(3) 0.005(3) 0.002(2) 0.006(3)
C13 0.031(4) 0.029(4) 0.015(3) 0.000(3) 0.006(3) -0.005(3)
C14 0.025(4) 0.043(4) 0.022(4) -0.004(3) 0.010(3) 0.004(3)
C15 0.025(4) 0.056(5) 0.041(5) -0.018(4) 0.001(4) -0.010(4)
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C17 0.035(4) 0.027(4) 0.017(4) 0.001(3) 0.012(3) 0.005(3)
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C20 0.027(4) 0.034(4) 0.021(4) 0.001(3) 0.010(3) 0.003(3)
C21 0.034(4) 0.028(4) 0.036(5) -0.009(3) 0.011(4) 0.000(3)
C22 0.032(4) 0.031(4) 0.032(4) -0.009(3) 0.009(3) 0.005(3)
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C35 0.050(5) 0.045(5) 0.039(5) -0.003(4) 0.014(4) -0.014(4)
C36 0.041(5) 0.038(4) 0.030(4) -0.009(4) 0.002(4) -0.004(4)

`_geom_special_details`

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All esds (except the esd in the dihedral angle between two l.s. planes)

are estimated using the full covariance matrix. The cell esds are taken

into account individually in the estimation of esds in distances, angles

and torsion angles; correlations between esds in cell parameters are only

used when they are defined by crystal symmetry. An approximate (isotropic)

treatment of cell esds is used for estimating esds involving l.s. planes.

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Pd N9 H9B 108.3 . . ?
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 C5 C6 C7 124.9(6) . . ?
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4. Compound [Pd(OH₂)(H₂L)] (6).

data_Cpd_6
data_global
_audit_creation_method SHELXL-97

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For related literature on the .

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in any way actionable. All coauthors have made significant scientific contributions to the work reported, including the ideas and their execution, and share responsibility and accountability for the results.

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_publ_section_exptl_refinement

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Hydrogen atoms were placed in calculated positions and refined using the riding model [C-H 0.93-0.97 \%, with $U_{iso}(H) = 1.2$ or 1.5 times $U_{eq}(C)$. The hydrogen atoms of the coordinated water molecule were refined as a quasi-methyl group with O-H distances set at 0.82 \%. One hydrogen was assigned zero occupancy.
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Fig. 1: Structure showing 50 % probability displacement ellipsoids for non-hydrogen atoms and hydrogen atoms as arbitrary spheres (Burnett & Johnson, 1996). The dichloromethane molecule of crystallisation is not shown. There is a hydrogen bond between O5 and N5, and bifurcated hydrogen bonds between O5 and O3, and O5 and N4. There is an intermolecular hydrogen bond between N6 and O2.
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_publ_section_acknowledgements

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No acknowledgements
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_publ_section_references

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_cell_angle_alpha 90.1220(10)
_cell_angle_beta 98.3350(10)
_cell_angle_gamma 93.2520(10)
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Refinement of F2 against ALL reflections. The weighted R-factor
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goodness of fit S are based on F2, conventional R-factors R are
based
on F, with F set to zero for negative F2. The threshold
expression of
F2 > 2sigma(F2) is used only for calculating R-factors(gt) etc.
and is
not relevant to the choice of reflections for refinement. R-
factors based
on F2 are statistically about twice as large as those based on F,
and R-
factors based on ALL data will be even larger.
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P=(Fo2+2Fc2)/3'
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C12 C1 0.0441(2) 0.34252(13) 0.60440(9) 0.0416(4) Uani 1 1 d . . .
O1 O 0.2465(5) 0.1817(3) -0.2226(2) 0.0294(8) Uani 1 1 d . . .
O2 O 0.3606(5) -0.2405(3) 0.0751(2) 0.0253(8) Uani 1 1 d . . .
O3 O 0.2651(5) 0.3602(3) 0.15735(19) 0.0225(7) Uani 1 1 d . . .
O4 O 0.0826(6) 0.1595(3) 0.4097(2) 0.0366(9) Uani 1 1 d . . .
O5 O 0.0717(4) 0.1862(3) 0.07340(19) 0.0186(7) Uani 1 1 d . . .
H5A H 0.1170 0.2526 0.0730 0.028 Uiso 1 1 calc R . .
H5B H 0.0845 0.1619 0.1191 0.028 Uiso 1 1 calc R . .
N1 N 0.1925(5) 0.1886(3) -0.0906(2) 0.0194(8) Uani 1 1 d . . .
N2 N 0.2851(5) -0.0216(3) -0.0673(2) 0.0176(8) Uani 1 1 d . . .
N3 N 0.2441(5) -0.0570(3) 0.0796(2) 0.0177(8) Uani 1 1 d . . .
N4 N 0.2462(5) 0.3525(3) -0.0120(2) 0.0193(8) Uani 1 1 d . . .
N5 N 0.1866(5) 0.0475(3) 0.1879(2) 0.0188(8) Uani 1 1 d . . .
N6 N 0.3192(5) 0.5115(3) 0.0757(2) 0.0209(8) Uani 1 1 d . . .
H6 H 0.3626 0.5822 0.0765 0.025 Uiso 1 1 calc R . .
N7 N 0.1459(6) 0.1803(3) 0.2838(2) 0.0226(9) Uani 1 1 d . . .
H7 H 0.1543 0.2304 0.2468 0.027 Uiso 1 1 calc R . .
N8 N 0.3891(5) 0.4233(3) 0.3417(2) 0.0232(9) Uani 1 1 d . . .
C1 C 0.2382(7) 0.1375(4) -0.1578(3) 0.0226(10) Uani 1 1 d . . .
C2 C 0.2904(6) 0.0137(4) -0.1423(3) 0.0210(10) Uani 1 1 d . . .
C3 C 0.3534(7) -0.0588(4) -0.1950(3) 0.0236(10) Uani 1 1 d . . .
H3 H 0.3553 -0.0368 -0.2476 0.028 Uiso 1 1 calc R . .
C4 C 0.4143(6) -0.1658(4) -0.1683(3) 0.0237(10) Uani 1 1 d . . .
H4 H 0.4586 -0.2153 -0.2032 0.028 Uiso 1 1 calc R . .
C5 C 0.4093(6) -0.1992(4) -0.0897(3) 0.0208(10) Uani 1 1 d . . .

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H5 H 0.4529 -0.2694 -0.0710 0.025 Uiso 1 1 calc R . .
C6 C 0.3371(6) -0.1244(4) -0.0404(3) 0.0183(9) Uani 1 1 d . . .
C7 C 0.3145(6) -0.1471(4) 0.0454(3) 0.0198(10) Uani 1 1 d . . .
C8 C 0.1829(6) 0.3096(4) -0.0848(3) 0.0193(10) Uani 1 1 d . . .
C9 C 0.1172(7) 0.3801(4) -0.1483(3) 0.0231(10) Uani 1 1 d . . .
H9 H 0.0784 0.3490 -0.1988 0.028 Uiso 1 1 calc R . .
C10 C 0.1123(6) 0.4983(4) -0.1328(3) 0.0222(10) Uani 1 1 d . . .
H10 H 0.0675 0.5474 -0.1733 0.027 Uiso 1 1 calc R . .
C11 C 0.1732(7) 0.5435(4) -0.0578(3) 0.0230(10) Uani 1 1 d . . .
H11 H 0.1688 0.6223 -0.0466 0.028 Uiso 1 1 calc R . .
C12 C 0.2415(6) 0.4667(4) 0.0002(3) 0.0191(9) Uani 1 1 d . . .
C13 C 0.2276(6) -0.0562(4) 0.1608(3) 0.0187(9) Uani 1 1 d . . .
C14 C 0.2512(7) -0.1496(4) 0.2129(3) 0.0247(11) Uani 1 1 d . . .
H14 H 0.2738 -0.2226 0.1944 0.030 Uiso 1 1 calc R . .
C15 C 0.2403(7) -0.1312(4) 0.2926(3) 0.0252(11) Uani 1 1 d . . .
H15 H 0.2571 -0.1926 0.3279 0.030 Uiso 1 1 calc R . .
C16 C 0.2051(7) -0.0238(4) 0.3211(3) 0.0259(11) Uani 1 1 d . . .
H16 H 0.1986 -0.0112 0.3747 0.031 Uiso 1 1 calc R . .
C17 C 0.1798(6) 0.0642(4) 0.2657(3) 0.0205(10) Uani 1 1 d . . .
C18 C 0.3341(6) 0.4575(4) 0.1470(3) 0.0198(10) Uani 1 1 d . . .
C19 C 0.4452(7) 0.5253(4) 0.2156(3) 0.0226(10) Uani 1 1 d . . .
H19A H 0.4662 0.6049 0.1992 0.027 Uiso 1 1 calc R . .
H19B H 0.5606 0.4916 0.2277 0.027 Uiso 1 1 calc R . .
C20 C 0.3568(7) 0.5259(4) 0.2908(3) 0.0249(11) Uani 1 1 d . . .
H20A H 0.4004 0.5952 0.3218 0.030 Uiso 1 1 calc R . .
H20B H 0.2287 0.5304 0.2756 0.030 Uiso 1 1 calc R . .
C21 C 0.1014(7) 0.2213(4) 0.3533(3) 0.0246(11) Uani 1 1 d . . .
C22 C 0.0813(7) 0.3518(4) 0.3569(3) 0.0257(11) Uani 1 1 d . . .
H22A H -0.0148 0.3675 0.3868 0.031 Uiso 1 1 calc R . .
H22B H 0.0502 0.3808 0.3034 0.031 Uiso 1 1 calc R . .
C23 C 0.2546(7) 0.4147(4) 0.3963(3) 0.0268(11) Uani 1 1 d . . .
H23A H 0.2298 0.4922 0.4126 0.032 Uiso 1 1 calc R . .
H23B H 0.3019 0.3730 0.4436 0.032 Uiso 1 1 calc R . .
C24 C 0.5718(7) 0.4361(5) 0.3874(3) 0.0272(11) Uani 1 1 d . . .
H24A H 0.5776 0.5021 0.4235 0.033 Uiso 1 1 calc R . .
H24B H 0.6564 0.4533 0.3507 0.033 Uiso 1 1 calc R . .
C25 C 0.6293(7) 0.3292(4) 0.4356(3) 0.0269(11) Uani 1 1 d . . .
H25A H 0.7518 0.3439 0.4611 0.032 Uiso 1 1 calc R . .
H25B H 0.5548 0.3185 0.4772 0.032 Uiso 1 1 calc R . .
C26 C 0.6176(7) 0.2171(5) 0.3873(3) 0.0317(12) Uani 1 1 d . . .
H26A H 0.4978 0.2052 0.3581 0.038 Uiso 1 1 calc R . .
H26B H 0.7005 0.2246 0.3487 0.038 Uiso 1 1 calc R . .
C27 C 0.6603(9) 0.1118(5) 0.4386(4) 0.0423(15) Uani 1 1 d . . .
H27A H 0.7790 0.1230 0.4675 0.063 Uiso 1 1 calc R . .
H27B H 0.6533 0.0437 0.4053 0.063 Uiso 1 1 calc R . .
H27C H 0.5757 0.1021 0.4754 0.063 Uiso 1 1 calc R . .
C28 C 0.1333(7) 0.2040(5) 0.5987(3) 0.0298(12) Uani 1 1 d . . .
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0.00260(13)
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C12 0.0425(8) 0.0406(8) 0.0426(8) 0.0061(7) 0.0057(7) 0.0116(6)
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O3 0.039(2) 0.0161(16) 0.0134(16) 0.0001(13) 0.0066(14) 0.0011(14)
O4 0.061(3) 0.036(2) 0.0165(19) 0.0036(16) 0.0159(18) 0.0044(19)
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0.0009(13)
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N2 0.020(2) 0.0139(18) 0.019(2) 0.0026(15) 0.0033(16) 0.0016(15)
N3 0.024(2) 0.0103(17) 0.020(2) -0.0033(15) 0.0068(16) -0.0018(15)
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N5 0.024(2) 0.0176(19) 0.0151(19) 0.0029(15) 0.0060(16) -0.0010(16)
N6 0.029(2) 0.0133(18) 0.020(2) 0.0008(16) 0.0045(17) 0.0006(16)
N7 0.036(2) 0.021(2) 0.0124(19) 0.0030(16) 0.0078(17) 0.0030(17)
N8 0.031(2) 0.025(2) 0.014(2) -0.0002(16) 0.0037(17) 0.0012(17)
C1 0.032(3) 0.022(2) 0.014(2) -0.0010(19) 0.002(2) 0.005(2)
C2 0.025(3) 0.019(2) 0.019(2) -0.0003(19) 0.0028(19) 0.0009(19)
C3 0.031(3) 0.021(2) 0.018(2) -0.0035(19) 0.003(2) -0.003(2)
C4 0.024(3) 0.028(3) 0.020(2) -0.004(2) 0.005(2) 0.003(2)
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C6 0.021(2) 0.018(2) 0.016(2) -0.0018(18) 0.0018(18) -0.0013(18)
C7 0.024(2) 0.019(2) 0.015(2) 0.0006(18) 0.0016(19) -0.0036(19)
C8 0.027(3) 0.019(2) 0.013(2) 0.0038(18) 0.0097(19) 0.0018(19)
C9 0.030(3) 0.026(2) 0.014(2) 0.0025(19) 0.003(2) 0.003(2)
C10 0.027(3) 0.022(2) 0.018(2) 0.0074(19) 0.003(2) 0.007(2)
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C13 0.025(2) 0.020(2) 0.011(2) 0.0040(18) 0.0031(18) 0.0013(19)
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C16 0.033(3) 0.029(3) 0.016(2) 0.003(2) 0.007(2) 0.001(2)
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C20 0.036(3) 0.021(2) 0.018(2) -0.0034(19) 0.003(2) 0.005(2)
C21 0.028(3) 0.028(3) 0.018(2) -0.003(2) 0.004(2) 0.002(2)
C22 0.032(3) 0.030(3) 0.015(2) -0.003(2) 0.002(2) 0.006(2)
C23 0.038(3) 0.026(3) 0.018(2) -0.004(2) 0.005(2) 0.006(2)
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C25 0.029(3) 0.035(3) 0.017(2) 0.001(2) 0.004(2) 0.004(2)
C26 0.032(3) 0.031(3) 0.031(3) 0.004(2) 0.001(2) 0.005(2)
C27 0.054(4) 0.031(3) 0.045(4) 0.007(3) 0.012(3) 0.012(3)
C28 0.032(3) 0.035(3) 0.022(3) -0.004(2) 0.006(2) 0.001(2)

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All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

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Pd N1 2.022(4) . ?
Pd O5 2.042(3) . ?
Pd N3 2.068(4) . ?
C11 C28 1.749(5) . ?
C12 C28 1.774(5) . ?
O1 C1 1.221(6) . ?
O2 C7 1.236(6) . ?
O3 C18 1.233(5) . ?
O4 C21 1.213(6) . ?
O5 H5A 0.8200 . ?
O5 H5B 0.8200 . ?
N1 C1 1.379(6) . ?
N1 C8 1.404(6) . ?
N2 C6 1.330(6) . ?
N2 C2 1.343(6) . ?
N3 C7 1.359(6) . ?
N3 C13 1.403(6) . ?
N4 C12 1.334(6) . ?
N4 C8 1.340(6) . ?
N5 C17 1.342(6) . ?
N5 C13 1.347(6) . ?
N6 C18 1.355(6) . ?
N6 C12 1.413(6) . ?
N6 H6 0.8600 . ?
N7 C21 1.365(6) . ?
N7 C17 1.416(6) . ?
N7 H7 0.8600 . ?
N8 C23 1.473(6) . ?
N8 C20 1.475(6) . ?
N8 C24 1.484(7) . ?
C1 C2 1.514(6) . ?
C2 C3 1.375(6) . ?
C3 C4 1.394(7) . ?

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C3 H3 0.9300 . ?
C4 C5 1.395(7) . ?
C4 H4 0.9300 . ?
C5 C6 1.387(6) . ?
C5 H5 0.9300 . ?
C6 C7 1.511(6) . ?
C8 C9 1.400(6) . ?
C9 C10 1.389(7) . ?
C9 H9 0.9300 . ?
C10 C11 1.379(7) . ?
C10 H10 0.9300 . ?
C11 C12 1.388(7) . ?
C11 H11 0.9300 . ?
C13 C14 1.397(6) . ?
C14 C15 1.385(7) . ?
C14 H14 0.9300 . ?
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C15 H15 0.9300 . ?
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C16 H16 0.9300 . ?
C18 C19 1.520(6) . ?
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C19 H19B 0.9700 . ?
C20 H20A 0.9700 . ?
C20 H20B 0.9700 . ?
C21 C22 1.521(7) . ?
C22 C23 1.525(7) . ?
C22 H22A 0.9700 . ?
C22 H22B 0.9700 . ?
C23 H23A 0.9700 . ?
C23 H23B 0.9700 . ?
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C25 H25A 0.9700 . ?
C25 H25B 0.9700 . ?
C26 C27 1.517(7) . ?
C26 H26A 0.9700 . ?
C26 H26B 0.9700 . ?
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N1 Pd N3 162.24(14) . . ?
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Pd O5 H5B 109.5 . . ?
H5A O5 H5B 109.5 . . ?
C1 N1 C8 121.1(4) . . ?
C1 N1 Pd 114.2(3) . . ?
C8 N1 Pd 123.4(3) . . ?
C6 N2 C2 123.6(4) . . ?
C6 N2 Pd 118.6(3) . . ?
C2 N2 Pd 117.8(3) . . ?
C7 N3 C13 121.6(4) . . ?
C7 N3 Pd 113.1(3) . . ?
C13 N3 Pd 125.0(3) . . ?
C12 N4 C8 118.1(4) . . ?
C17 N5 C13 120.6(4) . . ?
C18 N6 C12 128.5(4) . . ?
C18 N6 H6 115.8 . . ?
C12 N6 H6 115.8 . . ?
C21 N7 C17 127.2(4) . . ?
C21 N7 H7 116.4 . . ?
C17 N7 H7 116.4 . . ?
C23 N8 C20 108.8(4) . . ?
C23 N8 C24 110.2(4) . . ?
C20 N8 C24 109.4(4) . . ?
O1 C1 N1 127.9(4) . . ?
O1 C1 C2 120.5(4) . . ?
N1 C1 C2 111.5(4) . . ?
N2 C2 C3 119.3(4) . . ?
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C2 C3 C4 118.8(5) . . ?
C2 C3 H3 120.6 . . ?
C4 C3 H3 120.6 . . ?
C3 C4 C5 120.5(4) . . ?
C3 C4 H4 119.8 . . ?
C5 C4 H4 119.8 . . ?
C6 C5 C4 117.9(4) . . ?
C6 C5 H5 121.0 . . ?
C4 C5 H5 121.0 . . ?
N2 C6 C5 119.8(4) . . ?
N2 C6 C7 114.5(4) . . ?
C5 C6 C7 125.7(4) . . ?
O2 C7 N3 128.7(4) . . ?
O2 C7 C6 118.6(4) . . ?
N3 C7 C6 112.7(4) . . ?
N4 C8 C9 122.7(4) . . ?
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C9 C8 N1 124.1(4) . . ?

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C10 C9 C8 117.4(4) . . ?
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 C9 C10 H10 119.7 . . ?
 C10 C11 C12 117.3(4) . . ?
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 C12 C11 H11 121.3 . . ?
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 N4 C12 N6 117.3(4) . . ?
 C11 C12 N6 118.8(4) . . ?
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 N5 C13 N3 113.7(4) . . ?
 C14 C13 N3 126.4(4) . . ?
 C15 C14 C13 118.6(4) . . ?
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 C14 C15 H15 119.2 . . ?
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 C17 C16 H16 121.7 . . ?
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 N5 C17 N7 112.6(4) . . ?
 C16 C17 N7 124.8(4) . . ?
 O3 C18 N6 123.9(4) . . ?
 O3 C18 C19 120.9(4) . . ?
 N6 C18 C19 115.2(4) . . ?
 C18 C19 C20 113.3(4) . . ?
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 C20 C19 H19B 108.9 . . ?
 H19A C19 H19B 107.7 . . ?
 N8 C20 C19 114.3(4) . . ?
 N8 C20 H20A 108.7 . . ?
 C19 C20 H20A 108.7 . . ?
 N8 C20 H20B 108.7 . . ?
 C19 C20 H20B 108.7 . . ?
 H20A C20 H20B 107.6 . . ?
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 N7 C21 C22 115.4(4) . . ?
 C21 C22 C23 110.8(4) . . ?
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 N8 C24 H24A 108.7 . . ?
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 C25 C24 H24B 108.7 . . ?
 H24A C24 H24B 107.6 . . ?
 C26 C25 C24 114.6(4) . . ?
 C26 C25 H25A 108.6 . . ?
 C24 C25 H25A 108.6 . . ?
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 C24 C25 H25B 108.6 . . ?
 H25A C25 H25B 107.6 . . ?
 C27 C26 C25 112.7(5) . . ?
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 C25 C26 H26A 109.1 . . ?
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 H27B C27 H27C 109.5 . . ?
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