

Rare earth element analysis in natural waters by multiple isotope dilution - sector field ICP-MS.

Tristan C. C. Rousseau,^{*a} Jeroen E. Sonke,^a Jerome Chmeleff,^a Frederic Candaudap,^a François Lacan,^b Geraldo Boaventura^c, Patrick Seyler^a and Catherine Jeandel^b.

*corresponding author: tristanrousseau@yahoo.fr

^a: GET, Université de Toulouse, CNRS, IRD, CNES, 14 Avenue Edouard Belin, F-31400 Toulouse, France, 14 Avenue Edouard Belin, F-31400 Toulouse, France

^b: LEGOS, Université de Toulouse, CNRS, IRD, CNES, 14 Avenue Edouard Belin, F-31400 Toulouse, France

^c: Universidade De Brasilia, UNB, LAGEQ, Campus universitario Darcy Ribeiro 70.910-900 Brasilia -DF -

Supplementary Information

Contents:

1. Spike calibration on MC-ICPMS.....	p.1
2. Optimum Spike/Sample mixing.....	p.5
3. Nobias pre-concentration protocol.....	p.7
4. Oxides and mass bias monitoring solutions.....	p.7
5. Desolvator-SF-ICPMS settings and performances.....	p.8
6. Isobaric corrections on ¹³⁸ La and ¹⁷⁶ Lu.....	p.10

1. Spike calibration on MC-ICPMS

Isotopically enriched REE spikes were originally obtained from Oak Ridge National Laboratory in the 1990's and dissolved and stored in 10% HNO₃ at 4°C. We calibrated these spike mother solutions for their concentration and isotopic composition (IC) in 2010 with a Thermo-Finingan Neptune MC-ICP-MS at the Midi-Pyrenees Observatory (Toulouse, France).

1.1. Cup configuration, mass bias and interferences corrections

MC-ICP-MS cup configurations

Five different MC-ICP-MS cup configurations were used for the 10 enriched REE spike calibrations (Table S1). La, Ce, Nd, Eu, Er and Lu were analyzed in static mode and Sm, Gd, Dy, Yb in dynamic mode in order to be able to measure all REE isotopes and isobaric interferences.

Table S1: A total of five MC-ICP-MS cup configurations were used to calibrate the single REE enriched spike mother solutions. Ratios used for exponential law mass bias correction and for reverse isotope dilution are indicated in the last two columns. Interfered isotopes are marked with a star, third isotopes used for isobaric corrections are marked with a circle note that ¹⁴²Nd could not be corrected for the minor isobaric interference ¹⁴²Ce.

	Main Cup Config.	L4	L3	L2	L1	C	H1	H2	H3	H4	Ratios used for Mass Biass Corection	Ratios used forReverse Isotope Dilution
La	1	¹³⁶ Ce	¹³⁷ Ba	¹³⁸ Ce*	¹³⁹ La	¹⁴⁰ Ce	¹⁴¹ Pr	¹⁴² Ce	¹⁴⁴ Nd	¹⁴⁷ Sm	¹⁴⁰ Ce/ ¹⁴² Ce*	¹³⁸ La/ ¹³⁹ La
Ce	1	¹³⁶ Ce*	¹³⁷ Ba ^o	¹³⁸ Ce*	¹³⁹ La	¹⁴⁰ Ce	¹⁴¹ Pr	¹⁴² Ce	¹⁴⁴ Nd ^o	¹⁴⁷ Sm	¹⁴⁰ Ce/ ¹⁴² Ce*	¹³⁶ Ce/ ¹⁴⁰ Ce
Nd	1	¹⁴² Nd*	¹⁴³ Nd*	¹⁴⁴ Nd*	¹⁴⁵ Nd	¹⁴⁶ Nd	¹⁴⁷ Sm ^o	¹⁴⁸ Nd*	¹⁵⁰ Nd*		¹⁴⁵ Nd/ ¹⁴³ Nd	¹⁴⁶ Nd/ ¹⁴⁵ Nd
Sm Mode1	2	¹⁴⁴ Sm	¹⁴⁵ Nd	¹⁴⁶ Nd ^o	¹⁴⁷ Sm	¹⁴⁸ Sm*	¹⁴⁹ Sm	¹⁵⁰ Sm*	¹⁵² Sm*	¹⁵⁵ Gd	¹⁴⁷ Sm/ ¹⁴⁹ Sm	
Sm Mode2	2	¹⁴⁹ Sm	¹⁵⁰ Sm*	¹⁵¹ Eu	¹⁵² Sm*	¹⁵³ Eu	¹⁵⁴ Sm*	¹⁵⁵ Gd ^o	¹⁵⁷ Gd	¹⁶⁰ Gd	¹⁵² Sm/ ¹⁴⁹ Sm	¹⁴⁷ Sm/ ¹⁴⁹ Sm
Eu	2	¹⁴⁹ Sm	¹⁵⁰ Sm	¹⁵¹ Eu	¹⁵² Sm	¹⁵³ Eu	¹⁵⁴ Sm	¹⁵⁵ Gd	¹⁵⁷ Gd	¹⁶⁰ Gd	¹⁵¹ Eu/ ¹⁵³ Eu	¹⁵¹ Eu/ ¹⁵³ Eu
Gd Mode1	2	¹⁴⁹ Sm ^o	¹⁵⁰ Sm	¹⁵¹ Eu	¹⁵² Gd*	¹⁵³ Eu	¹⁵⁴ Gd*	¹⁵⁵ Gd ^o	¹⁵⁷ Gd	¹⁶⁰ Gd ^o	¹⁵⁵ Gd/ ¹⁵⁷ Gd	
Gd Mode2	2	¹⁵² Gd	¹⁵³ Eu	¹⁵⁴ Gd	¹⁵⁵ Gd	¹⁵⁶ Gd*	¹⁵⁷ Gd	¹⁵⁸ Gd*	¹⁶⁰ Gd*	¹⁶³ Dy ^o	¹⁵⁵ Gd/ ¹⁵⁷ Gd	¹⁵⁵ Gd/ ¹⁵⁷ Gd
Dy Mode1	3	¹⁵⁵ Dy	¹⁵⁶ Gd*	¹⁵⁷ Gd	¹⁵⁸ Dy*	¹⁵⁹ Tb	¹⁶⁰ Dy*	¹⁶¹ Dy	¹⁶³ Dy	¹⁶⁶ Er	¹⁶³ Dy/ ¹⁶¹ Dy	
Dy Mode2	3	¹⁵⁶ Dy*	¹⁵⁷ Gd ^o	¹⁵⁸ Dy*	¹⁵⁹ Tb	¹⁶⁰ Gd*	¹⁶¹ Dy	¹⁶² Dy*	¹⁶⁴ Dy	¹⁶⁷ Er ^o	¹⁶² Dy*/ ¹⁶¹ Dy	¹⁶³ Dy/ ¹⁶¹ Dy
Er	4	¹⁶² Er*	¹⁶³ Dy ^o	¹⁶⁴ Er*	¹⁶⁵ Ho	¹⁶⁶ Er	¹⁶⁷ Er	¹⁶⁸ Er*	¹⁷⁰ Er*	¹⁷³ Yb ^o	¹⁶⁶ Er/ ¹⁶⁷ Er	¹⁶⁶ Er/ ¹⁶⁷ Er
Yb Mode1	5	¹⁶⁷ Er ^o	¹⁶⁸ Er*	¹⁶⁹ Tm	¹⁷⁰ Er*	¹⁷¹ Yb	¹⁷² Yb	¹⁷³ Yb	¹⁷⁵ Lu	¹⁷⁸ Hf	¹⁷³ Yb/ ¹⁷² Yb	
Yb Mode2	5	¹⁶⁸ Yb	¹⁶⁹ Tm	¹⁷⁰ Yb ^o	¹⁷¹ Yb	¹⁷² Yb	¹⁷³ Yb	¹⁷⁴ Yb*	¹⁷⁶ Yb*	¹⁷⁹ Hf ^o	¹⁷³ Yb/ ¹⁷² Yb	¹⁷² Yb/ ¹⁷¹ Yb
Lu	5	¹⁷¹ Yb	¹⁷² Yb	¹⁷³ Yb ^o	¹⁷⁴ Yb	¹⁷⁵ Lu	¹⁷⁶ Lu*	¹⁷⁷ Hf ^o	¹⁷⁹ Hf	¹⁸² W	¹⁷⁵ Lu/ ¹⁷⁶ Lu*	¹⁷⁵ Lu/ ¹⁷⁶ Lu*

Instrumental mass bias

The MC-ICP-MS discriminates against the transmission of light isotopes relative to heavy isotopes. This is called mass bias, and requires to be corrected for. We did so by bracketing the pure spike and mixed spike/JMC solutions with natural abundance REE solutions. Since mass bias is concentration dependent, the REE bracketing solution had approximately the same concentrations (within 10%) as the pure spike and mixed spike/JMC solutions. Fractionation factors, *f*, were calculating using the exponential mass fractionation law:

$$f = \frac{\ln\left(\frac{r_{1/2}}{R_{1/2}}\right)}{\ln\left(\frac{M_1}{M_2}\right)} \quad (\text{Eq.S1})$$

$R_{1/2}$: true ratio of relative abundances between isotopes 1 et 2

$r_{1/2}$: measured ratio in Volts between isotope 1 and 2

M_1 : atomic mass of isotope 1

M_2 : atomic mass of isotope 2

The ratios measured in the bracketed spike or mixed spike/JMC solutions are corrected using interpolated 'f' values from bracketing solutions.

$$r_{\text{cor}} = \frac{r_{\text{mes}}}{\left(\frac{M_1}{M_2}\right)^f} \quad (\text{Eq.S2})$$

r_{mes} : Ratio between isotope 1 and 2 measured in the spike or JMC/spike mixed solutions

r_{cor} : Corrected Ratio between isotope 1 and 2

Isobaric Interference corrections

Isobaric interference corrections were made by subtracting the signal of an interference free isotope of the isobaric interfering one divided by its abundance multiplied by the interfering isotope abundance:

$$V_{1\text{corr}} = V_{1\text{mes}} - \frac{V_{3\text{mes}}}{A_3} * A_1 \quad (\text{Eq.S3})$$

As there is also a mass bias between isotopes 1 and 3, it was taken into account using equations S1 and S2.

$$V_{1\text{corr}} = V_{1\text{mes}} - \left(\frac{M_1}{M_3} * \left(\frac{A_1}{A_3}\right)^f\right) * V_3 \quad (\text{Eq.S4})$$

When the interfered isotope was necessary for mass bias calculation, the interfering isotope contribution was calculated iteratively, applying first a non-mass bias corrected isobaric interference correction. This allowed to calculate a first fractionation factor used to recalculate the interfering signal with Eq. S4 to finally calculate a more precise fractionation factor.

1.2. Enriched REE spike calibration

The relative abundances of REE isotopes in the enriched REE spike mother solutions were calculated as follows:

$$A^X_M = \frac{1}{\left(\frac{\sum(A^Y_M)}{A^X_M} + 1\right)} \quad (\text{Eq.S5})$$

A^X_M : Relative abundance for the isotope X of element M

A^Y_M : Relative abundances for the isotopes Y of the element M, excluding X

,as illustrated for Nd:

$$A^{142}\text{Nd} + A^{143}\text{Nd} + A^{144}\text{Nd} + A^{145}\text{Nd} + A^{147}\text{Nd} + A^{148}\text{Nd} + A^{150}\text{Nd} = 1 \quad (\text{Eq.S6})$$

Dividing all terms by A^{143}_{Nd} and rearranging:

$$A^{143}Nd = \frac{1}{\left(\frac{\sum(A^yNd)}{A^{143}Nd} + 1\right)} \quad (\text{Eq.S7})$$

Abundance ratios in equation S7 were then substituted by the signal ratios in volts measured by MC-ICP-MS after blank, interference and mass bias corrections.

$$\hat{A}^{143}Nd = \frac{1}{\left(\frac{\sum(V^yNd)}{V^{143}Nd} + 1\right)} \quad (\text{Eq.S8})$$

\hat{A}^{143}_{Nd} : calculated abundance for ^{143}Nd in the spike

V^y_{Nd} : Signal in volts for the Y's atomic masses of the element M measured by MC-ICP-MS

All Nd isotope abundances in the spike could then be deduced, for ex. for ^{142}Nd :

$$\hat{A}^{142}Nd = \hat{A}^{143}Nd * \frac{V^{142}Nd}{V^{143}Nd} \quad (\text{Eq.S9})$$

The spike's atomic masses were then determined using the measured relative abundances of isotopes in the spike and individual isotope atomic masses from:

NIST (<http://www.nist.gov/pml/data/comp.cfm/>)

$$MNd_{Spk} = \sum(\hat{A}^x_{Nd} * M^x_{Nd}) \quad (\text{Eq.S10})$$

MNd_{Spk} : Nd's Spike atomic mass calibrated with MC-ICP-MS

M^x_{Nd} : NIST isotope mass for the isotopes 'x'

Concentrations were determined by reverse isotope dilution (RID), which is achieved by mixing a commercial mono-elementary REE solution, with isotopes of natural relative abundances, with the corresponding enriched REE mother spike solution. We used commercial 1000 mg.kg⁻¹ single REE solutions from the Johnson Matthey Company (JMC) that have a certified uncertainty of 0.3% RSD.

RID isotope pairs were chosen according to the relative abundances and the absence of isobaric interferences, when possible. The RID formula can be written as:

$$[REE]_{spk} = [REE]_{jmc} * \frac{\frac{W_{jmc}}{W_{spk}}}{\left(\frac{R_{spk} - R_m}{R_m - R_{nat}} * \frac{A_{2spk}}{A_{2nat}} * \frac{M_{nat}}{M_{spk}}\right)} \quad (\text{Eq.S11})$$

W_{jmc} : Mass in g of certified JMR REE solution mixed with the spike

W_{spk} : Mass in g of the spike solution

R_{spk} : Ratio of A_1/A_2 in the spike (determined during the IC calibration)

R_{nat} : Ratio of natural A_1/A_2

R_m : Corrected ratio of V_1/V_2 in the mixed solution measured by MC-ICP-MS

2. Optimum Spike/Sample mixing

The optimum spike to natural REE isotope ratios was determined for each REE using the uncertainty magnification factor formula:

$$M = \frac{(R_{\text{nat}} - R_{\text{spk}}) * R_{\text{mix}}}{(R_{\text{mix}} - R_{\text{nat}}) * (R_{\text{spk}} - R_{\text{mix}})} \quad (\text{Eq.S12})$$

R_{nat} and R_{spk} being constant, the function $M=f(R_{\text{mix}})$ has an uncertainty minimum for:

$$\frac{dM}{dR_{\text{mix}}} = 0 \quad (\text{Eq.S13})$$

The solution to Eq.S13 can be formulated for $R_{\text{mix}} = R_{\text{mix}_{ideal}}$ and corresponds to the ideal amount of spike/natural REE mixing:

$$R_{\text{mix}_{ideal}} = \sqrt{R_{\text{spk}} * R_{\text{nat}}} \quad (\text{Eq.S14})$$

Figure S1 illustrates the mixing between natural Nd and enriched ^{146}Nd spike for the ratio $^{146}\text{Nd}/^{145}\text{Nd}$. The value for M decreases between the R_{nat} (2.07) and the $R_{\text{mix}_{ideal}}$ (19.63) corresponding to the underspiking zone and increases between $R_{\text{mix}_{ideal}}$ and R_{spk} (186.4) corresponding to the overspiking zone.

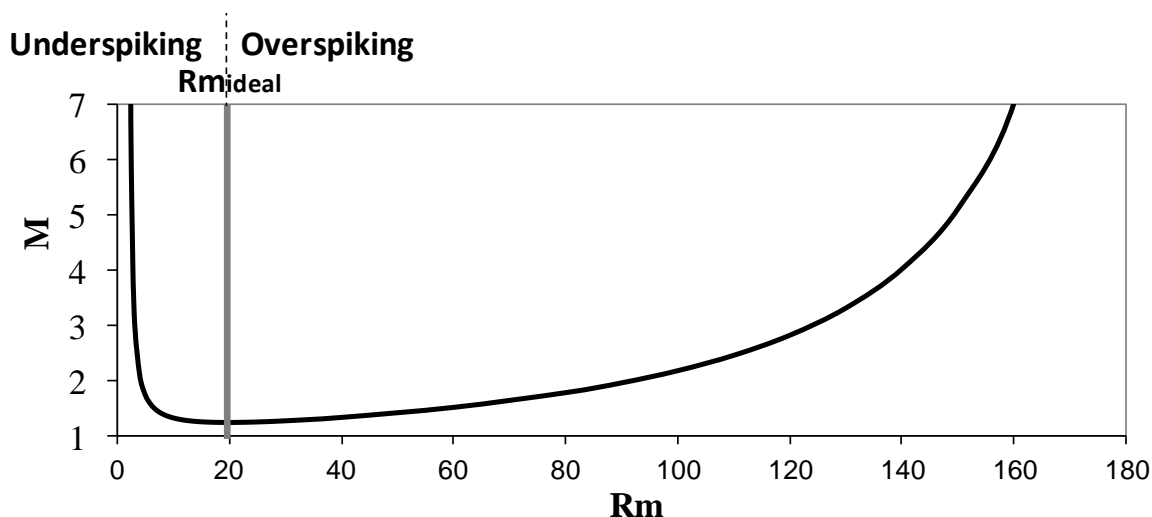


Figure S1: Uncertainty magnification factor 'M' as a function of the $^{146}\text{Nd}/^{145}\text{Nd}$ mixing ratio used for Nd isotope dilution.

In practice, the ideal amount of isotopic spikes were approximated using the reverse isotope dilution equation (Eq.S11) for a given sample [REE] and replacing R_m by $R_{\text{mix}_{ideal}}$. One difficulty is that added spike isotopes may themselves generate molecular and isobaric interferences. Therefore, simulations of ideally spiked samples were made numerically considering several plausible levels of plasma oxide and hydroxyde formation in order to

evaluate the magnitude of oxihydroxide interferences (ie: Ba and LREE on MREE and MREE on HREE) and isobaric interferences (ie: Ba, La, Ce and Yb, Lu, Hf).

After this optimization to limit isobaric and oxide interferences, a stock of mixed LREE spike and mixed HREE spike solutions was prepared. These stock solutions contain respectively 51ppb for La, 15ppb for Ce, 113 ppb for Nd, 48 ppb for Sm, 18 ppb for Eu and 92 ppb for Gd (mixed spike LREE) and 116 ppb for Dy, 65 ppb for Er, 41 ppb for Yb and 17 ppb for Lu (mixed spike HREE). Dilutions of those mother solutions were made to achieve 200ul to 1ml of spike aliquots when spiking samples. A SF-ICPMS mass spectrum of both HREE and LREE mixed spike solutions is reported in Figure S2.

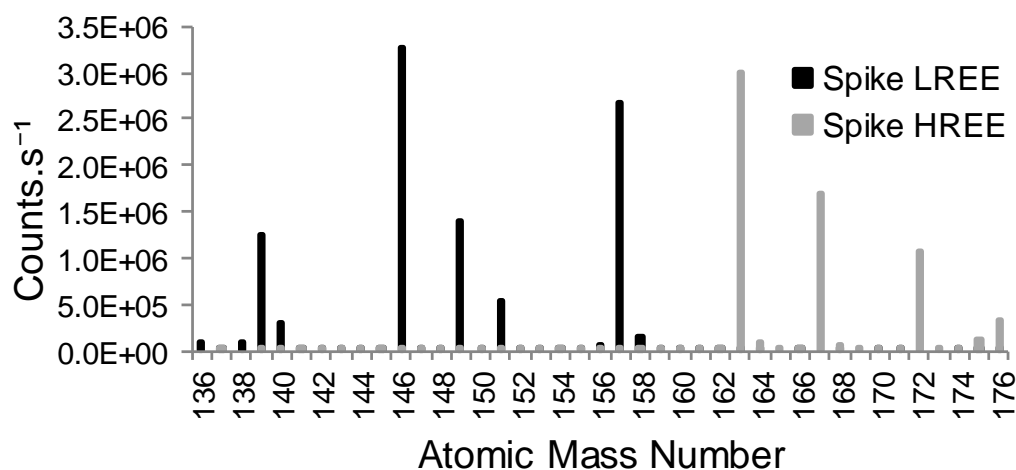


Figure S2: HREE (black) and LREE (grey) mixed spike mass spectrum measured with Thermo Element-XR coupled with the Aridus 2 desolvator.

The average dispersion of the uncertainty magnification factor 'M' obtained on the 19 samples analyzed in this study are reported in Figure S3. The grey line represents for each element the theoretical uncertainty magnification factor corresponding to an ideal proportion of sample/spike mixing and the boxplots represent the observed uncertainty magnification factor. Except for La and Lu which are overspiked on purpose all isotope/sample mixing proportions were close to ideal.

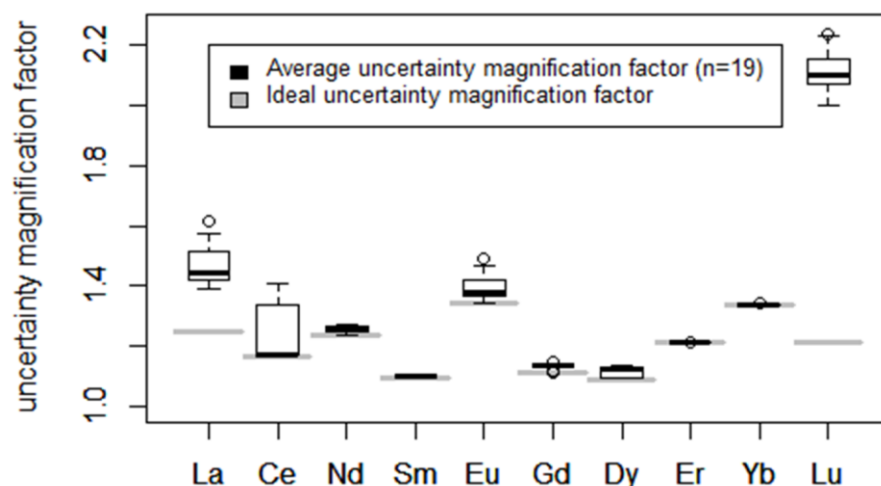


Figure S3: REE isotope dilution 'M' uncertainty magnification factors based on 19 samples spiked in this study (Boxplots) relative to the minimum theoretical uncertainty level achievable (grey lines).

3. Nobias pre-concentration protocol

The Nobias pre-concentration setup is displayed in Figure S4, rigid Teflon tubing is used to pump wash, samples and elution solutions reducing contamination risks between different samples. During washing and pre-concentration, waste are pumped via a Tygon tube connected at the bottom of the Nobias column through the same peristaltic pump in a parallel channel ensuring equal fluxes of $10\text{ml}\cdot\text{min}^{-1}$ in and out of the column.

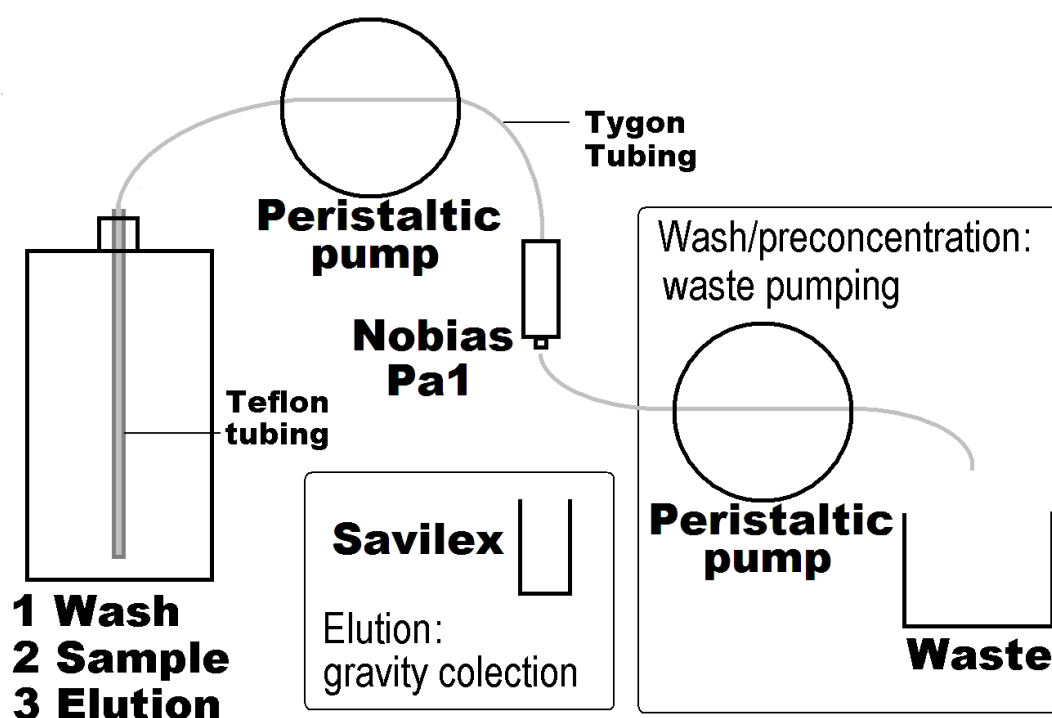


Figure S4: Nobias preconcentration setup

4. Oxides and mass bias monitoring solutions

The monitoring of Ba and REE oxides production were made analyzing two in house bracketing synthetic solutions of natural isotopic abundances (JMC solutions). One contains elements Ba, La, Ce, Pr, Tb and Er and the other Nd, Sm, Eu, Gd, Dy and Yb.

For La Ce and Lu mass bias fractionation factors were monitored by the analysis of bracketing mixed spike solutions. For other REE and Ba, mass bias was monitored with the two bracketing solutions Figure S5.

	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145
Ba	0		0		2	7	8	11	72							
La									0.1	99.9						
Ce							0		0		88		11			
Pr												100				
Nd													27	12	24	8
Sm															3	
	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161
Nd	17		6		6											
Sm		15	11	14	7		27		23							
Eu						48		52								
Gd							0		2	15	20	16	25			22
Tb																
Dy														100		
	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177
Dy	25	25	28													
Ho																
Er	0		2		34	23	27		15							
Tm																
Yb							0		3	14	22	16	32		13	
Lu																

Figure S5: Two external bracketing solutions were used to monitor oxides formation and mass bias during a SF-ICP-MS session. The first solution contained Ba, La, Ce, Pr, Tb, Er (dark grey). The second solution contained Nd, Sm, Eu, Gd, Dy and Yb (light grey). Arrows point towards the monitored interfered masses, framed isotopes were used for mass bias monitoring.

5. Desolvator-SF-ICPMS settings and performances

5.1 Comparative test of two desolvator introduction systems

Ba and REE oxides formation were compared with two desolvation systems: the APEX-Q (ESI Inc.) with no N₂ additional gas and the Aridus II (Cetac Inc.) with N₂ as additional gas. The same monitoring solutions (ie: Ba, La, Ce, Pr, Tb, Er and Nd, Sm, Eu, Gd, Dy) were analyzed with both systems and displayed low oxides formation levels and a decreasing trend across the lanthanide serie with exception for Gd and Dy Figure S6. The best results were achieved with the Aridus II kept for the multispike method. The oxide formation levels presented here with this desolvation system corresponds to tuned values for UO/U of 0.02%.

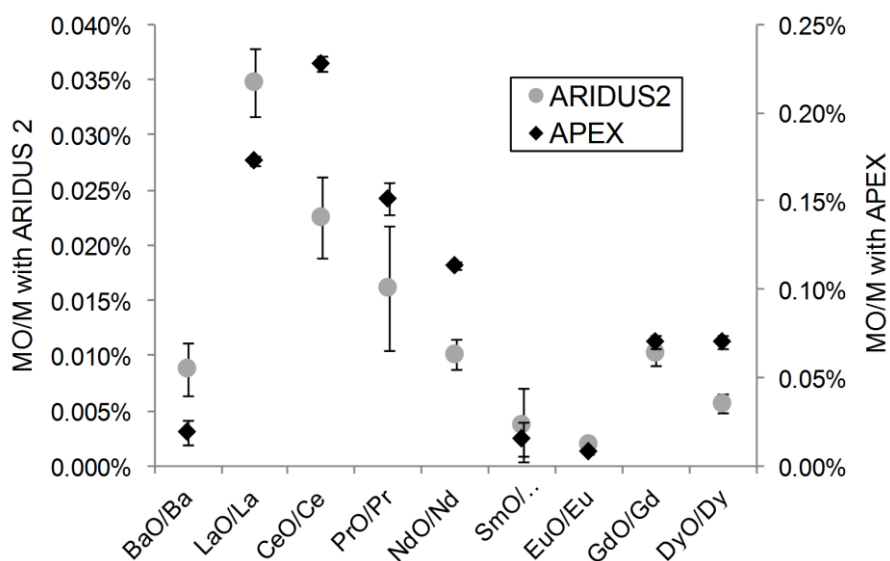


Figure S6: REE oxides formation in the Thermo Element XR ICPMS; comparison between ARIDUS 2 and APEX desolvating systems.

5.2 Comparative test of two data acquisition methods

For the multispike method we aimed in achieving the best precision on isotopic ratios. With traditional acquisition methods made of long measurements high precision are achieved on ion counting per masses, however small variations of the sample flow in the introduction system can lead to an increasing of RSD on isotope ratios measurements. As listed in Table S2, the 60 consecutive sweeps method displayed higher average RSD on individual measurements but lower 2RSD on isotopic ratios than a method constituted of 3 blocks of 3 long measurements.

Table S2: Comparison of standard deviation behavior on 5 replicate of single isotope analysis and isotopic ratios analysis for two different acquisition methods of same duration (n=5).

Acquisition method	¹⁴³ Nd	¹⁴⁶ Nd	143/146	¹⁵¹ Eu	¹⁵³ Eu	151/153	¹⁷² Yb	¹⁷³ Yb	173/172
	average RSD	average RSD	2RSD ΔAmu=3	average RSD	average RSD	2RSD ΔAmu=2	average RSD	average RSD	2RSD ΔAmu=1
3*3 long meas.	1.6%	0.9%	0.61%	1.2%	0.8%	0.71%	0.9%	1.1%	0.72%
1*60 short meas.	1.7%	1.6%	0.28%	1.6%	1.5%	0.31%	2.1%	2.2%	0.31%

5.3 Desolvator-SF-ICPMS setup and configuration

The Table S3 lists the set up used for the multispike method, a wash time of 120s and a take up time of 90s allows the appropriate drop in the precedent sample inward and stabilization of the next sample signal.

Table S3: Instrument parameters

<i>ICP system</i>		<i>Mass spectrometer</i>	
RF power, W	1200	Sampler	Nickel, orifice 1.0 mm
Coolant argon flow rate, L min ⁻¹	16	Skimmer Nickel,	orifice 0.7 mm
Auxiliary gas flow rate L min	1	Torch position	X=4.90 Y=3.9 Z=-1.6
Nebulizer gas flow rate L min	1.2	Extraction, V	-2000
		Focus, V	-1200
		X-deflection, V	2.5
<i>Sample introduction</i>		<i>Data acquisition</i>	
Sampler		Mass range, amu	129-178
Peristaltic pump	3rpm	Dwell time/mass, ms	0.04-0.4
Nebulizer	GE Micromist TL 100μl	peaks/mass	4
Sample uptake rate, μl.min ⁻¹	260	Number of scans	60
Rinse time, min	4	Total acquisition time	6min
Uptake time, s	120		
<i>Desolvation-system</i>			
Desolvation-system	Aridus 2, membrane desolvation (CETAC)		
Spray chamber temperature, °C	110		
Membrane temperature, °C	160		
Ar sweep gas l.min ⁻¹	5.99		
N ₂ desolvation gas	12		

6. Mass bias Monitoring

The average and standard deviation of 7 replicates of the measured/natural isotopic ratios of 8 elements monitored measured over the course of one analytical session are reported in Table S4. Details of the trends of 4 elements are represented in Figure S7. A comparison of using session averaged mass bias factors or interpolating evolutive mass bias factors shows that the final concentration results are within 0.1%.

Table S4: Average and standard deviation of the measured/natural isotopic ratios of the mass bias monitoring solution during one analytical session (n=7).

	¹⁴² Ce/ ¹⁴⁰ Ce	¹⁴⁶ Nd/ ¹⁴⁵ Nd	¹⁴⁹ Sm/ Sm147	¹⁵³ Eu/ ¹⁵¹ Eu	¹⁵⁷ Gd/ ¹⁵⁵ Gd	Dy163/ ¹⁶¹ Dy	Er167/ ¹⁶⁶ Er	¹⁷² Yb/ ¹⁷³ Yb
Rmes/ Rnat	1.009	1.013	1.007	1.014	1.008	1.009	1.001	1.011
Sd	0.002	0.002	0.004	0.004	0.001	0.003	0.003	0.007

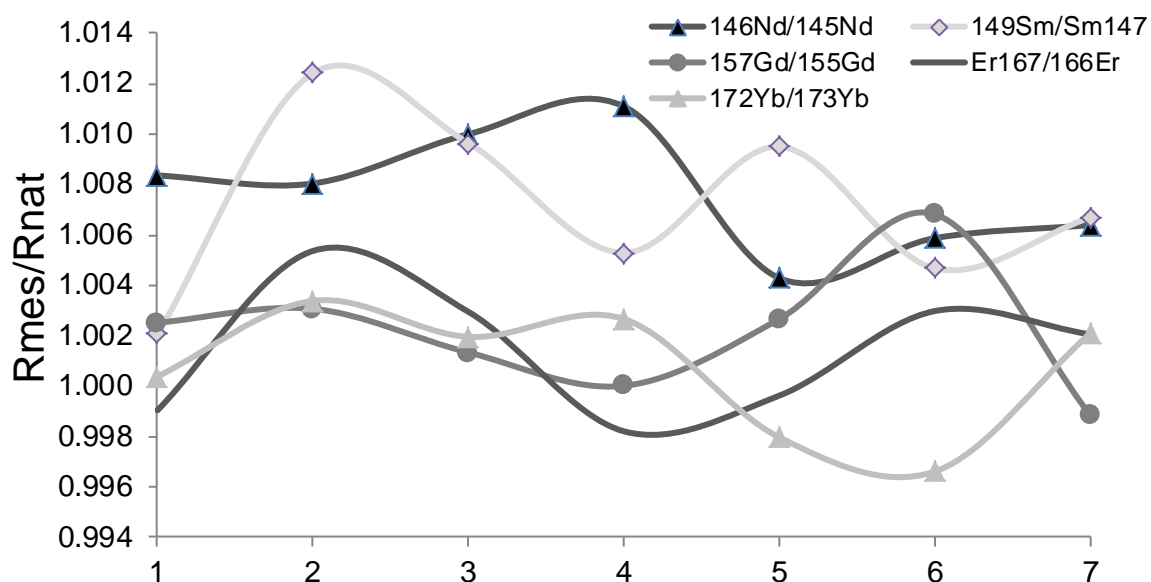


Figure S7: Mass bias evolution of Nd, Sm, Gd, Er, and Yb during one analytical session

7. Isobaric corrections on ¹³⁸La and ¹⁷⁶Lu

The linear relation between ¹³⁸Ce/¹⁴⁰Ce vs ¹³⁶Ce/¹⁴⁰Ce and ¹⁷⁶Yb/¹⁷²Yb vs ¹⁷²Yb/¹⁷¹Yb is reported on Figure S8 and allows to subtract ¹³⁸Ce and ¹⁷⁶Yb interfering on La and Lu for any spike/sample proportion. The isobaric interference calculation is corrected for mass bias fractionation combining Eq 15 and 16 with Eq 17. (Eq. S15 and S16)

$$\text{Cps}^{138}\text{La} = \text{Cps}^{138} - \frac{\text{Cps}^{137}\text{Ba}}{\text{A}^{137}\text{Ba}} * \frac{\text{A}^{138}\text{Ba}}{f_{138/137}} - \left(\frac{\text{Cps}^{136}\text{Ce} * 0.0305}{f_{136/140}} + 0.0028 * \text{Cps}^{140}\text{Ce} \right) * f_{138/140} \text{ (Eq.S15)}$$

$$\text{Cps}^{176}\text{Lu} = \text{Cps}^{176} - \frac{\text{Cps}^{177}\text{Hf}}{\text{A}^{177}\text{Hf}} * \frac{\text{A}^{176}\text{Hf}}{f_{176/177}} - \left(\frac{\text{Cps}^{171}\text{Yb} * 0.909}{f_{171/172}} + 0.0101 * \text{Cps}^{172}\text{Yb} \right) * f_{176/172} \text{ (Eq.S16)}$$

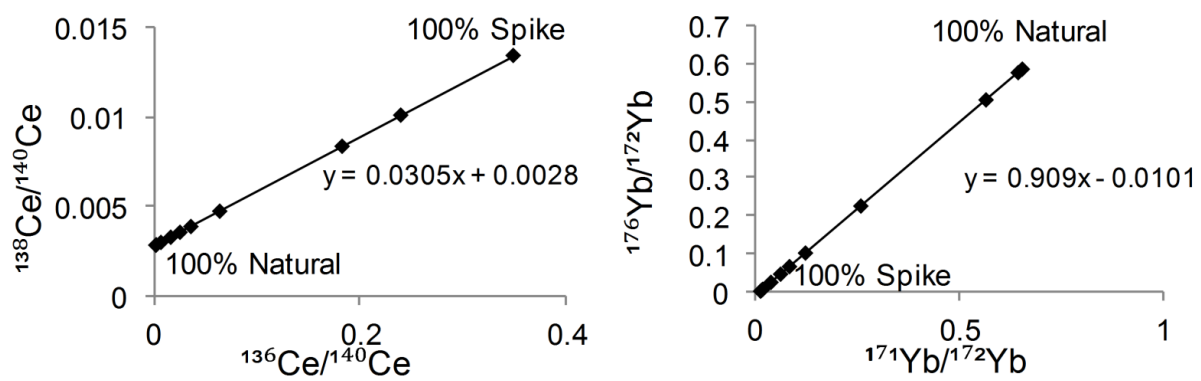


Figure S8: Isotope ratios of Ce and Yb for different proportions of spike/sample mixing.