# **Supporting Information**

# Heavy metal recovery from electroplating wastewater by synthesis of the mixed-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/metal oxide magnetite photocatalysts

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#### Preparation of M-Fe<sub>3</sub>O<sub>4</sub> nanoparticles from EPW

200 mL of S-EPW was placed into a 250 mL beaker, and its pH was adjusted to 2 using  $H_2SO_4$  solution (3 mol L<sup>-1</sup>) under continuous stirring. Then, FeSO<sub>4</sub> $\bigcirc$ 7H<sub>2</sub>O was introduced to reduce Cr<sup>6+</sup> in EPW and provided Fe<sup>2+</sup> for ferrites, and the optimum ratio of FeSO<sub>4</sub> $\bigcirc$ 7H<sub>2</sub>O: Cr<sup>6+</sup> was tested with the mass ratios of 30: 1, 50: 1, 100: 1, 200: 1, and 300: 1 in series. After the reduction of Cr<sup>6+</sup> for 15 min, NaOH solution (6 mol L<sup>-1</sup>) was dropped to increase the pH to 10. Then the beaker was sealed and stored in a thermostat water bath at 80 °C for 10 h. The precipitates were separated by centrifugation, washed with distilled water and ethanol, and then dried in vacuum at 60 °C for 10 h to form the M-Fe<sub>3</sub>O<sub>4</sub> products.

#### Preparation of M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub> core-shell nanoparticles

In a typical procedure, 0.02 g M-Fe<sub>3</sub>O<sub>4</sub> nanoparticles were dispersed in 80 mL ethanol under sonication for 10 min, and then the mixture was transferred to a threenecked flask with continuous mechanical stirring (200 rpm). 20 mL deionized water, 2.32 mL aqueous ammonia (mass fraction of 25%), and 0.45 mL tetraethyl orthosilicate (the density of 0.932 g mL<sup>-1</sup>) were introduced and mixed together at room temperature. After 6 h, the M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub> nanoparticles were collected via centrifugation and dried in vacuum at 60 °C for 10 h.

## Leaching test

The Toxicity Characteristic Leaching Procedure (TCLP) was used to assess the chemical stability of the M-Fe<sub>3</sub>O<sub>4</sub> products. Accordingly, distilled water with a pH of  $4.93 \pm 0.05$  was used as the extraction fluid with a liquid-to-solid ratio of 20: 1. The obtained mixtures were shaken at a rate of  $30 \pm 2$  rpm for 18 h, and then the leachate was filtered and determined with ICP.<sup>1,2</sup>

#### XRD and magnetic analysis of M-Fe<sub>3</sub>O<sub>4</sub>

The crystal phases of the as-prepared M-Fe<sub>3</sub>O<sub>4</sub> samples are shown in Fig. S1a, and the phases of Fe<sub>3</sub>O<sub>4</sub>, FeCr<sub>2</sub>O<sub>4</sub>, ZnFe<sub>2</sub>O<sub>4</sub>, and CuFe<sub>2</sub>O<sub>4</sub> are mainly found in the M-Fe<sub>3</sub>O<sub>4</sub> products. Among them, Fe<sub>3</sub>O<sub>4</sub> and CuFe<sub>2</sub>O<sub>4</sub> possess the inverse spinel structure,<sup>3, 4</sup> while FeCr<sub>2</sub>O<sub>4</sub> and ZnFe<sub>2</sub>O<sub>4</sub> exhibit the normal spinel structure.<sup>5, 6</sup> In the preparation process of M-Fe<sub>3</sub>O<sub>4</sub>, the reduction of Cr<sup>6+</sup> is first occurred with the addition of FeSO<sub>4</sub>co<sub>3</sub>7H<sub>2</sub>O, and the reaction can be expressed as Eq. (1):

$$Cr_2O_7^{2-}+6Fe^{2+}+14H^+\rightarrow 2Cr^{3+}+6Fe^{3+}+7H_2O$$
 (1)

Then, the amount of  $Cr^{3+}$  and  $Fe^{3+}$  ions are increased, accompanied by the decreased  $Fe^{2+}$  content, while the  $Cu^{2+}$ ,  $Zn^{2+}$ , and  $Ni^{2+}$  ions can substitute  $Fe^{2+}$  ions to form M-Fe<sub>3</sub>O<sub>4</sub>, and thus the principle of the ferrite process can be presented in Eq. (2-5):<sup>7</sup>

$$Fe^{2+} + 2Fe^{3+} + 8OH^{-} \rightarrow Fe_3O_4 + 4H_2O$$

$$\tag{2}$$

$$Zn^{2+} + 2Fe^{3+} + 8OH^{-} \rightarrow ZnFe_2O_4 + 4H_2O$$
(3)

$$Cu^{2+} + 2Fe^{3+} + 8OH^{-} \rightarrow CuFe_2O_4 + 4H_2O$$
(4)

$$Fe^{2+} + 2Cr^{3+} + 8OH^{-} \rightarrow FeCr_2O_4 + 4H_2O$$
(5)

According to the increased added amount of  $FeSO_4 \mathfrak{S}7H_2O$ , the following reaction may also occur as Eq. (6):<sup>8</sup>

$$\chi \text{ Me}^{2+} + (3-\chi) \text{ Fe}^{2+} + 6\text{OH}^{-} + 1/2\text{O}_2 \rightarrow \text{Me}_{\gamma}\text{Fe}(3-\chi)\text{O}_4 + 3\text{H}_2\text{O}$$
 (6)

In the XRD patterns, there is no diffraction peak for NiFe<sub>2</sub>O<sub>4</sub>, since the mass concentration of Ni<sup>2+</sup> in S-EPW is too low (4 mg L<sup>-1</sup>). In addition, the diffraction peak intensities of M-Fe<sub>3</sub>O<sub>4</sub> are first increased and then decreased as the mass ratios of FeSO<sub>4</sub>c<sub>3</sub>7H<sub>2</sub>O: Cr<sup>6+</sup> increased from 30: 1 to 300: 1, which are in conformity with the magnetic properties of M-Fe<sub>3</sub>O<sub>4</sub> (Fig. S1b). Theoretically, the needed mass ratio of  $FeSO_4$   $m cm^{6+}$  is 23: 1, and  $Fe^{2+}$  will be easily oxidized to  $Fe^{3+}$  in the practical condition where exposed to air. In the case of low mass ratio (30: 1), poor crystal quality of M-Fe<sub>3</sub>O<sub>4</sub> is observed, combined with a small saturated magnetization  $(M_s)$ of 5.94 emu g<sup>-1</sup> and a high coercivity (H<sub>c</sub>) of 145.5 O<sub>e</sub> (Table S2). In contrast, a higher crystallization degree is obtained in the mass ratio of 50: 1, where the M<sub>s</sub> and H<sub>c</sub> values are 55.05 emu g<sup>-1</sup> and 55.67 Oe, respectively. If the mass ratios increased further, the M<sub>s</sub> values of M-Fe<sub>3</sub>O<sub>4</sub> are not changed much, i.e., 54.90 (100: 1), and 69.42 emu g<sup>-1</sup> (200: 1), and higher H<sub>c</sub> values are presented, which will increase the trend of aggregation for the M-Fe<sub>3</sub>O<sub>4</sub> nanoparticles. On the other hand, both of them are not cost-efficient, since more Fe<sup>2+</sup> ions are consumed, compared to the cases with lower mass ratios. Furthermore, Cr, Cu, Zn, and Ni ions in M-Fe<sub>3</sub>O<sub>4</sub> prepared with the mass ratio of 50: 1 are more stable than those in other M-Fe<sub>3</sub>O<sub>4</sub> samples (Table S3). Based on the above results, the mass ratio of 50: 1 is the best one for M-Fe<sub>3</sub>O<sub>4</sub> preparation, and the obtained M-Fe<sub>3</sub>O<sub>4</sub> products are chosen as the supports for the metal oxide photocatalysts in this work.



**Fig. S1** (a) XRD patterns and (b) room temperature (300 K) magnetic hysteresis loops of M-Fe<sub>3</sub>O<sub>4</sub> prepared with various mass ratios of FeSO<sub>4</sub> $\sim$ 37H<sub>2</sub>O: Cr<sup>6+</sup>.

**Table S1.** Heavy metal concentrations in supernatant liquors before and after the precipitation reactions.

Elements	Cr	Cu	Zn	Ni	Fe	рН	COD <sub>Cr</sub>
R-EPW	113.36	98.04	60.92	2.59	15.60	2.34	270
<b>R-EPW</b> after precipitation	2.15	0.02	UD	0.02	UD	-	185
Recovery rate (%)	98.1	99.9	100	99.2	100	-	-
S-EPW	118.22	89.67	49.46	3.93	19.86	-	-
S-EPW after precipitation	1.20	0.01	UD	UD	UD	-	-
Recovery rate (%)	98.9	99.9	100	100	100	-	-

Note:

UD: Below detection limit.

All the parameters are expressed in mg  $L^{-1}$  except pH and recovery rate (%). The Cr<sup>6+</sup> content in R-EPW was detected to be 101.27 mg  $L^{-1}$  by the 1, 5-diphenylcarbohydrazide spectrophotometric method.<sup>9</sup> The chemical oxygen demand (COD<sub>Cr</sub>) of R-EPW was measured using the potassium dichromate method.

Samples	M <sub>s</sub> (emu g <sup>-1</sup> )	H <sub>c</sub> (Oe)
30: 1	5.94	145.5
50: 1	55.05	55.67
100: 1	54.90	158.45
200: 1	69.42	73.18
300: 1	47.55	87.56

**Table S2** Magnetic parameters of M-Fe<sub>3</sub>O<sub>4</sub> prepared with various mass ratios of FeSO<sub>4</sub><sup>cos</sup>7H<sub>2</sub>O: Cr<sup>6+</sup>.

**Table S3** Chemical stability of the M-Fe<sub>3</sub>O<sub>4</sub> products prepared with various mass ratios of FeSO<sub>4</sub> $\sim$ 37H<sub>2</sub>O: Cr<sup>6+</sup>.

	Heavy metal concentration (mg L <sup>-1</sup> )			
Mass ratios of $FeSO_4 \circ 3/H_2 \circ Cr^{\circ}$	Cr	Cu	Zn	Ni
30: 1	UD	0.20	1.25	0.17
50: 1	UD	2.70	5.89	2.82
100: 1	0.79	40.00	9.21	3.72
200: 1	UD	20.90	3.37	3.94
300: 1	0.42	31.00	2.41	3.02
TCLP Standard <sup>a</sup>	5.00	15.00	-	-

Note:

UD: Below detection limit.

<sup>a</sup> Ref: D. Chen, J. Hou, L. H. Yao, H. M. Jin, G. R. Qian and Z. P. Xu, *Sep. Purif. Technol.*, 2010, **75**, 210.



Fig. S2 XRD pattern of M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>.



Fig. S3 TEM image of M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>.



Fig. S4 TEM images of (a) M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/ZnO, and (b) M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/CuO.

	Table S4 Physica	l parameters	of the M	A-Fe <sub>3</sub> O <sub>4</sub> (a	DSiO <sub>2</sub> /metal	oxides.
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Samples	Band gap energy (eV)	Absorption edge (nm)	BET (m <sup>2</sup> g <sup>-1</sup> )	Pore size (nm)
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /ZnO	3.15	393.65	15	3.37
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /CuO	2.03	610.84	18	3.37
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /Fe <sub>2</sub> O <sub>3</sub>	2.10	590.48	16	24.5
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /NiO	3.53	351.27	177	4.23

Table S5 Magnetic parameters of M-Fe<sub>3</sub>O<sub>4</sub>, M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub> and the M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/metal oxides.

Samples	M <sub>s</sub> (emu g <sup>-1</sup> )	H <sub>c</sub> (Oe)
M-Fe <sub>3</sub> O <sub>4</sub> (50: 1)	55.05	55.67
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub>	17.91	71.04
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /ZnO	0.30	30.39
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /CuO	0.49	74.74
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /Fe <sub>2</sub> O <sub>3</sub>	23.03	182.29
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /NiO	2.28	53.83

**Table S6** Chemical element contents of M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/ZnO and M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/CuO obtained from XPS and EDS.

	M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /ZnO	M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /CuO	
Elements	EDS	XPS	EDS
Zn content (wt %)	76.98	-	-
Cu content(wt %)	-	46.24	47.48
Si content(wt %)	0.33	4.01	0.16
O content(wt %)	18.18	-	16.74
Fe content(wt %)	0.19	-	0.38



Fig. S5 Time-dependent absorption spectra of MO over (a) M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/ZnO and (b) M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/NiO under UV-vis irradiation.

Samples	Degradation rates (%) after 150 min
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /ZnO, 1.00 g L <sup>-1</sup>	91.5
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /CuO, 0.50 g L <sup>-1</sup>	17.6
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /CuO, 1.00 g L <sup>-1</sup>	3.4
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /Fe <sub>2</sub> O <sub>3</sub> , 1.00 g L <sup>-1</sup>	19.0
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /NiO, 1.00 g L <sup>-1</sup>	37.4
P-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /Fe <sub>2</sub> O <sub>3</sub> , 1.00 g L <sup>-1</sup>	16.6
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /S-metal oxides, 1.00 g L <sup>-1</sup>	17.4
M-Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /R-metal oxides, 1.00 g L <sup>-1</sup>	13.2
P25, 1.00 g L <sup>-1</sup>	95.4

Table S7 Degradation rates of the as-prepared Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/metal oxides.



**Fig. S6** Recycling photocatalytic degradations of MO over (a) M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/ZnO (1.00 g L<sup>-1</sup>), (b) M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/CuO (0.50 g L<sup>-1</sup>), (c) M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/Fe<sub>2</sub>O<sub>3</sub> (1.00 g L<sup>-1</sup>), (d) P-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/NiO (1.00 g L<sup>-1</sup>) under UV-vis light irradiation.



**Fig. S7** Photocatalytic degradation of MO over P25 (Degussa, specific surface area of  $50 \text{ m}^2 \text{ g}^{-1}$ ) (1.00 g L<sup>-1</sup>). The MO degradation rate of the commercial Degussa P25 titania is 95.4%, a little higher than that (91.5%) of M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/ZnO, while it is unable to reuse by magnetic recovery in the treated wastewater, and thus a certain advantage is displayed with the magnetite photocatalysts of the M-Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub>/metal oxides.

## References

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