

Electronic Supplemental Information for An “Off-the-shelf” Capillary Microfluidic Device that Enables Tuning of the Droplet Breakup Regime at Constant Flow Rates

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Formation of double emulsions

Microfluidic double emulsions were produced in glass capillary microfluidic devices using the following conditions. The middle phase contained pure water with 1.35% (w/w) 250 nm latex nanoparticles (Surfactant-free poly methyl methacrylate, Arkema Inc.) which were fluorescently labeled using a solvent evaporation method described elsewhere¹ and 1.35% (w/w) Pluronic F68 (BASF). The inner and outer phases consisted of a mixture of 64% (v/v) Chlorinated Oil, (ParOil 10N, Dover Chemical Corp.) 34% (v/v) mineral oil, and 2% (v/v) ABIL EM 90 surfactant (Evonik Industries). The solutions were flowed together through orifices of 100 microns (Figure S1(a)) or 250 microns (Figure S1(b)).

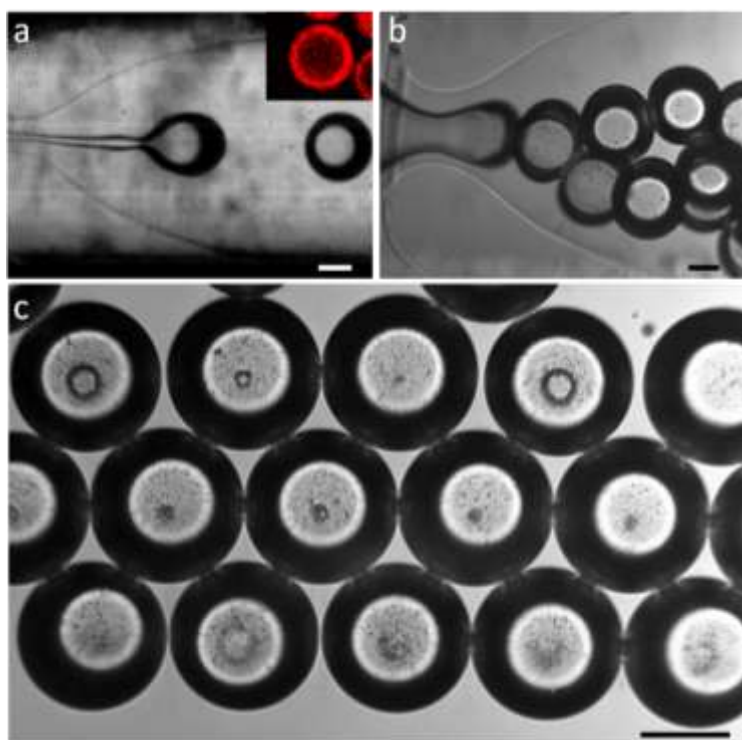


Figure S1. Microfluidic production of double emulsions with different devices. a) Production of a microfluidic double emulsion by jetting using a glass capillary device with a 100 μm orifice. Inner and middle phase flow rates were 0.5 $\mu\text{L}/\text{min}$, while the outer phase flow rate was 10 $\mu\text{L}/\text{min}$. Insert shows fluorescent nanoparticles in the middle phase. (i.e. aqueous outer phase of the double emulsion droplet) **b)** Screen shot of Supplemental Video 1 showing generation of a double emulsion by a device with a 250 μm orifice. Inner and middle phase flow rates are 5 $\mu\text{L}/\text{min}$ and the outer phase flow rate is 25 $\mu\text{L}/\text{min}$. **c)** Monodisperse droplets generated by device in Supplemental Video 1. Scale bars are 100 μm .

Image of tip wetting

Two different microfluidic devices were built using a tapered injection tips without chemical functionalization. Wetting of the tip is present in both cases and affecting the droplet break-up.

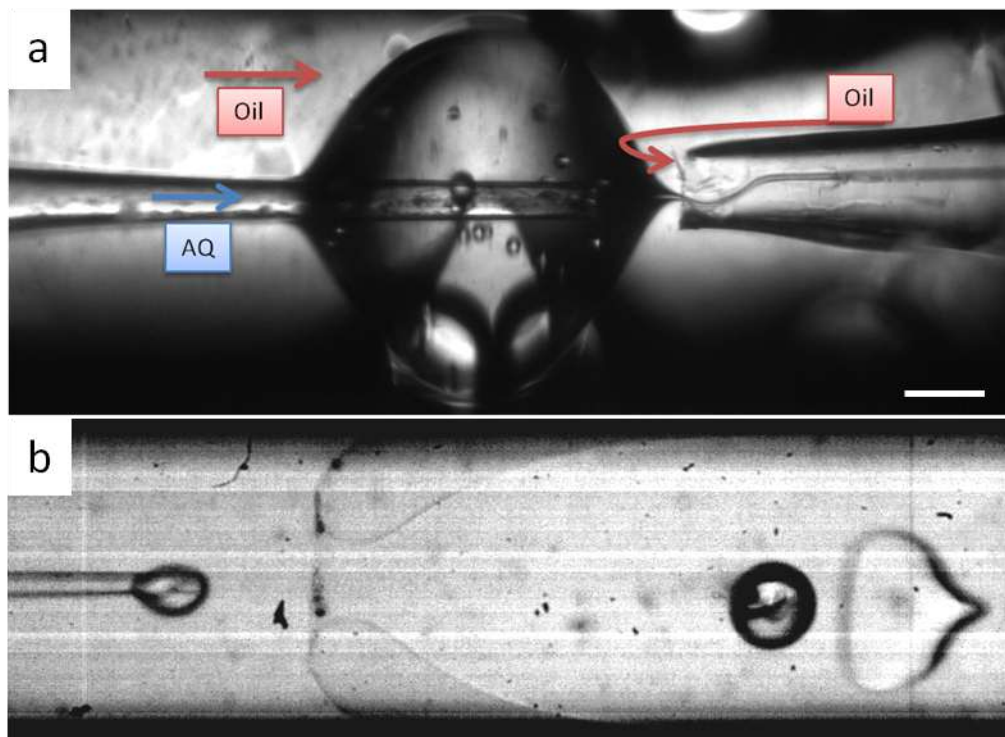


Figure S2. Wetting of the injection tip in two different microfluidics devices without chemical modification. a) Tapered collection orifice. **b)** Flamed collection orifice. Scale bar is 100 μm .

Images used to build graph in Figure 4

Capillary microfluidic droplet generation was performed using a pure water in mineral oil with 2% (v/v) Span 80 system. Images were used to construct Figure 4 and are presented in the supplemental information to show the phenomenon occurring using a different surfactant.

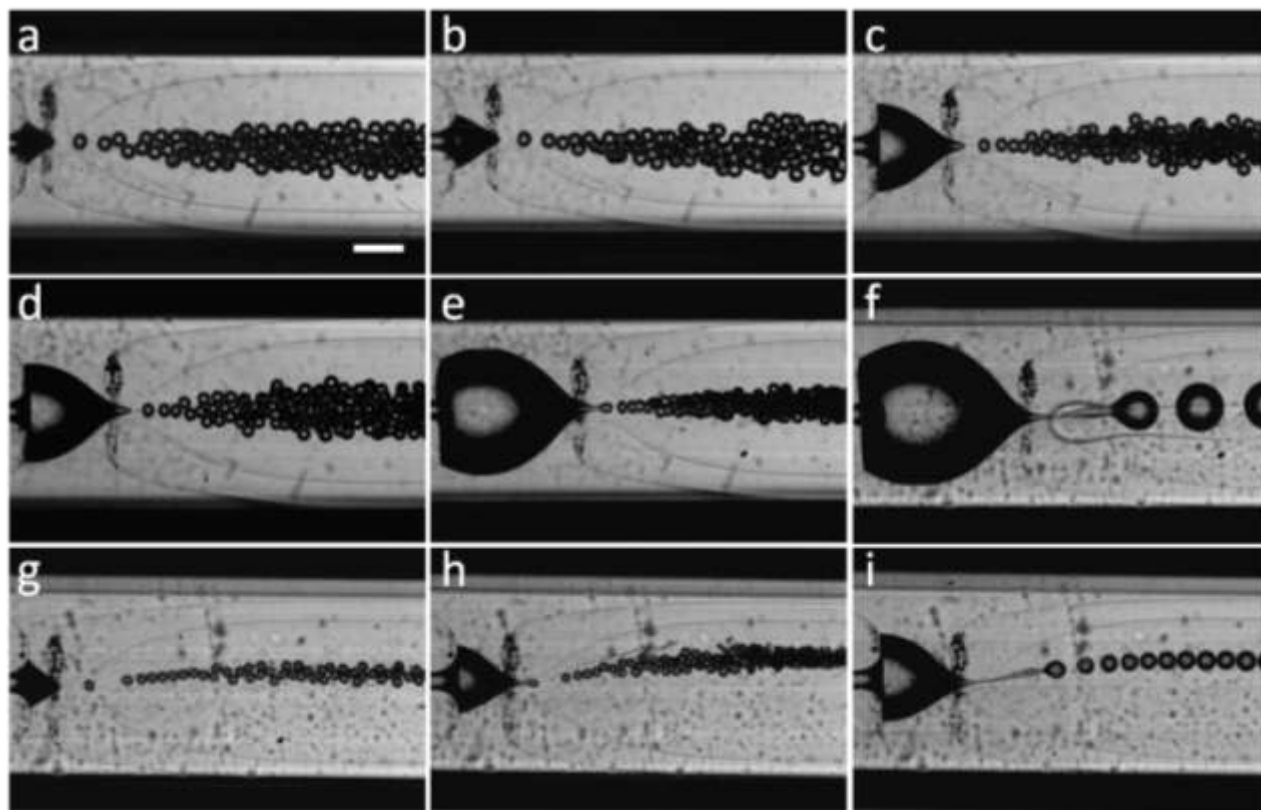


Figure S3. Changing the tip separation in a water, mineral oil system with Span 80 surfactant to generate the data used for Figure 4. a-f) Flow rate ratio is 10, the continuous phase flow rate (q_c) is 20 $\mu\text{L}/\text{min}$ and the dispersed phase flow rate (q_d) is 2 $\mu\text{L}/\text{min}$. Tip separation varies from 50 μm up to 600 μm **g-i)** Flow rate ratio is 100, q_c is 20 $\mu\text{L}/\text{min}$ and q_d is 0.2 $\mu\text{L}/\text{min}$. Tip separation varies from 50 μm to 300 μm . Scale bar is 200 μm .

Supplemental Video 1

As shown in Figure S1(b), a double emulsion was produced by using the formulation described above and a device with a 250 μm orifice. The inner and middle phase flow rates were maintained at 5 $\mu\text{L}/\text{min}$ and the outer phase flow rate was 25 $\mu\text{L}/\text{min}$. Stable droplet generation can be observed over the 25 second period in the video and monodisperse droplets are shown in Figure S1(c).

1. J. D. Wan, L. Shi, B. Benson, M. J. Bruzek, J. E. Anthony, P. J. Sinko, R. K. Prudhomme and H. A. Stone, *Langmuir*, 2012, **28**, 13143-13148.