

# Supplementary information for: A nanoliter-scale open chemical reactor

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## 1 Calibration of the $pH$ inside the $\mu$ CSTR

Figure 1 shows that the fluorescence of Oregon Green depends linearly on  $pH$  in the range 3.7 – 6.0. Figure 2 shows the effect of increasing concentration of the Edblom oscillator species on Oregon Green fluorescence. The presence of bromate has a negligible effect. In contrast,  $NaSO_3$  and  $K_4[Fe(CN)_6]$  clearly reduce the dye fluorescence at constant  $pH$ . The highest concentrations used in this work were  $[NaSO_3] = 100$  mM and  $[K_4[Fe(CN)_6]] = 65$  mM, resulting in a decrease of fluorescence of 20%, which was compatible with a correct determination of the  $pH$  inside the microreactor.

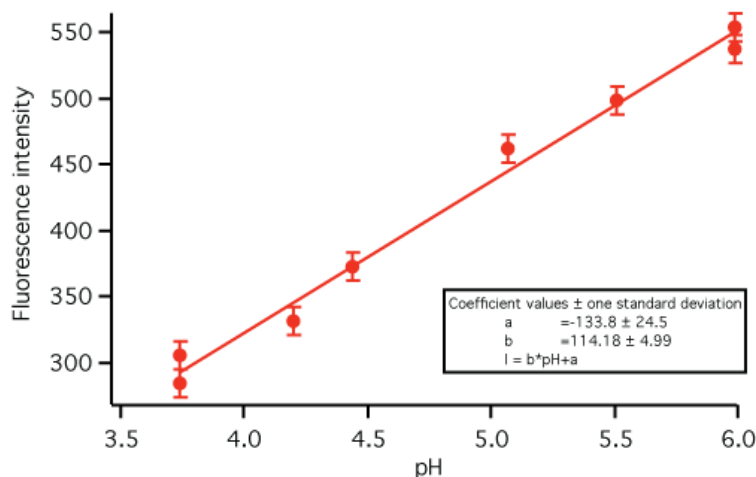


Figure S 1: Fluorescence intensity inside the  $\mu$ CSTR of a 10  $\mu$ M solution of Oregon Green in buffers of different  $pH$  recorded with a 2.5X objective.

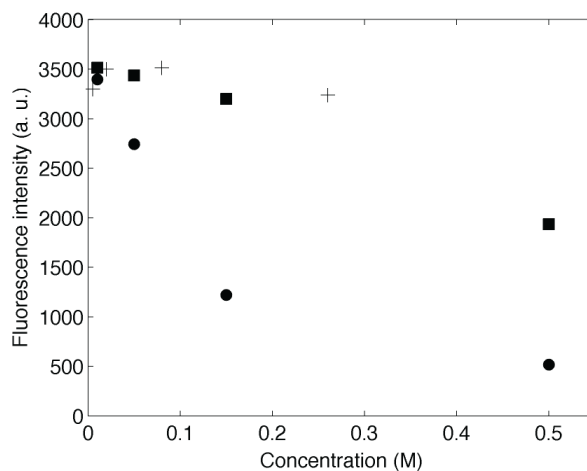


Figure S 2: Influence of reagent concentration on the maximum fluorescence intensity of Oregon Green 10  $\mu$ M for  $KBrO_3$  (crosses),  $NaSO_3$  (squares), and  $K_4[Fe(CN)_6]$  (disks).

## 2 3D view of the $\mu$ CSTR

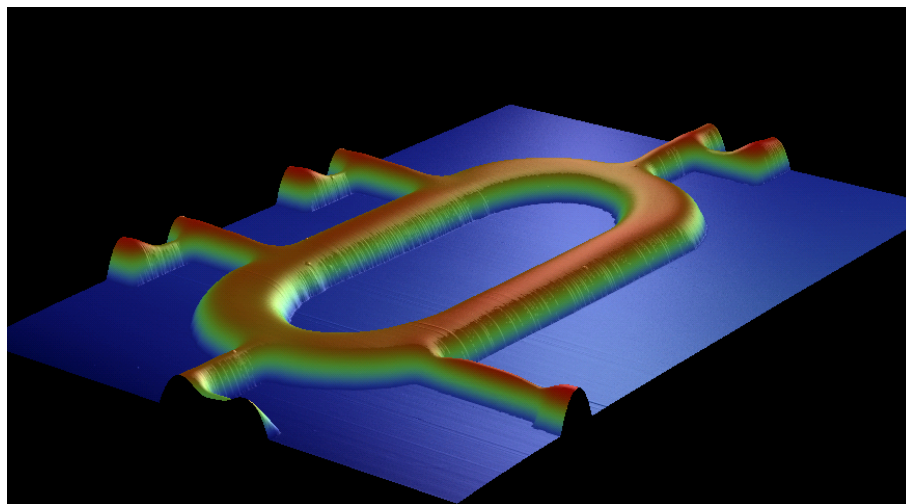


Figure S 3: 3D profile of the mould used to fabricate the  $\mu$ CSTR, acquired using a profilometer. The injection channels and the annular reactor are 100 and 200  $\mu\text{m}$  wide, respectively. The height is color coded, the maximum height of the annular channel being 10  $\mu\text{m}$ .

## 3 Reproducibility and influence of mixing

### 3.1 Determination of the mixing time

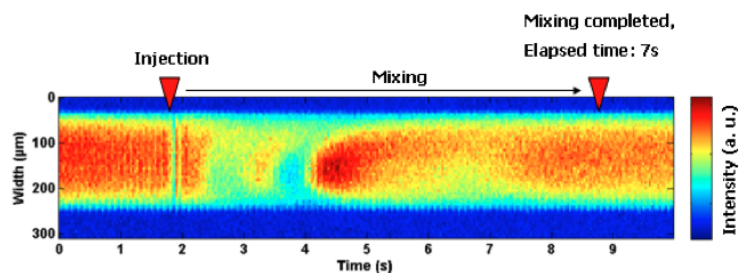


Figure S 4: Determination of the mixing time in the  $\mu$ CSTR. Fluorescent intensity profile across the width of the annular channel *vs* time (kymograph) during injection and mixing.

### 3.2 Influence of mixing on the behaviour of the Edblom oscillator in the $\mu$ CSTR

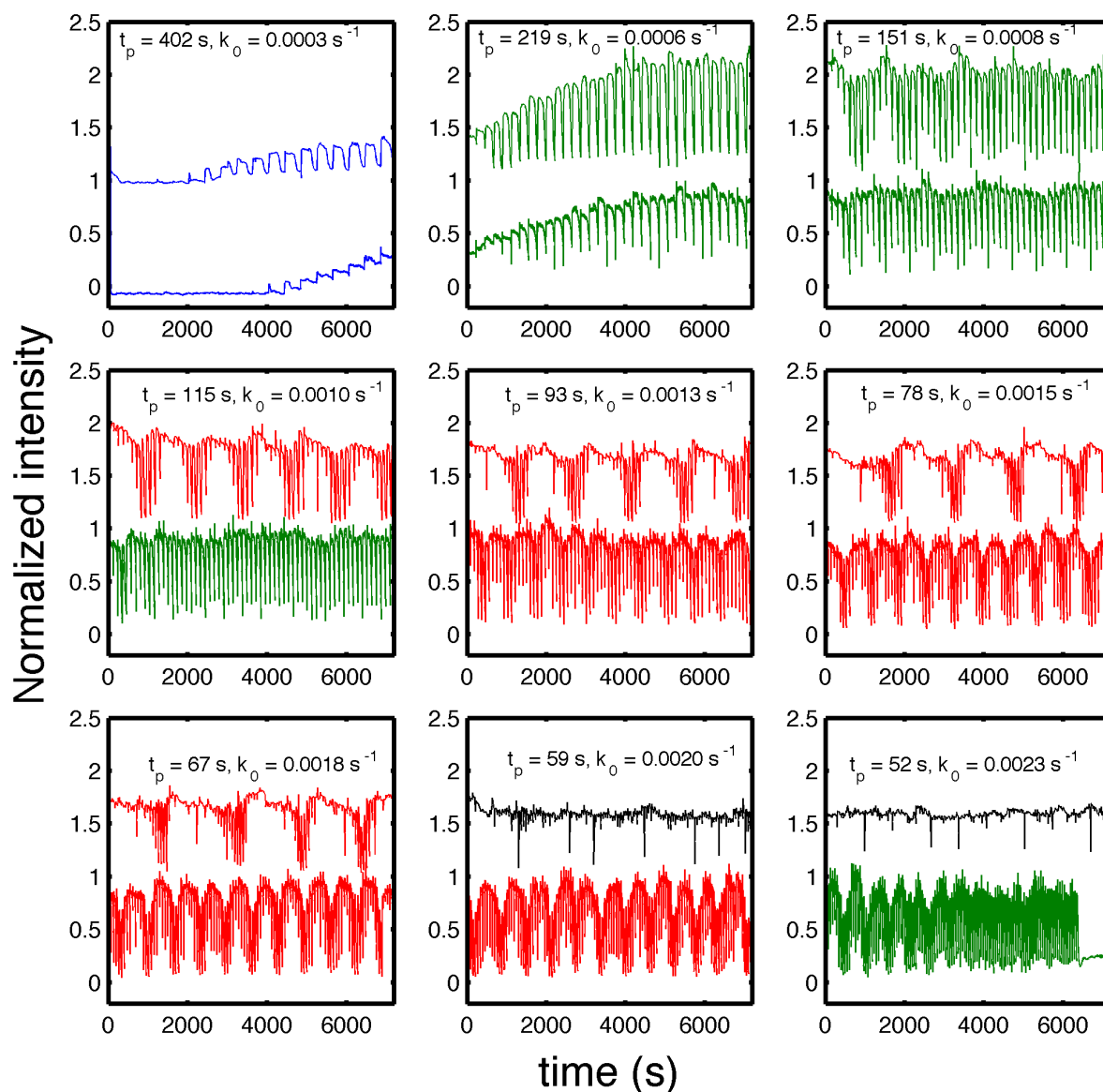


Figure S 5: Influence of mixing on the behavior of the Edblom oscillator. Normalized fluorescence intensities *vs* time for optimal mixing (lower curves) and non-optimal mixing (upper curves) at different injection periods,  $t_p$ , and their corresponding feeding rates,  $k_0$ .  $[Na_2SO_3] = 50$  mM,  $[H_2SO_4] = 5$  mM,  $[K_4Fe(CN)_6] = 20$  mM and  $[KBrO_3] = 65$  mM. Optimal mixing was completed in 7 s, while non-optimal mixing took 20 s. Color indicates the state of the oscillator: low pH (blue), forced oscillations (green), sustained oscillations (red), and high pH (black). Curves are shifted vertically for clarity.

#### 4 pH of the bromate channel with and without purging

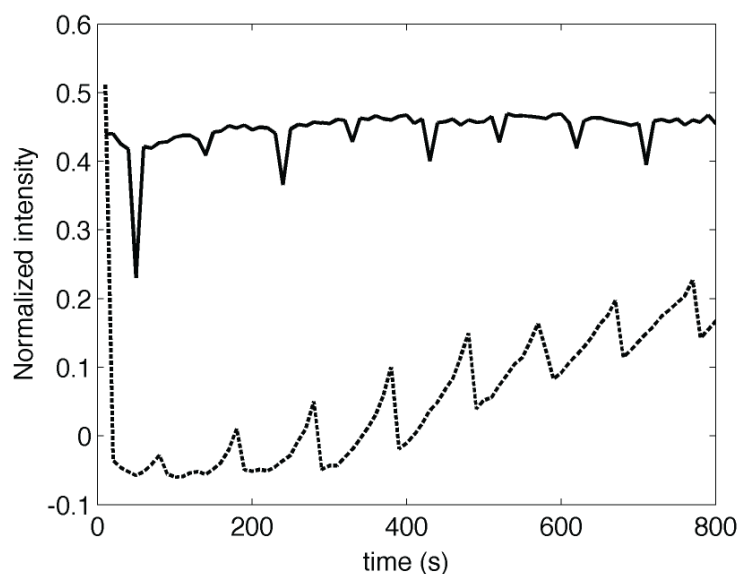


Figure S 6: Effect of the purging on the  $pH$  of the injected solution of  $KBrO_3$  65 mM. The  $pH$  is given by the fluorescence of Oregon Green 10  $\mu M$ . Purging was on (solid line) or off (dashed line). The intensity was measured inside the injection channel, between valves 1 and 2.

#### 5 Experimental $pH$ vs time plots

In this section are displayed, in large format, the normalized fluorescence intensity *vs* time plots represented in the phase diagram in Fig. 5A in the Main Text. The following conditions are common to all graphs: 5 mM  $H_2SO_4$ , 20 mM  $K_4[Fe(CN)_6]$ , and 65 mM  $KBrO_3$ . The graphs are color-coded as in the Main Text: low  $pH$  (black), forced oscillations (green), sustained oscillations (red), and high  $pH$  (black).

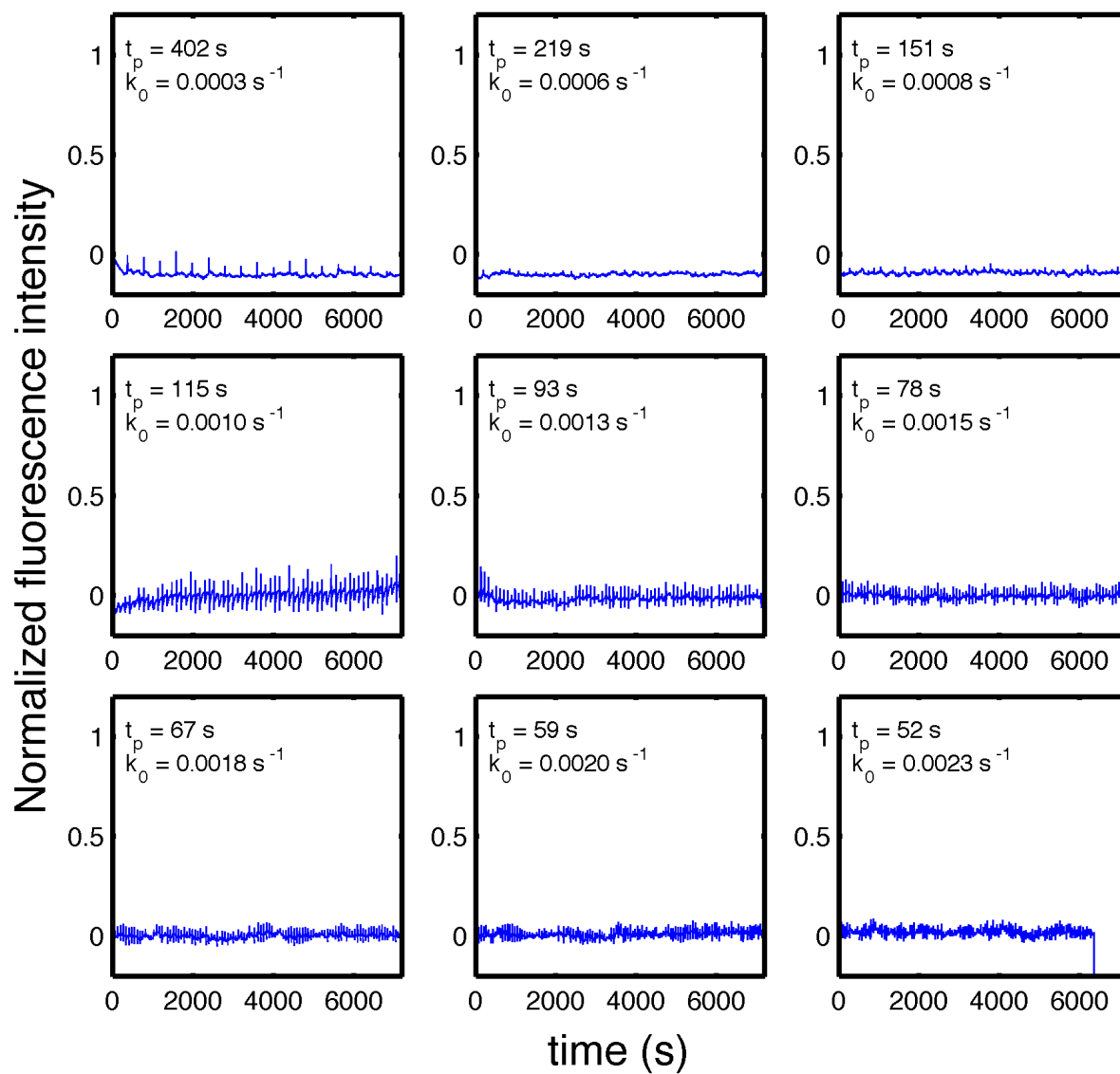


Figure S 7: Experimental normalized average fluorescence intensity for different injection periods,  $t_p$ , and their corresponding feeding rates,  $k_0$ , when the concentration of injected  $\text{Na}_2\text{SO}_3$  was 25 mM.

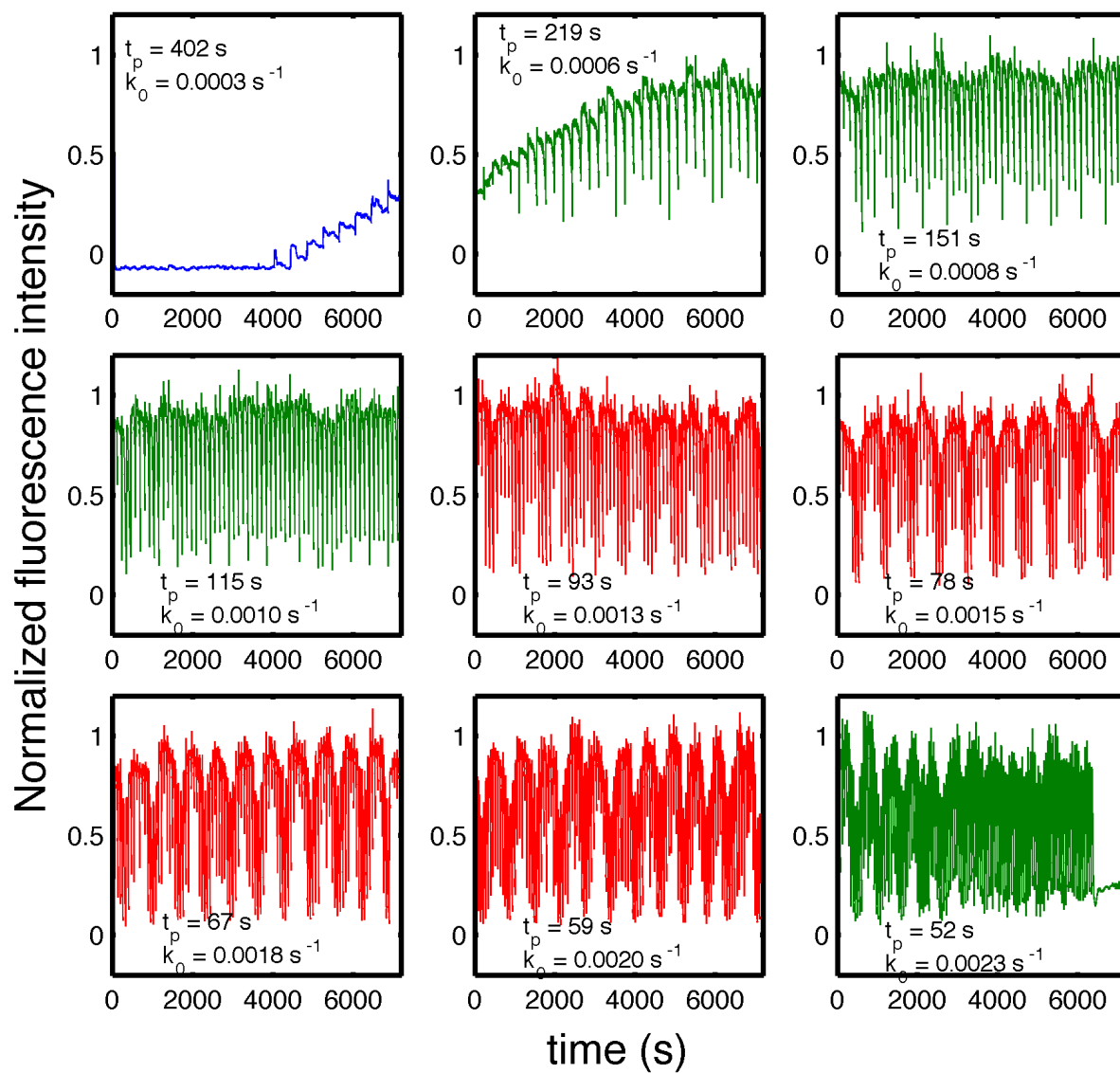


Figure S 8: Experimental normalized average fluorescence intensity for different injection periods,  $t_p$ , and their corresponding feeding rates,  $k_0$ , when the concentration of injected  $Na_2SO_3$  was 50 mM.

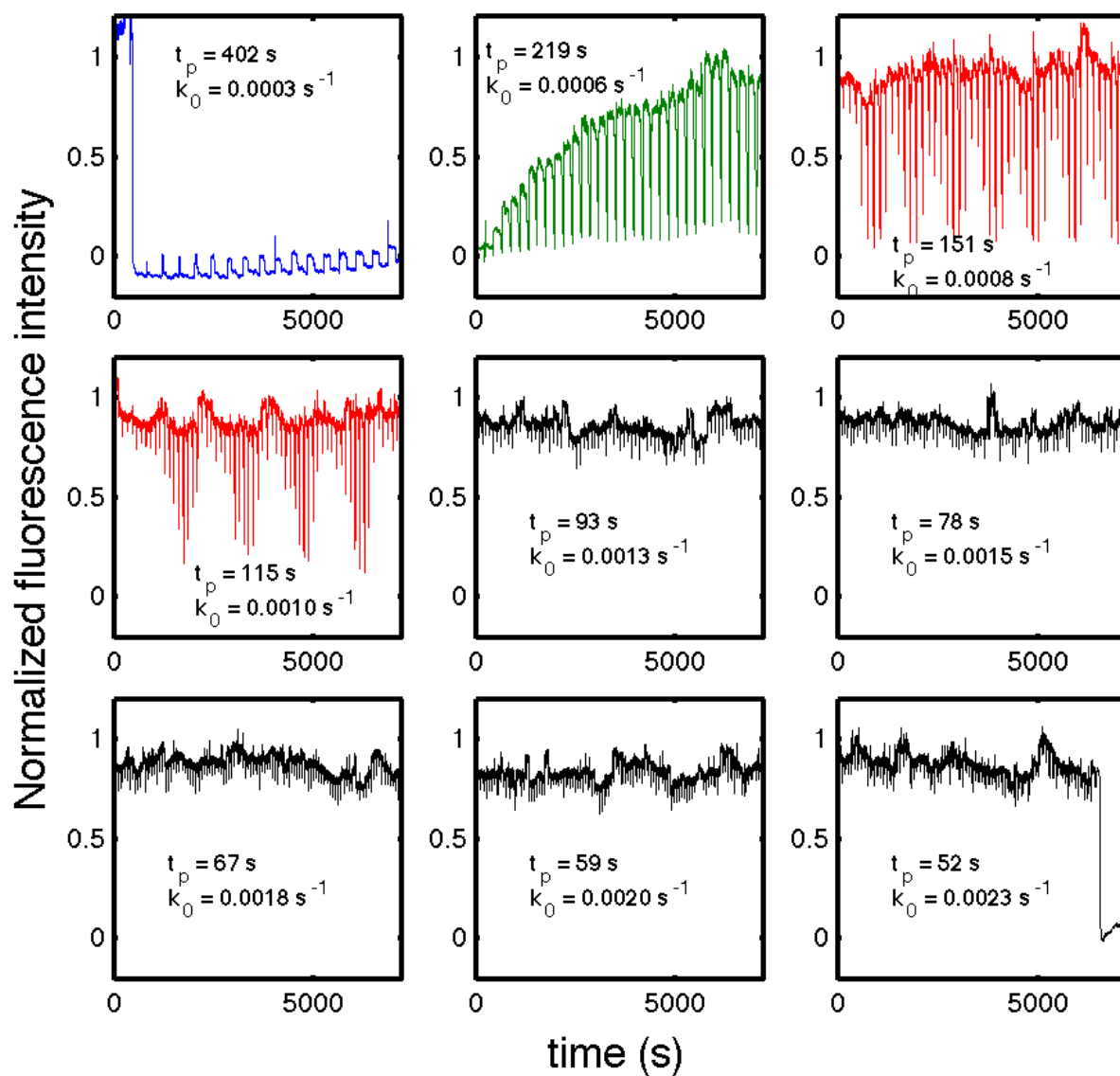


Figure S 9: Experimental normalized average fluorescence intensity for different injection periods,  $t_p$ , and their corresponding feeding rates,  $k_0$ , when the concentration of injected  $Na_2SO_3$  was 75 mM.



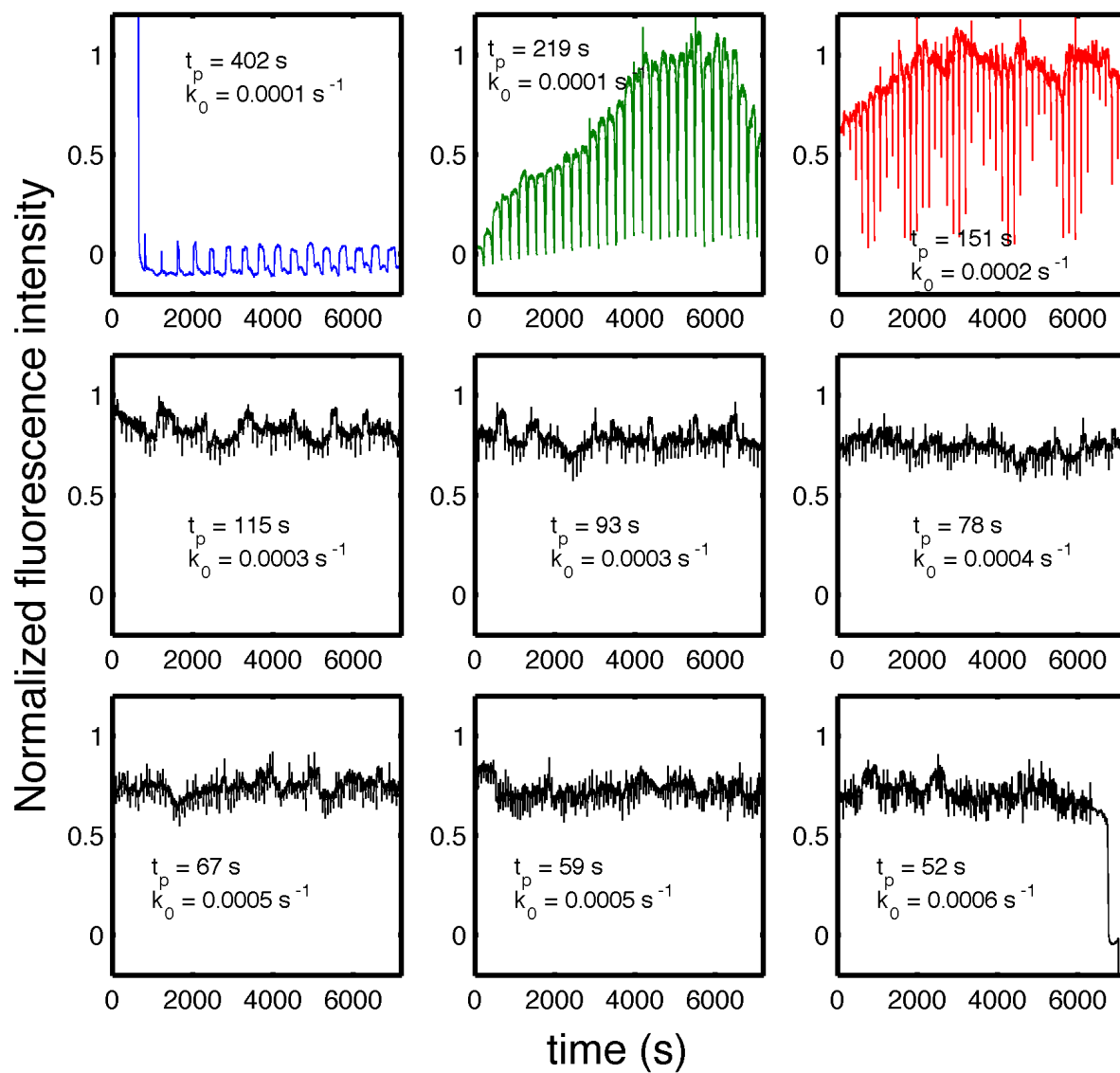
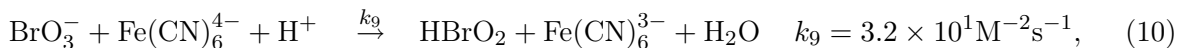
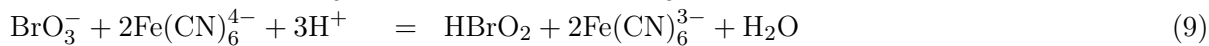
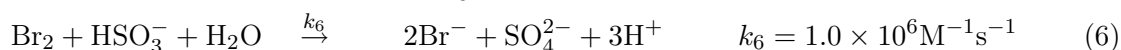
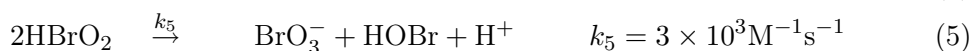
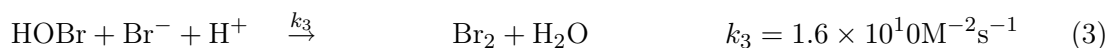
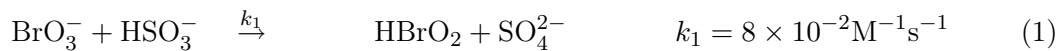


Figure S 10: Experimental normalized average fluorescence intensity for different injection periods,  $t_p$ , and their corresponding feeding rates,  $k_0$ , when the concentration of injected  $Na_2SO_3$  was 100 mM.

## 6 Simulations

### 6.1 Model of the Edblom oscillator

Edblom et al<sup>1</sup> demonstrated that the main features of the oscillator studied in this work were described with the following set of reactions



where (9) defines the stoichiometry of the oxydation of  $\text{Fe}(\text{CN})_6^{4-}$  and (10) accounts for the mechanism from which the rate is computed. The rates for reactions 1 to 9 are

$$r_1 = k_1[\text{BrO}_3^-][\text{HSO}_3^-] \quad (11)$$

$$r_2 = k_2[\text{HBrO}_2][\text{Br}^-][\text{H}^+] \quad (12)$$

$$r_3 = k_3[\text{HOBr}][\text{Br}^-][\text{H}^+] \quad (13)$$

$$r_4 = k_4[\text{Br}_2] \quad (14)$$

$$r_5 = k_5[\text{HBrO}_2]^2 \quad (15)$$

$$r_6 = k_6[\text{Br}_2][\text{HSO}_3^-] \quad (16)$$

$$r_7 = k_7[\text{H}^+][\text{SO}_3^{2-}] \quad (17)$$

$$r_8 = k_8[\text{HSO}_3^-] \quad (18)$$

$$r_9 = k_9[\text{BrO}_3^-][\text{Fe}(\text{CN})_6^{4-}][\text{H}^+]. \quad (19)$$

The differential equations describing the temporal evolution of the species involved in the Edblom oscillator in a CSTR are thus

<sup>1</sup>E. C. Edblom, Y. Luo, M. Orban, K. Kustin and I. R. Epstein, *J. Phys. Chem.*, **1989**, 93, 2722-2727.

$$\frac{d[\text{Br}^-]}{dt} = -r_2 - r_3 + r_4 + 2r_6 - k_0[\text{Br}^-] \quad (20)$$

$$\frac{d[\text{Br}_2]}{dt} = r_3 - r_4 - r_6 - k_0[\text{Br}_2] \quad (21)$$

$$\frac{d[\text{HOBr}]}{dt} = 2r_2 - r_3 + r_4 + r_5 - k_0[\text{HOBr}] \quad (22)$$

$$\frac{d[\text{HBrO}_2]}{dt} = r_1 - r_2 - 2r_5 + r_9 - k_0[\text{HBrO}_2] \quad (23)$$

$$\frac{d[\text{BrO}_3^-]}{dt} = -r_1 + r_5 - r_9 + k_0([\text{KBrO}_3]^{IN} - [\text{BrO}_3^-]) \quad (24)$$

$$\frac{d[\text{SO}_3^{2-}]}{dt} = -r_7 + r_8 + k_0([\text{Na}_2\text{SO}_3]^{IN} - [\text{SO}_3^{2-}]) \quad (25)$$

$$\frac{d[\text{HSO}_3^-]}{dt} = -r_1 - r_6 + r_7 - r_8 - k_0[\text{HSO}_3^-] \quad (26)$$

$$\frac{d[\text{Fe}(\text{CN})_6^{4-}]}{dt} = -2r_9 + k_0([\text{K}_4\text{Fe}(\text{CN})_6]^{IN} - [\text{Fe}(\text{CN})_6^{4-}]) \quad (27)$$

$$\frac{d[\text{Fe}(\text{CN})_6^{3-}]}{dt} = 2r_9 - k_0[\text{Fe}(\text{CN})_6^{3-}] \quad (28)$$

$$\frac{d[\text{H}^+]}{dt} = -r_2 - r_3 + r_4 + r_5 + 3r_6 - r_7 + r_8 - 3r_9 + r_{10} + k_0([\text{H}^+]^{IN} - [\text{H}^+]), \quad (29)$$

where  $k_0$  is the feeding rate,  $[I]^{IN}$  is the concentration of species I being injected in the CSTR.  $[\text{H}^+]$  is being injected as  $\text{H}_2\text{SO}_4$ , an acid with  $pK_{a,1} = -3$  and  $pK_{a,2} = 2$ . The lowest  $p\text{H}$  of the oscillator being about 2, we can consider that  $\text{H}_2\text{SO}_4$  exists in solution only as species  $\text{HSO}_4^-$  and  $\text{SO}_4^{2-}$ . At a given time, for a proton concentration in the reactor  $[\text{H}^+]$ , an injection of  $[\text{H}_2\text{SO}_4]^{IN}$  results in an injected concentration of protons given by

$$[\text{H}^+]^{IN} = [\text{H}_2\text{SO}_4]^{IN} \left( 1 + \frac{1}{(1 + [\text{H}^+]/K_{a,2})} \right). \quad (30)$$

We consider here that the protonation equilibria of  $\text{H}_2\text{SO}_4$  are infinitely fast compared with reactions 1 to 9. We do neglect the contribution of protons coming from a remaining quantity of  $\text{HSO}_4^-$  at low  $p\text{H}$  that would liberate protons when the  $p\text{H}$  rises in the reactor.

Equations (20) to (29) take the form of Equation 1 in the Main Text, that we reproduce here for clarity,

$$\frac{dC_i(t)}{dt} = f_i(k_j, C_l(t)) + k_0(C_i^{IN} - C_i(t)). \quad (31)$$

The system of equations (20) to (29) can be simulated in a macroscopic CSTR as is. In contrast, to simulate these equations in a  $\mu\text{CSTR}$  we need to take into account the digital character of the injection. For each species  $i$ , (31) was rewritten as

$$\frac{dC_i(t)}{dt} = \chi(1 - H)f_i(k_j, C_l(t)) + H\frac{k_0}{t_{inj}}(C_i^{IN} - C_i(t)), \quad (32)$$

where  $H$  is a function that takes into account the digital character of the injection. It is equal to 1 during the injection phase, that lasted  $t_{inj} = 5$  s in our simulations, and equal to 0 otherwise. Note

that this implementation assumes perfect mixing as soon as the injection phase ends.  $\chi$  is a coupling parameter that we have added to remove a divergence due to the sharp change in the derivative introduced by the discontinuous function  $H$ . After an injection, the concentrations of the different species may change quite abruptly and make the computed derivative very large, thus introducing, for instance, negative values of the concentrations. To smooth this effect, the contribution of  $f_i(k_j, C_l(t))$  to (32) was switched on linearly after an injection, with  $\chi = t/t_{switch}$ , and  $t_{switch} = 10$  s.

Differential equations were solved in Matlab using `ode23s` solver for stiff problems. It is a one-step solver that uses a modified Rosenbrock formula of order 2.

## 6.2 Comparison experiments/simulations in a closed reactor

The experimental and simulated phase diagram of the Edblom oscillator in the same conditions (5 mM  $\text{H}_2\text{SO}_4$ , 20 mM  $\text{K}_4[\text{Fe}(\text{CN})_6]$ , and 65 mM  $\text{KBrO}_3$ ), displayed in Figure 11, are significantly different. Several reasons can be invoked to explain this discrepancy: i) mixing in the experiments takes 7 s, while in the simulations it is instantaneous, ii) injection and mixing are considered independent processes in the simulations, but they are simultaneous, and coupled to spatial transport, in the experiments, iii) the high surface to volume ratio of the  $\mu\text{CSTR}$  is not taken into account in the simulations, notably the evaporation of important intermediates such as  $\text{Br}_2$  through the porous walls of PDMS, and iv) the influence of the fluorescent dye is disregarded in the simulations. Instead of studying each of these processes in detail we decided to take a phenomenological description. To do so we performed a series of experiments, and the corresponding simulations, using the  $\mu\text{CSTR}$  as a closed reactor for different concentrations of  $\text{H}_2\text{SO}_4$  and  $\text{Na}_2\text{SO}_3$ . In these experiments the four reagents were injected 50 consecutive times into the annular reactor and mixed to create a reproducible initial condition corresponding to 1/4 of the volume of the reactor for each injected solution. The injection valves were closed, mixing remained active and fluorescence was recorded. The results are displayed in Figure 12. For all the experiments the fluorescence intensity (the  $p\text{H}$ ) stays high and stable until it abruptly drops (within 30 s) and remains low. The time at which the fluorescence ( $p\text{H}$ ) drops depends on  $[\text{Na}_2\text{SO}_3]$  and  $[\text{H}_2\text{SO}_4]$ . The behavior of the Edblom oscillator at 5 mM  $\text{H}_2\text{SO}_4$  in a closed reactor is significantly different for the experiments and the simulations. In contrast, results are similar when we compare simulations and experiments at 10 and 5 mM  $\text{H}_2\text{SO}_4$  respectively. We argue that increasing the concentration of  $\text{H}_2\text{SO}_4$  in the simulations to 10 mM phenomenologically takes into account the factors evoked above that are not incorporated in the simulations. We thus compare, in the Figure 5 of the Main Text, the experimental phase diagram at 5 mM  $\text{H}_2\text{SO}_4$  with the simulated phase diagram at 10 mM  $\text{H}_2\text{SO}_4$ .

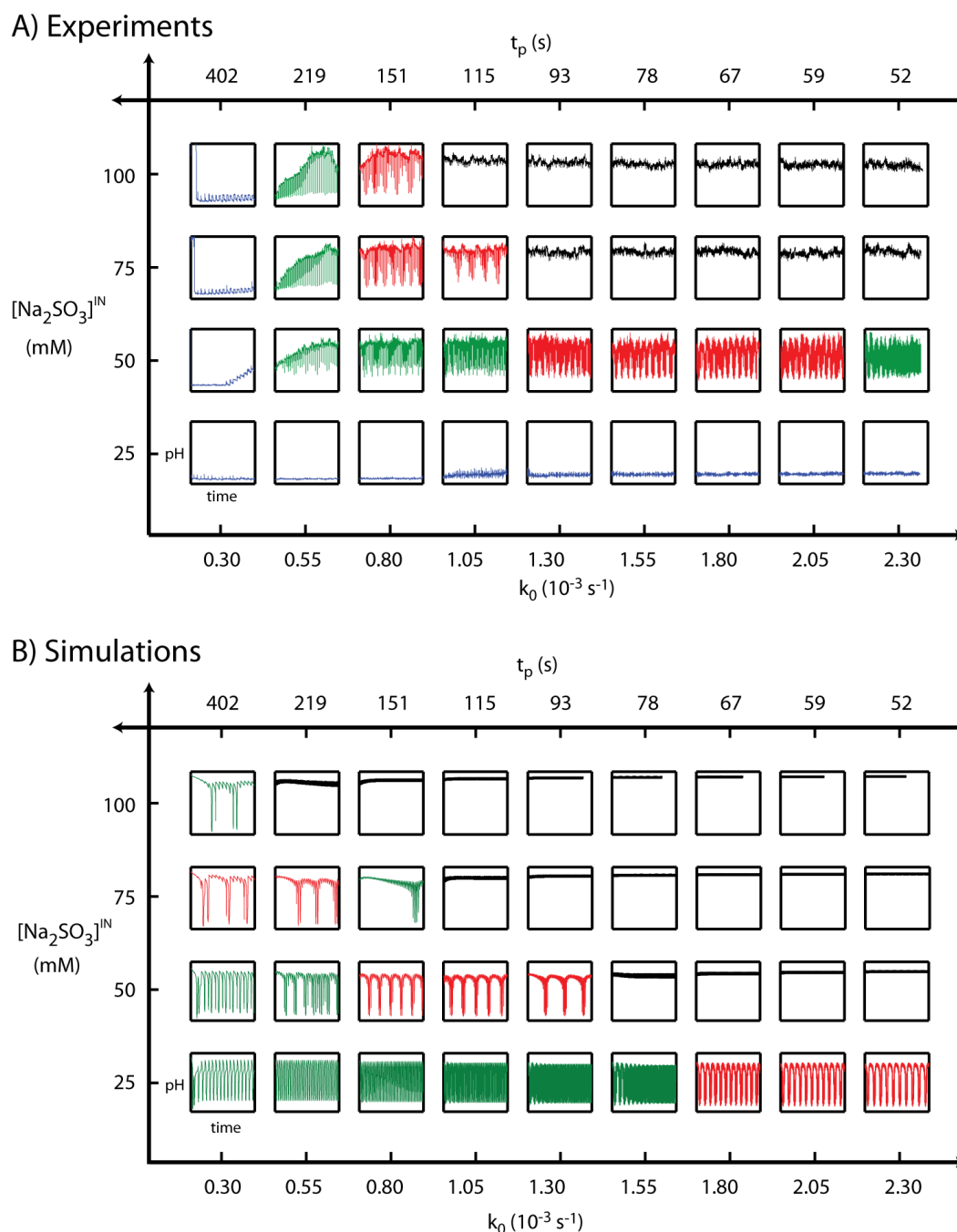


Figure S 11: Experimental (top) and simulated (bottom) phase diagram of the Edblom oscillator in the  $\mu$ CSTR for different  $\text{Na}_2\text{SO}_3$  input concentrations and at different feeding rates  $k_0$  (and their corresponding injection periods  $t_p$ ). Each square represents  $\text{pH}$  vs. time during a 2 h experiment. Time traces are colour-coded according to the observed steady state: low  $\text{pH}$  (blue), forced oscillations (green), sustained oscillations (red), and high  $\text{pH}$  (black). In contrast with Fig. 5 in the Main Text, here  $[\text{H}_2\text{SO}_4] = 5 \text{ mM}$  both for the experiment and for the simulations. The remaining injected concentrations are  $\text{K}_4[\text{Fe}(\text{CN})_6]$  20 mM and  $\text{KBrO}_3$  65 mM.

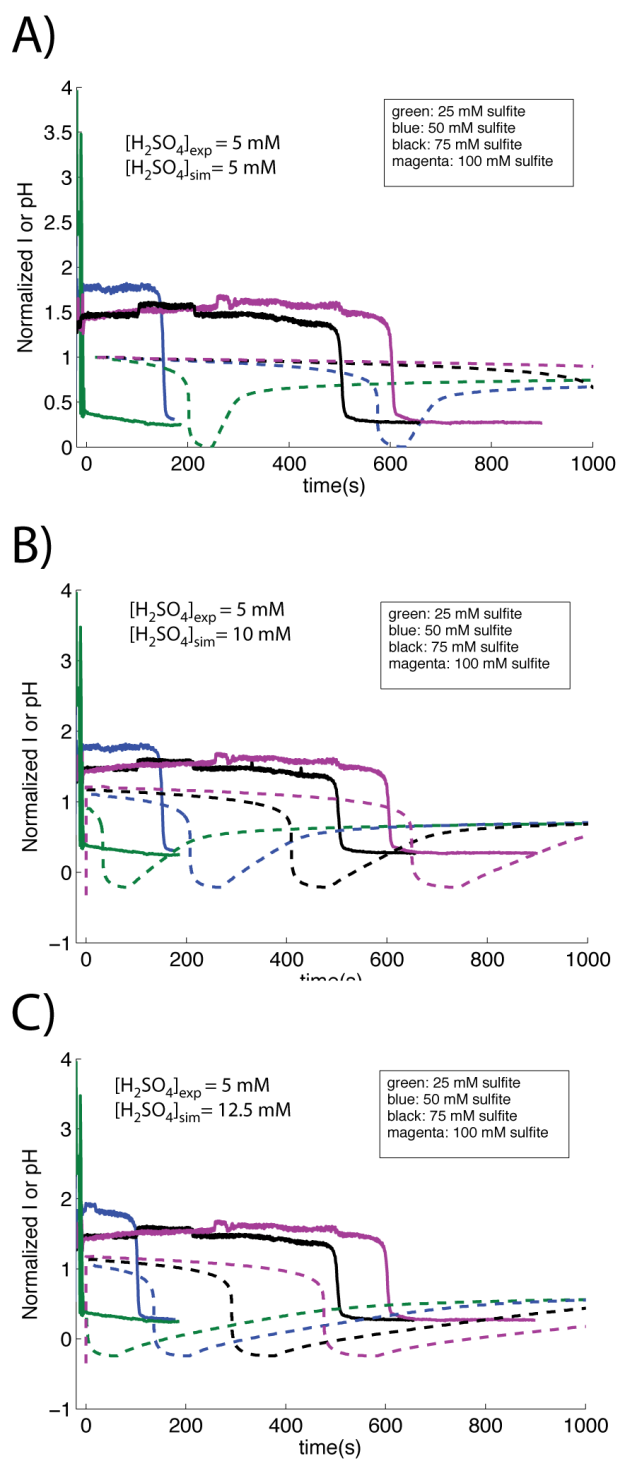


Figure S 12: Normalized intensity (experiments, solid lines) or normalized  $pH$  (simulations, dashed lines) *vs* time after mixing in a closed reactor for different concentrations of  $Na_2SO_3$  (25 mM, green, 50 mM, blue, 75 mM, black, and 100 mM, magenta) and  $H_2SO_4$ , and for 20 mM  $K_4[Fe(CN)_6]$  and 65 mM  $KBrO_3$ .

### 6.3 Simulated *pH vs time* plots

In this subsection are displayed, in large format, the normalized *pH vs time* plots represented in the phase diagram in Fig. 5B in the Main Text. The following conditions are common to all graphs:  $[\text{H}_2\text{SO}_4] = 10 \text{ mM}$ ,  $\text{K}_4[\text{Fe}(\text{CN})_6] = 20 \text{ mM}$  and  $\text{KBrO}_3 = 65 \text{ mM}$ . The graphs are color-coded as in the Main Text: low *pH* (black), forced oscillations (green), sustained oscillations (red), high *pH* (black).

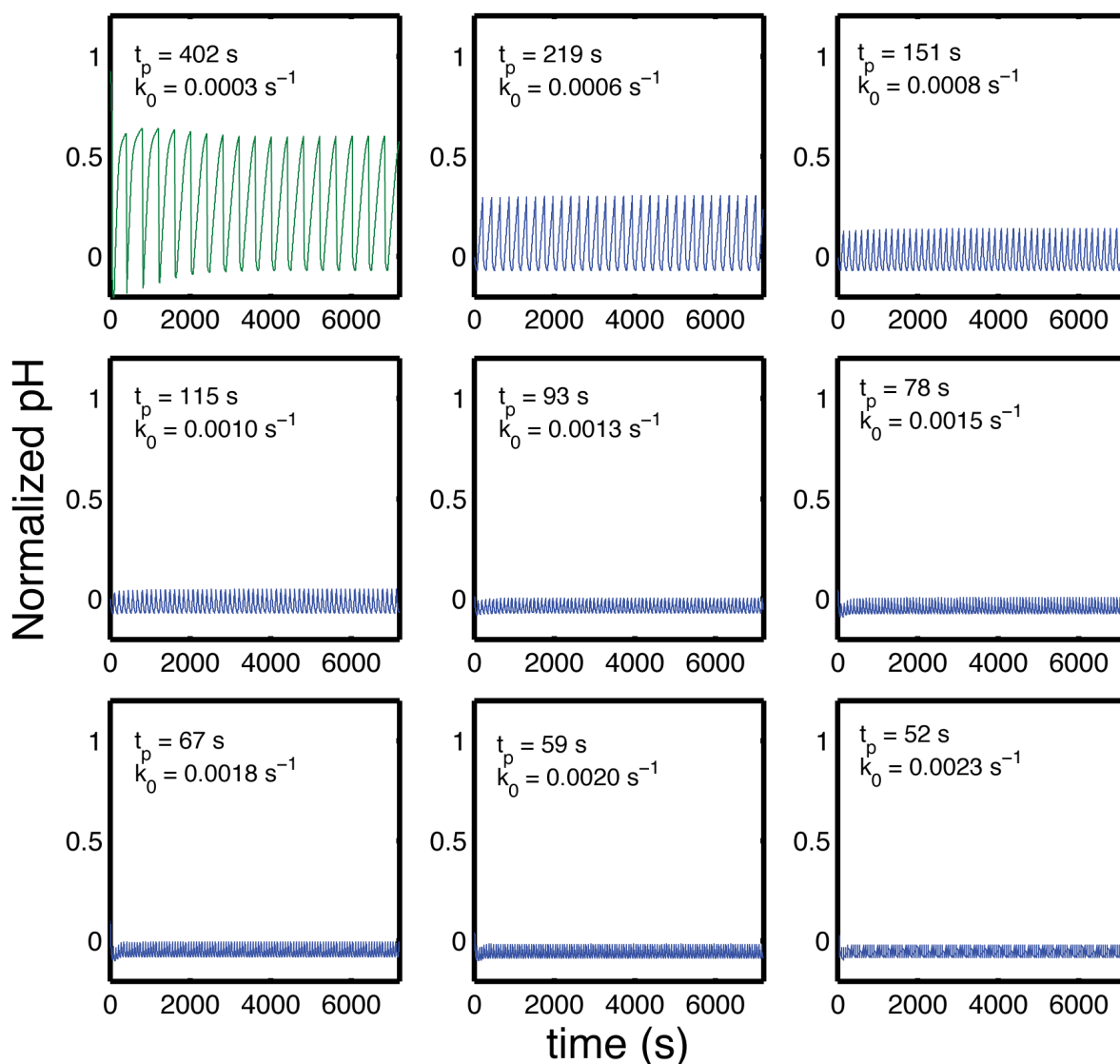


Figure S 13: Simulated normalized average fluorescence intensity for different injection periods,  $t_p$ , and their corresponding feeding rates,  $k_0$  when the concentration of injected  $\text{Na}_2\text{SO}_3$  was 25 mM.

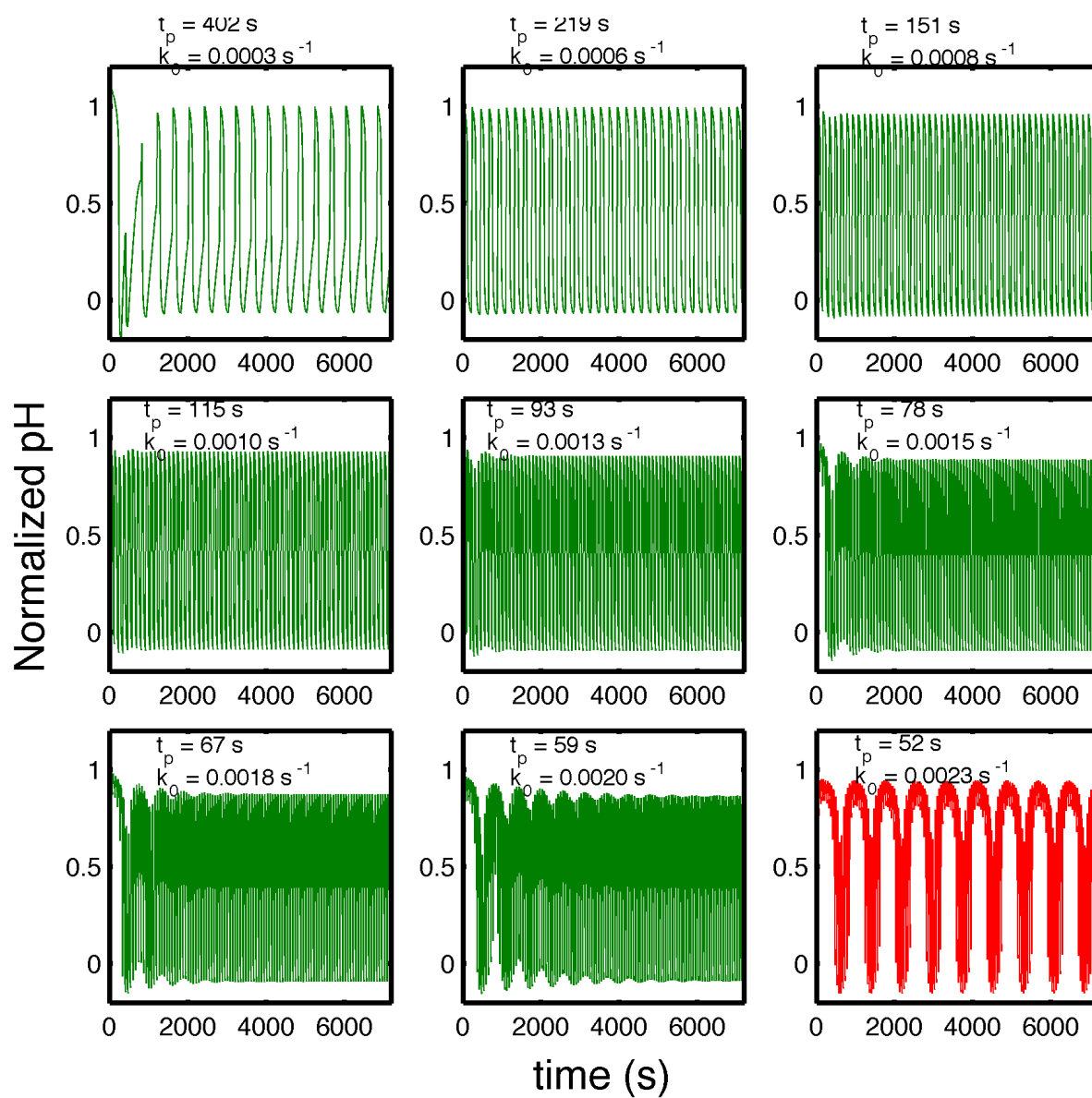


Figure S 14: Simulated normalized average fluorescence intensity for different injection periods,  $t_p$ , and their corresponding feeding rates,  $k_0$  when the concentration of injected  $\text{Na}_2\text{SO}_3$  was 50 mM.



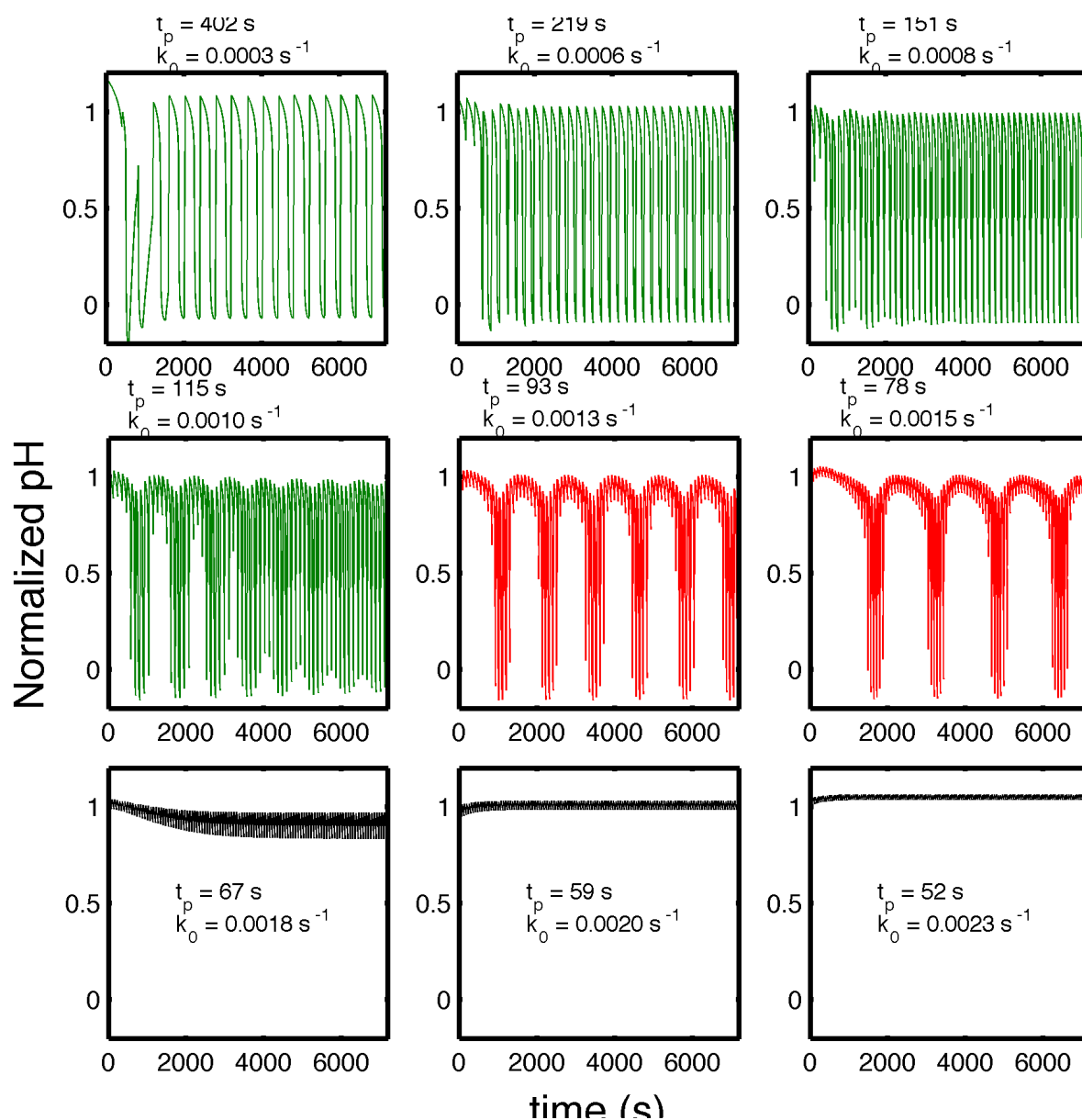


Figure S 15: Simulated normalized average fluorescence intensity for different injection periods,  $t_p$ , and their corresponding feeding rates,  $k_0$  when the concentration of injected  $\text{Na}_2\text{SO}_3$  was 75 mM.

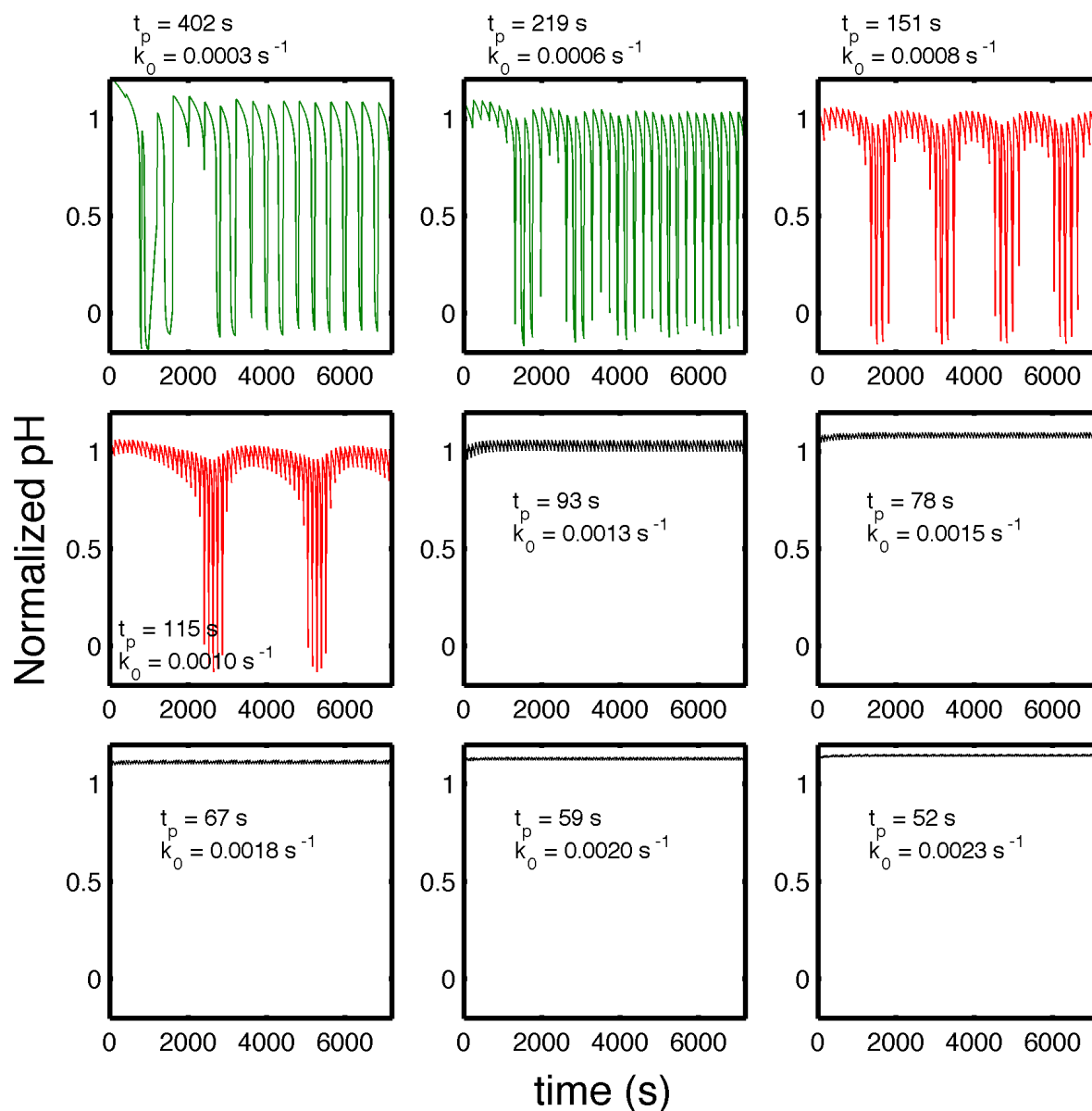


Figure S 16: Simulated normalized average fluorescence intensity for different injection periods,  $t_p$ , and their corresponding feeding rates,  $k_0$  when the concentration of injected  $\text{Na}_2\text{SO}_3$  was 100 mM.

## 7 Attached files

### 7.1 Video of the Edblom oscillator in the $\mu\text{CSTR}$

A video showing two periods of the Edblom oscillator for 20 mM  $\text{K}_4[\text{Fe}(\text{CN})_6]$ , 65 mM  $\text{KBrO}_3$ , 75 mM  $\text{Na}_2\text{SO}_3$ , and 5 mM  $\text{H}_2\text{SO}_4$  being injected, with a period  $t_p = 115$  s, in the  $\mu\text{CSTR}$  and observed with 10  $\mu\text{M}$  Oregon green under a fluorescence microscope is available for download.

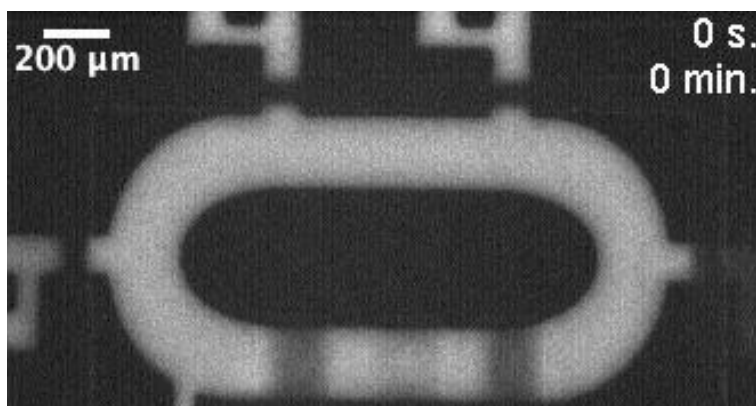


Figure S 17: First frame of the attached video.

## 7.2 Matlab code for simulations

The Matlab code for the simulations described in section 6 is available for download. It is constituted of the following functions:

```
function do_solve_Edblom_kinetics_for_several_input
% Calls the solver plot_solutions_parameter_Edblom_kinetics for
%different concentrations of sulfite and sulfuric acid

function plot_solutions_parameter_Edblom_kinetics(varargin)
%Calls the ODE solver function solve_kinetics_with_parameters_CSTR_Edblom( pumpingPeriod(i),
%fId ) for different values of pumpingPeriod. Then makes plots with the
%results from that function. 'param' and 'out' are the principal
%structures, with the parameters and the output values
%If varargin > 0 the first one is the input sulfite conc and the second one
%the input sulfuric acid conc

function [t y] = solve_kinetics_with_parameters_CSTR_Edblom(param, x0, iCondition)
% This function implements the kinetic model for the pH oscillator in a CSTR described
%in Edblom, JPhysChem 1989, Table 1
%in a continuous or digital CSTR modeled through k0
%Input is a structure param with the rate constants and the file id fId to write
%results in a text file, x0 is a vector containing the initial conditions,
%'iCondition' is a counter for an experiment with different k0
%OUTPUT are vectors time 't' and solution of the
%ODE 'y' as well as the structure param with normalized rates sigma_i

function param = create_parameter_struct_Edblom()
% Initializes the structure 'param' which stocks all the relevant parameters
%set by the user to solve the ODEs

function out = create_output_struct_Edblom()
% Initializes the structure 'out' which stocks all the quantities
%computed during the simulation
```

```
function jacob = edblom_jacobian(x, rate, H, chemCoupling, k0Comp)
% Claculates the Jacobian matrix of the Edblom ODE system
% written in function solve_kinetics_with_parameters_CSTR_Edblom
% INPUT: 'x' vector of concentrations, 'rate' structure of rates
% 'H' equal to 0 or 1 depending on injection conditions, 'cte'
% equal to 1 or 2 for digital or continuous injection,
% 'k0Comp' computed k0 value

function plot_Edblom_data(out, param)
% Plots outputs from function plot_solutions_parameter_Edblom_kinetics
% out and param are structures defined in that function
```