

Supplementary Material of Manuscript

Continuous Separation of Microparticles in a Microfluidic Channel via the Elasto-inertial Effect of Non-Newtonian Fluid

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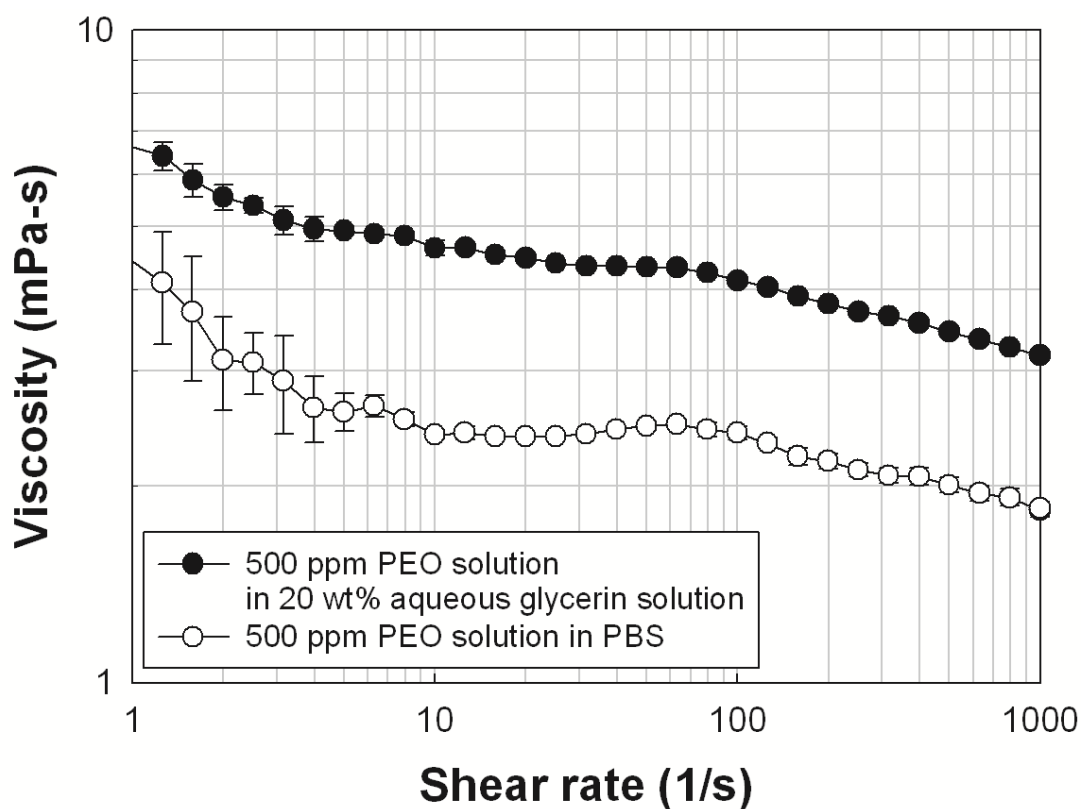


Fig. S-1 Viscosities of non-Newtonian fluids. Rheological measurements of viscosities were done using a controlled shear stress rheometer (AR2000, TA instruments) with a double gap Couette cell and a pressure-driven viscometer (Rheoscan-D 200, Rheomeditech, Korea) at shear rates of $1 < \dot{\gamma} < 10^3 \text{ s}^{-1}$. Since aqueous PEO solutions (500 ppm) in two solvents showed a typical shear-thinning viscosity, the mean viscosity as characteristic viscosity is dependent on shear rate. Mean viscosity can be defined at an average shear rate ($\dot{\gamma}_c = 2Q/hw^2$).

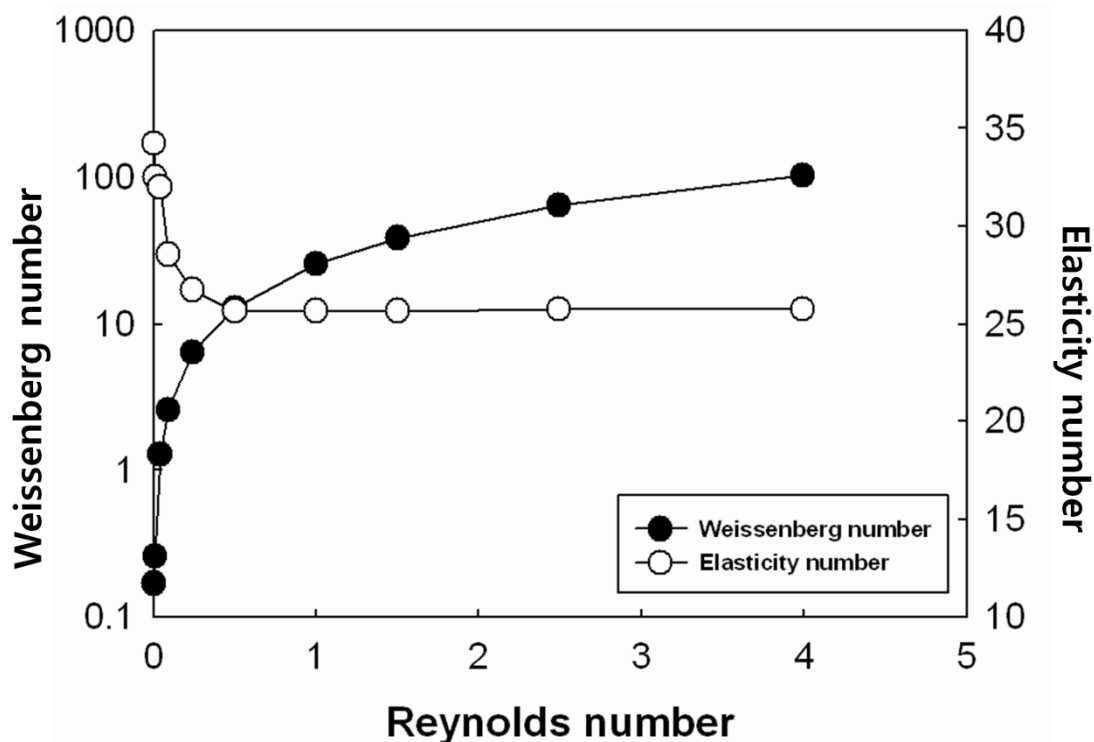


Fig. S-2 Characterization of elasto-inertia flow in a microchannel on a $Wi-Re-El$ diagram. Note that the Reynolds number (Re) and Weissenberg number (Wi) are proportional to flow rate, as shown in Eqs. (1) and (2). As Re increased, Wi increased but El decreased exponentially. The variations of Wi and El with increasing flow rate was associated with shear-dependent characteristic viscosity, η_c , used in the definition of the dimensionless numbers. However, when η_c reached infinite shear viscosity at sufficiently high flow rates, El did not vary with flow rate and became independent of Re . For instance, at sufficiently high flow rates (i.e., $Re = 0.5 \sim 4.0$), Wi increased (12.8 \sim 103) but El was remained nearly constant (25.7). The flow rate-independence of the elasticity number was also reported when zero-shear was adopted.⁶¹ It is worthy to note that in the asymptotic region of the elasticity number (i.e., at a fixed El), the degree of particle migration was dependent on flow rate.