

Figure SI 1. Experimental (red points), calculated (black solid line) and their difference (blue line at bottom) XRD patterns for $\text{Sr}_2\text{EuNb}_{1-x}\text{Ti}_x\text{O}_{6-x/2}$ with $x=0.25$; the vertical bars indicate the positions of Bragg peaks for this phase (upper bars) and for $\text{Sr}_3\text{Ti}_2\text{O}_7$ (lower bars). In the zoomed region weak peaks of an unidentified impurity phase are indicated by asterisks.

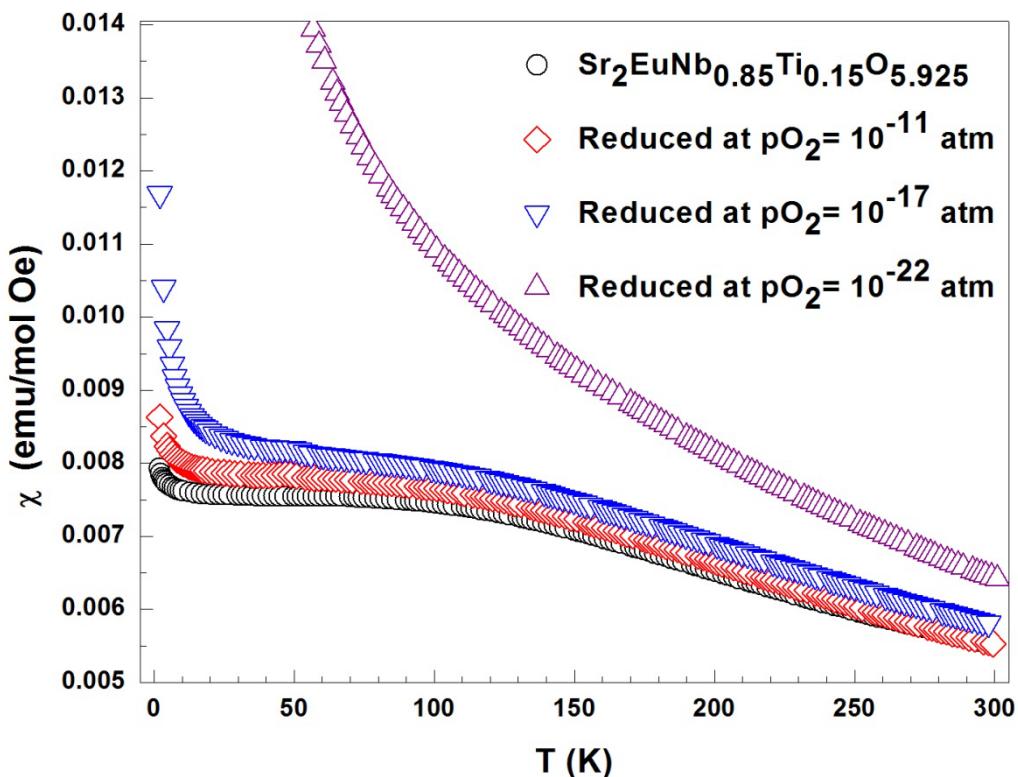


Figure SI 2. Magnetic susceptibility as a function of temperature for as-prepared $\text{Sr}_2\text{EuNb}_{0.85}\text{Ti}_{0.15}\text{O}_{5.925}$ and samples reduced under different $p\text{O}_2$ conditions. As the $p\text{O}_2$ decreases the magnetic susceptibility increases due to the consequent higher Eu^{2+} content in the material.

Table SI 1: Structural parameters for $\text{Sr}_2\text{EuNb}_{1-x}\text{Ti}_x\text{O}_{6-x/2}$ ($0 \leq x \leq 0.20$) compounds obtained from XRD.

	^a $\text{Sr}_2\text{EuNbO}_6$	^b $\text{Sr}_2\text{EuNb}_{0.95}\text{Ti}_{0.05}\text{O}_6$	^c $\text{Sr}_2\text{EuNb}_{0.90}\text{Ti}_{0.10}\text{O}_6$	^d $\text{Sr}_2\text{EuNb}_{0.85}\text{Ti}_{0.15}\text{O}_6$	^e $\text{Sr}_2\text{EuNb}_{0.80}\text{Ti}_{0.20}\text{O}_6$
a (Å)	5.8438(2)	5.84134(5)	5.8385(3)	5.8383(4)	5.8393(1)
b (Å)	5.9255(2)	5.91717(5)	5.9028(3)	5.8973(4)	5.8920(1)
c (Å)	8.3072(3)	8.30257(7)	8.2956(5)	8.2895(5)	8.2873(1)
β (deg)	90.216(2)	90.204(1)	90.198(4)	90.193(4)	90.183(1)
Sr position	4e	4e	4e	4e	4e
Occ Sr	1.00	1.00	1.00	1.00	1.00
x	-0.005(2)	-0.005(1)	-0.002(3)	-0.002(3)	0.007(2)
y	0.4654(6)	0.4657(4)	0.4701(6)	0.4712(8)	0.4736(6)
z	0.2521(9)	0.2507(7)	0.251(1)	0.253(1)	0.249(1)
U^{*100} (Å²)	0.70(2)	0.21(2)	0.62(3)	0.76(4)	0.58(3)
Nb/Ti position	2b	2b	2b	2b	2b
Occ Nb/Ti	0.50/0.00	0.473(4)/0.027(4)	0.459(6)/0.041(6)	0.432(5)/0.068(5)	0.420(4)/0.080(4)
U^{*100} (Å²)	0.62(4)	0.35(3)	0.71(4)	0.68(5)	0.36(3)
Eu position	2a	2a	2a	2a	2a
Occ Eu	0.50	0.50	0.50	0.50	0.50
U^{*100} (Å²)	0.76(4)	0.28(3)	0.68(3)	0.73(4)	0.62(4)
O(1) position	4e	4e	4e	4e	4e
x	0.075(4)	0.095(3)	0.093(5)	0.131(6)	0.104(5)
y	0.0378(4)	0.025(3)	0.036(5)	0.070(5)	0.037(6)
z	0.261(4)	0.260(3)	0.269(7)	0.261(7)	0.294(6)
Occ	1.00	1.00	1.00	1.00	1.00
U^{*100} (Å²)	0.76(3)	0.53(3)	0.82(5)	0.84(4)	0.72(4)
O(2) position	4e	4e	4e	4e	4e
x	0.235(6)	0.231(4)	0.236(7)	0.325(7)	0.222(5)
y	0.308(5)	0.312(3)	0.303(7)	0.308(7)	0.314(6)
z	-0.034(5)	-0.035(4)	0.021(6)	0.024(6)	-0.033(5)
Occ	1.00	1.00	1.00	1.00	1.00
U^{*100} (Å²)	0.76(3)	0.53(3)	0.82(5)	0.84(4)	0.72(4)
O(3) position	4e	4e	4e	4e	4e
x	0.293(5)	0.291(4)	0.286(5)	0.245(7)	0.308(6)
y	0.757(5)	0.776(4)	0.773(6)	0.747(8)	0.793(6)
z	-0.063(4)	-0.044(4)	-0.084(5)	-0.057(5)	-0.061(6)
Occ	1.00	1.00	1.00	1.00	1.00
U^{*100} (Å²)	0.76(3)	0.53(3)	0.82(5)	0.84(4)	0.72(4)

Space Group: P2₁/n (#14): 2a(000), 2b (00½), 4e (xyz),

^a $\chi^2 = 1.08$, $R_{wp} = 5.14\%$, $R_{exp} = 4.96\%$, $R_B = 3.10\%$, Composition: $\text{Sr}_2\text{EuNbTiO}_6$

^b $\chi^2 = 1.47$, $R_{wp} = 4.49\%$, $R_{exp} = 3.70\%$, $R_B = 5.10\%$, Composition: $\text{Sr}_2\text{EuNb}_{0.95(2)}\text{Ti}_{0.05(2)}\text{O}_6$

^c $\chi^2 = 1.11$, $R_{wp} = 6.33\%$, $R_{exp} = 6.01\%$, $R_B = 5.57\%$, Composition: $\text{Sr}_2\text{EuNb}_{0.92(2)}\text{Ti}_{0.08(2)}\text{O}_6$

^d $\chi^2 = 1.18$, $R_{wp} = 6.17\%$, $R_{exp} = 5.71\%$, $R_B = 5.68\%$, Composition: $\text{Sr}_2\text{EuNb}_{0.86(2)}\text{Ti}_{0.14(2)}\text{O}_6$

^e $\chi^2 = 1.42$, $R_{wp} = 5.82\%$, $R_{exp} = 4.88\%$, $R_B = 8.52\%$, Composition: $\text{Sr}_2\text{EuNb}_{0.84(2)}\text{Ti}_{0.16(2)}\text{O}_6$. Some $\text{Sr}_3\text{Ti}_2\text{O}_7$ is also present.

Table SI 2: Selected structural information for as prepared $\text{Sr}_2\text{EuNb}_{1-x}\text{Ti}_x\text{O}_6$ ($0 \leq x \leq 0.15$)

	$\text{Sr}_2\text{EuNbO}_6$	$\text{Sr}_2\text{EuNb}_{0.95}\text{Ti}_{0.05}\text{O}_6$	$\text{Sr}_2\text{EuNb}_{0.90}\text{Ti}_{0.10}\text{O}_6$	$\text{Sr}_2\text{EuNb}_{0.85}\text{Ti}_{0.15}\text{O}_6$
^a Tilt angle θ	16.5(6)	12.5(5)	13.8(6)	14.7(6)
^b Tilt angle ϕ	13.5(5)	12.2(5)	11.2(5)	11.5(6)
^c Tilt angle μ	12.2(5)	15.5(6)	15.1(5)	22.0(6)
Tolerance factor	0.9156	0.9160	0.9164	0.9168
^d $\text{B}'\text{-O}(1) \times 2$	2.09(2)	2.08(2)	2.05(2)	2.13(2)
$\text{B}'\text{-O}(2) \times 2$	1.96(2)	1.95(2)	1.97(2)	1.83(2)
$\text{B}'\text{-O}(3) \times 2$	2.00(2)	2.07(2)	2.01(2)	1.93(2)
Average $\text{B}'\text{-O}$	2.02(1)	2.03(1)	2.01(1)	1.96(1)
^d $\text{B}''\text{-O}(1) \times 2$	2.16(2)	2.23(2)	2.25(2)	2.33(2)
$\text{B}''\text{-O}(2) \times 2$	2.32(2)	2.31(2)	2.26(2)	2.40(2)
$\text{B}''\text{-O}(3) \times 2$	2.34(2)	2.19(2)	2.27(2)	2.36(2)
Average $\text{B}''\text{-O}$	2.27(1)	2.24(1)	2.26(1)	2.36(1)

^a $\text{B}' = \text{Nb/Ti}$, $\text{B}'' = \text{Eu}$

^b With [110]; $\theta = \frac{1}{2} [\text{180-angle} < \text{B}'\text{-O}(3)\text{-B}'' >]$

^c With [1-10]; $\phi = \frac{1}{2} [\text{180-angle} < \text{B}'\text{-O}(2)\text{-B}'' >]$

^d With [001]; $\mu = \frac{1}{2} [\text{180-angle} < \text{B}'\text{-O}(1)\text{-B}'' >]$