

## **Supporting Information**

**for**

### **Semiconducting nanostructured copper sulfide thin films from bidentate copper(II) complexes of *N*-(dialkylcarbamoithiyl)-nitrosubstituted benzamides by chemical vapour deposition**

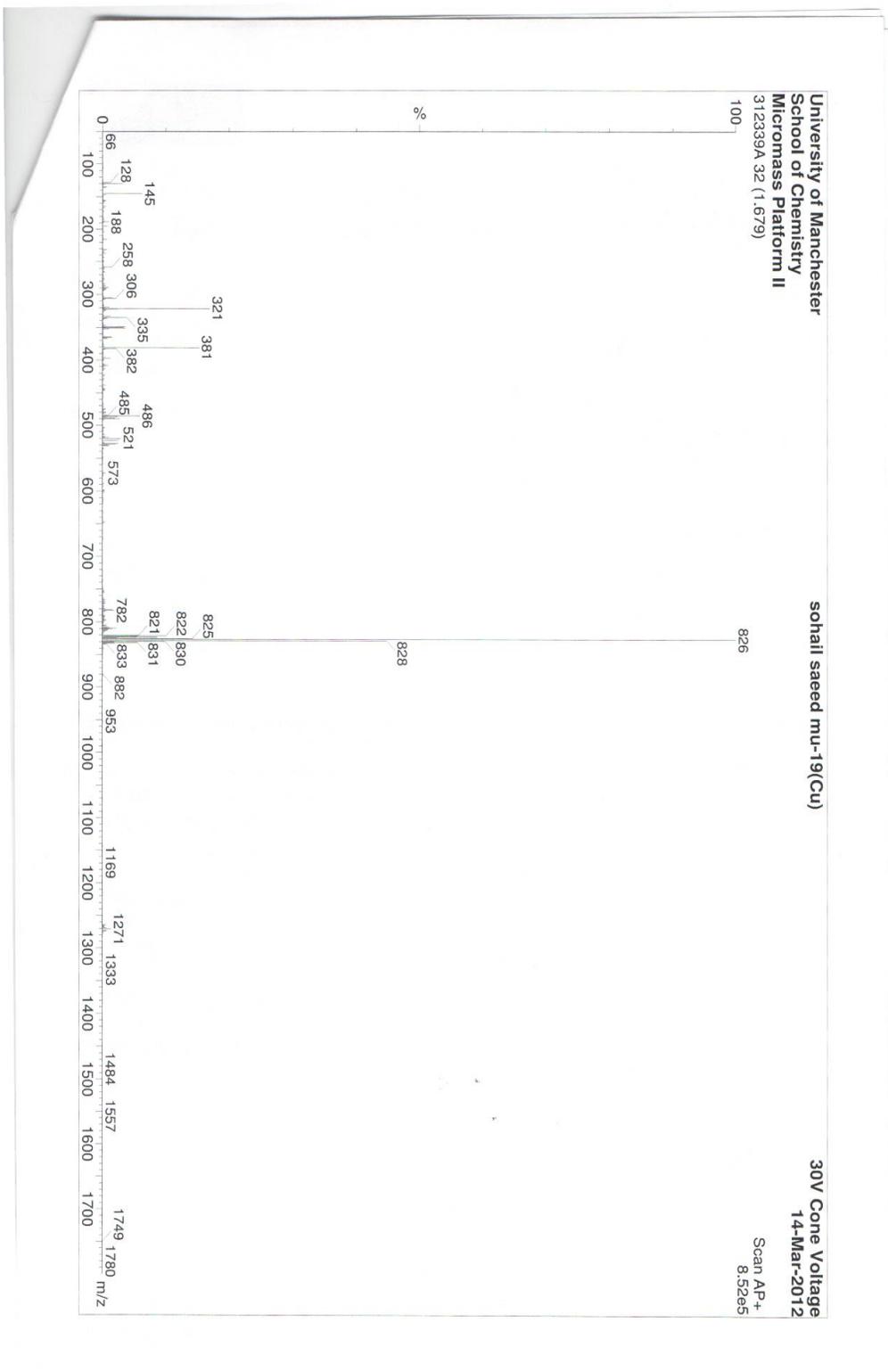
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**\*Corresponding author address:**

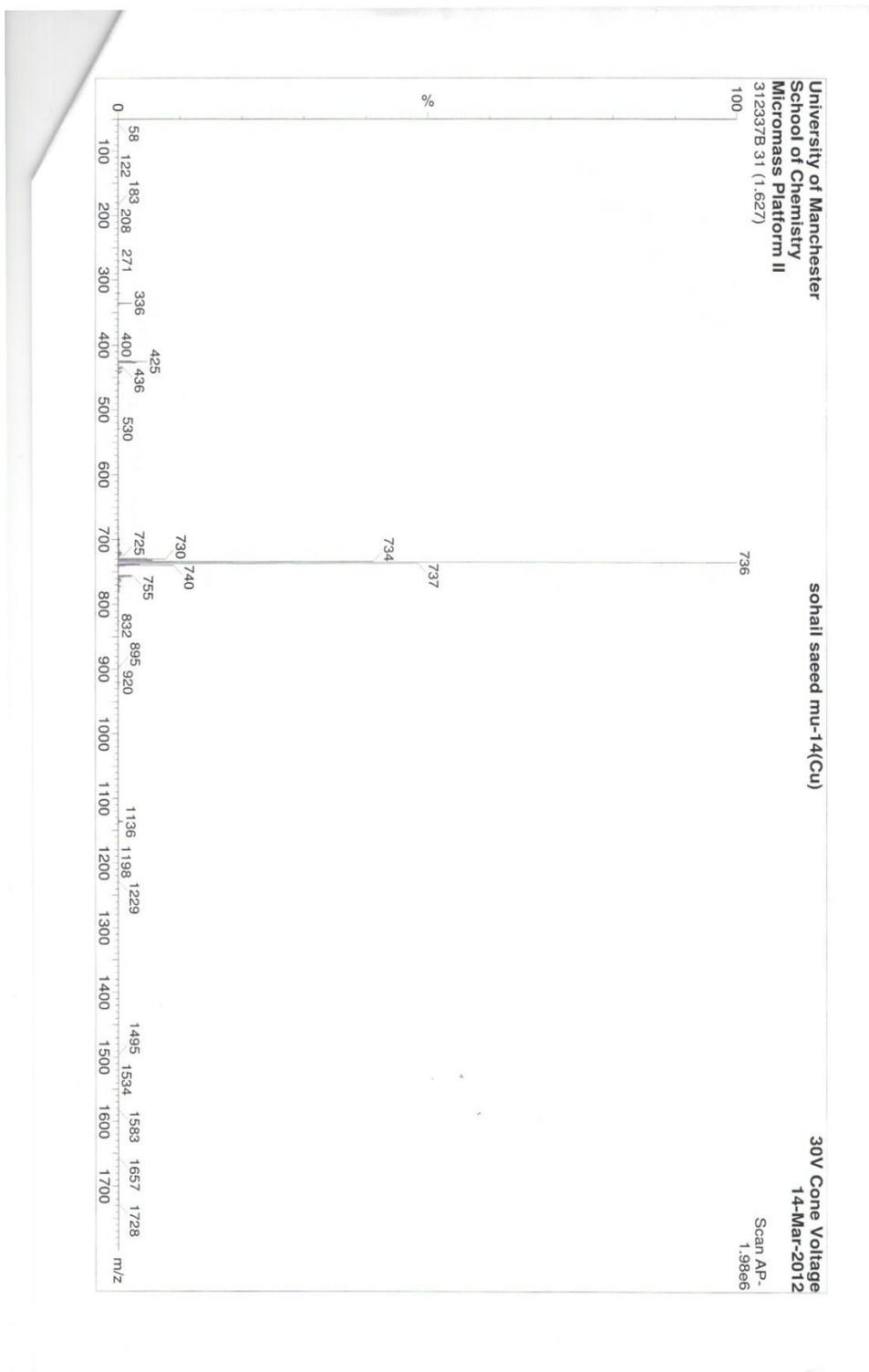
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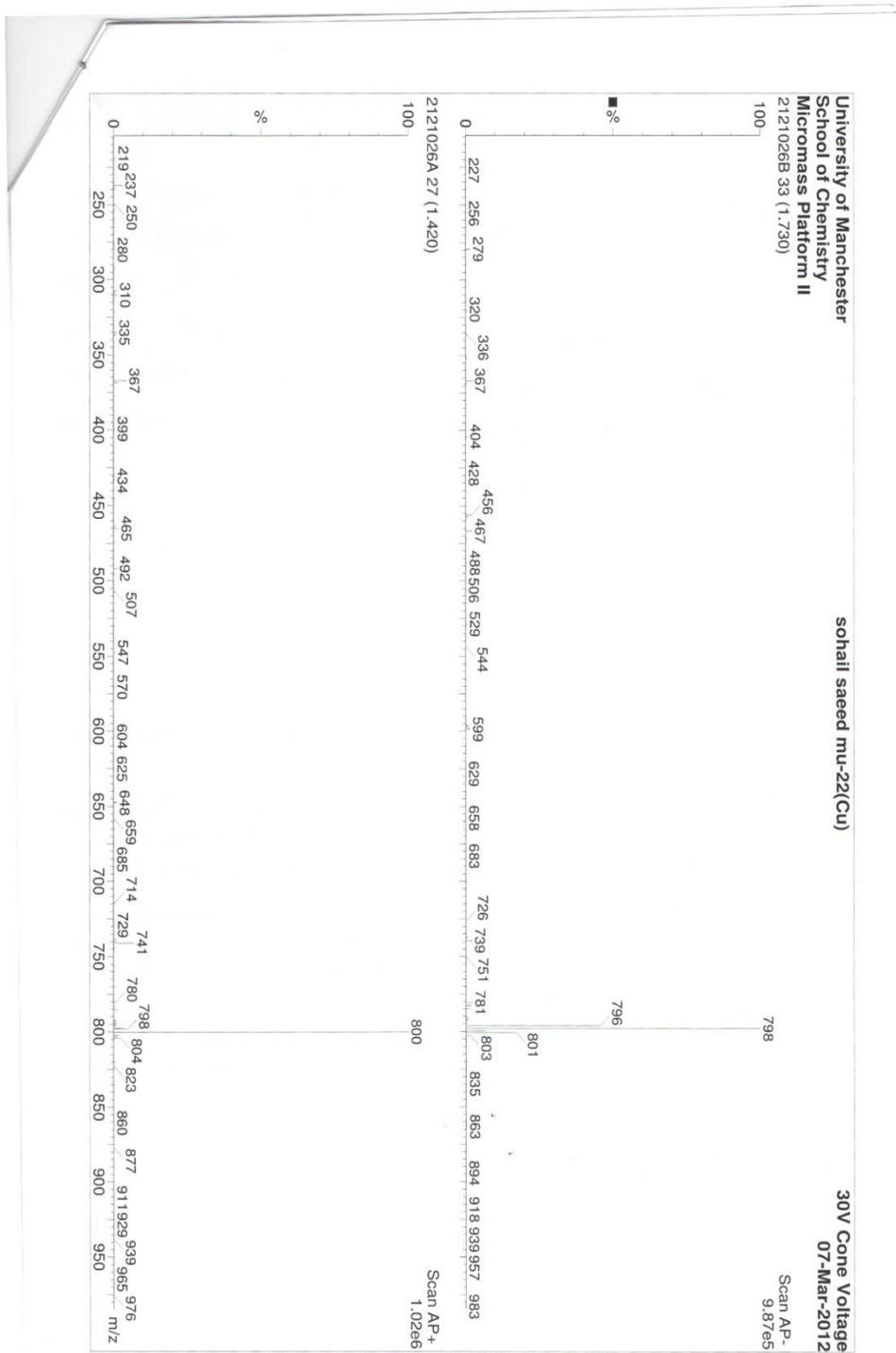
MS-APCI Spectra of copper complex (**1a**)



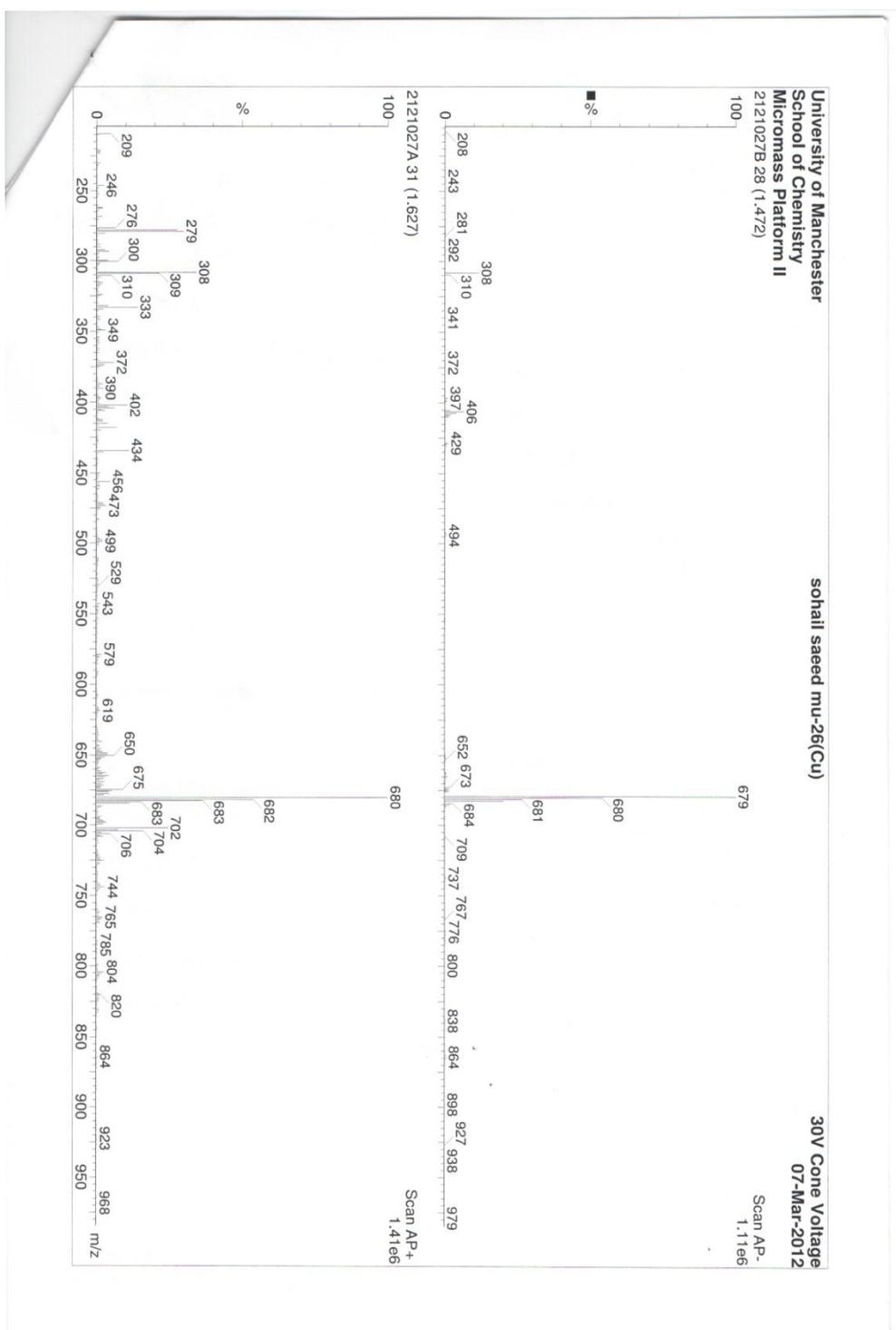
### MS-APCI Spectra of copper complex (2a)



MS-APCI Spectra of copper complex (3a)



### MS-APCI Spectra of copper complex (4a)



## X-Ray Crystallography of 2a

### Crystal data

$C_{32}H_{44}CuN_6O_6S_2$	$\gamma = 87.573 (4)^\circ$
$M_r = 736.39$	$V = 1828.8 (8) \text{ \AA}^3$
Triclinic, $P\bar{1}$	$Z = 2$
$a = 8.585 (2) \text{ \AA}$	Mo $K\alpha$ radiation, $\lambda = 0.71073 \text{ \AA}$
$b = 12.347 (3) \text{ \AA}$	$\mu = 0.76 \text{ mm}^{-1}$
$c = 17.326 (4) \text{ \AA}$	$T = 300 \text{ K}$
$\alpha = 85.325 (4)^\circ$	$0.50 \times 0.10 \times 0.08 \text{ mm}$
$\beta = 89.305 (4)^\circ$	

### Data collection

Bruker SMART 1000 CCD diffractometer	6286 independent reflections
Absorption correction: multi-scan <i>SADABS</i> (Sheldrick, 2004)	4382 reflections with $I > 2\sigma(I)$
$T_{\min} = 0.702$ , $T_{\max} = 0.942$	$R_{\text{int}} = 0.021$
10157 measured reflections	

### Refinement

Refinement on $F^2$	Primary atom site location: structure-invariant direct methods
Least-squares matrix: full	Secondary atom site location: difference Fourier map
$R[F^2 > 2\sigma(F^2)] = 0.049$	Hydrogen site location: inferred from neighbouring sites
$wR(F^2) = 0.119$	H-atom parameters constrained
$S = 1.05$	$w = 1/[\sigma^2(F_o^2) + (0.0411P)^2 + 1.3544P]$ where $P = (F_o^2 + 2F_c^2)/3$
6286 reflections	$(\Delta/\sigma)_{\max} = 0.002$
446 parameters	$\Delta\rho_{\max} = 0.41 \text{ e \AA}^{-3}$
6 restraints	$\Delta\rho_{\min} = -0.37 \text{ e \AA}^{-3}$

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters ( $\text{\AA}^2$ )

	x	y	z	$U_{\text{iso}}^*/U_{\text{eq}}$	Occ. (<1)
Cu1	0.13700 (5)	0.46084 (3)	0.08466 (2)	0.04884 (15)	
S1	0.10537 (12)	0.35834 (8)	-0.01477 (6)	0.0573 (3)	
S2	-0.02149 (12)	0.35095 (8)	0.15728 (5)	0.0584 (3)	
O1	0.2799 (3)	0.55317 (19)	0.02773 (14)	0.0556 (7)	
O2	0.6444 (5)	1.0128 (3)	-0.1032 (2)	0.1072 (13)	
O3	0.7362 (4)	0.9347 (3)	-0.2002 (2)	0.0937 (11)	
O4	0.1785 (3)	0.5477 (2)	0.17061 (14)	0.0615 (7)	
O5	0.2564 (7)	0.9794 (3)	0.3879 (2)	0.158 (2)	
O6	0.1703 (6)	0.8912 (3)	0.4863 (2)	0.1350 (17)	
N1	0.3386 (3)	0.4768 (2)	-0.08949 (16)	0.0477 (7)	
N2	0.6611 (4)	0.9342 (3)	-0.1404 (2)	0.0689 (10)	
N3	0.2607 (4)	0.3268 (2)	-0.14275 (17)	0.0533 (8)	
N4	0.0975 (4)	0.4442 (2)	0.28196 (16)	0.0529 (8)	
N5	0.2060 (6)	0.8989 (3)	0.4194 (2)	0.0879 (12)	
N6	0.0210 (4)	0.2716 (2)	0.30187 (17)	0.0566 (8)	
C1	0.3409 (4)	0.5504 (3)	-0.0388 (2)	0.0449 (8)	
C2	0.4328 (4)	0.6487 (3)	-0.06438 (19)	0.0451 (8)	
C3	0.4321 (4)	0.7354 (3)	-0.0188 (2)	0.0554 (10)	
H3	0.3799	0.7307	0.0286	0.066*	
C4	0.5076 (5)	0.8290 (3)	-0.0425 (2)	0.0604 (10)	
H4	0.5066	0.8876	-0.0120	0.073*	
C5	0.5846 (4)	0.8328 (3)	-0.1129 (2)	0.0520 (9)	
C6	0.5903 (5)	0.7477 (3)	-0.1587 (2)	0.0599 (10)	
H6	0.6447	0.7523	-0.2055	0.072*	
C7	0.5136 (4)	0.6545 (3)	-0.1341 (2)	0.0547 (10)	
H7	0.5163	0.5957	-0.1644	0.066*	
C8	0.2453 (4)	0.3926 (3)	-0.0842 (2)	0.0469 (9)	
C9	0.3776 (5)	0.3477 (3)	-0.2044 (2)	0.0728 (12)	
H9A	0.4111	0.2797	-0.2250	0.087*	
H9B	0.4680	0.3789	-0.1832	0.087*	

C10	0.3066 (7)	0.4283 (5)	-0.2713 (3)	0.1013 (17)	
H10A	0.2136	0.3976	-0.2902	0.122*	
H10B	0.2752	0.4961	-0.2499	0.122*	
C11	0.4100 (8)	0.4515 (6)	-0.3357 (4)	0.129 (2)	
H11A	0.4472	0.3839	-0.3556	0.155*	
H11B	0.4995	0.4879	-0.3183	0.155*	
C12	0.3297 (9)	0.5226 (5)	-0.3996 (3)	0.144 (3)	
H12A	0.3970	0.5290	-0.4442	0.216*	
H12B	0.3064	0.5934	-0.3823	0.216*	
H12C	0.2347	0.4905	-0.4129	0.216*	
C13	0.1529 (5)	0.2413 (3)	-0.1538 (2)	0.0582 (10)	
H13A	0.1441	0.2340	-0.2089	0.070*	
H13B	0.0507	0.2639	-0.1349	0.070*	
C14	0.1980 (5)	0.1303 (3)	-0.1138 (2)	0.0627 (11)	
H14A	0.2938	0.1026	-0.1367	0.075*	
H14B	0.2170	0.1376	-0.0595	0.075*	
C15	0.0708 (5)	0.0503 (3)	-0.1212 (3)	0.0693 (11)	
H15A	0.0531	0.0429	-0.1757	0.083*	
H15B	-0.0251	0.0792	-0.0993	0.083*	
C16	0.1094 (6)	-0.0615 (4)	-0.0811 (3)	0.0875 (15)	
H16A	0.0203	-0.1057	-0.0824	0.131*	
H16B	0.1368	-0.0543	-0.0283	0.131*	
H16C	0.1955	-0.0952	-0.1073	0.131*	
C17	0.1460 (4)	0.5324 (3)	0.2417 (2)	0.0482 (9)	
C18	0.1678 (4)	0.6266 (3)	0.28922 (19)	0.0450 (8)	
C19	0.2114 (4)	0.7257 (3)	0.2533 (2)	0.0529 (9)	
H19	0.2310	0.7322	0.2003	0.063*	
C20	0.2257 (5)	0.8142 (3)	0.2957 (2)	0.0613 (11)	
H20	0.2548	0.8804	0.2717	0.074*	
C21	0.1965 (5)	0.8033 (3)	0.3736 (2)	0.0607 (10)	
C22	0.1562 (6)	0.7062 (3)	0.4112 (2)	0.0734 (13)	
H22	0.1391	0.6999	0.4644	0.088*	

C23	0.1419 (5)	0.6188 (3)	0.3682 (2)	0.0681 (12)	
H23	0.1140	0.5526	0.3929	0.082*	
C24	0.0393 (4)	0.3581 (3)	0.2506 (2)	0.0494 (9)	
C25	0.0695 (5)	0.2742 (3)	0.3827 (2)	0.0663 (12)	
H25A	0.0123	0.2210	0.4147	0.080*	
H25B	0.0417	0.3454	0.3999	0.080*	
C26	0.2400 (6)	0.2512 (4)	0.3945 (2)	0.0788 (13)	
H26A	0.2975	0.3100	0.3688	0.095*	
H26B	0.2714	0.1847	0.3713	0.095*	
C27	0.2805 (8)	0.2393 (5)	0.4804 (3)	0.115 (2)	
H27A	0.2528	0.3072	0.5025	0.137*	
H27B	0.2173	0.1836	0.5061	0.137*	
C28	0.4432 (9)	0.2111 (6)	0.4967 (4)	0.153 (3)	
H28A	0.4603	0.2097	0.5514	0.230*	
H28B	0.5074	0.2643	0.4701	0.230*	
H28C	0.4697	0.1407	0.4793	0.230*	
C29	-0.0512 (5)	0.1721 (3)	0.2829 (2)	0.0672 (12)	
H29A	0.0009	0.1101	0.3112	0.081*	
H29B	-0.0373	0.1638	0.2280	0.081*	
C30	-0.2243 (6)	0.1730 (4)	0.3028 (3)	0.0814 (14)	0.782 (16)
H30A	-0.2357	0.1841	0.3574	0.098*	0.782 (16)
H30B	-0.2740	0.2356	0.2742	0.098*	0.782 (16)
C31	-0.3141 (11)	0.0744 (7)	0.2875 (5)	0.083 (3)	0.782 (16)
H31A	-0.4240	0.0891	0.2977	0.099*	0.782 (16)
H31B	-0.3023	0.0607	0.2334	0.099*	0.782 (16)
C32	-0.2593 (15)	-0.0244 (7)	0.3367 (5)	0.121 (5)	0.782 (16)
H32A	-0.3195	-0.0850	0.3257	0.181*	0.782 (16)
H32B	-0.2719	-0.0115	0.3904	0.181*	0.782 (16)
H32C	-0.1512	-0.0404	0.3258	0.181*	0.782 (16)
C30'	-0.2243 (6)	0.1730 (4)	0.3028 (3)	0.0814 (14)	0.218 (16)
H30C	-0.2872	0.2120	0.2626	0.098*	0.218 (16)
H30D	-0.2471	0.2021	0.3522	0.098*	0.218 (16)

C31'	-0.244 (4)	0.038 (3)	0.3063 (19)	0.079 (10)	0.218 (16)
H31C	-0.2189	0.0104	0.2566	0.095*	0.218 (16)
H31D	-0.1777	0.0004	0.3455	0.095*	0.218 (16)
C32'	-0.415 (4)	0.023 (3)	0.3266 (18)	0.130 (15)	0.218 (16)
H32D	-0.4386	-0.0522	0.3254	0.195*	0.218 (16)
H32E	-0.4793	0.0664	0.2898	0.195*	0.218 (16)
H32F	-0.4363	0.0456	0.3776	0.195*	0.218 (16)

### Atomic displacement parameters (Å<sup>2</sup>)

	$U^{11}$	$U^{22}$	$U^{33}$	$U^{12}$	$U^{13}$	$U^{23}$
Cu1	0.0560 (3)	0.0459 (3)	0.0456 (3)	-0.0145 (2)	0.0076 (2)	-0.00487 (19)
S1	0.0615 (6)	0.0526 (6)	0.0607 (6)	-0.0213 (5)	0.0132 (5)	-0.0149 (5)
S2	0.0679 (7)	0.0570 (6)	0.0511 (6)	-0.0247 (5)	0.0017 (5)	0.0018 (4)
O1	0.0652 (17)	0.0548 (16)	0.0491 (15)	-0.0245 (13)	0.0126 (13)	-0.0093 (12)
O2	0.136 (3)	0.065 (2)	0.125 (3)	-0.044 (2)	0.040 (2)	-0.020 (2)
O3	0.116 (3)	0.076 (2)	0.088 (2)	-0.0336 (19)	0.031 (2)	0.0099 (17)
O4	0.087 (2)	0.0543 (16)	0.0459 (15)	-0.0288 (14)	0.0144 (13)	-0.0078 (12)
O5	0.329 (7)	0.059 (2)	0.091 (3)	-0.055 (3)	-0.011 (3)	-0.010 (2)
O6	0.230 (5)	0.100 (3)	0.084 (3)	-0.050 (3)	0.036 (3)	-0.045 (2)
N1	0.0491 (18)	0.0453 (18)	0.0487 (17)	-0.0070 (14)	0.0036 (14)	-0.0023 (14)
N2	0.072 (2)	0.056 (2)	0.078 (3)	-0.0201 (18)	0.005 (2)	0.0060 (19)
N3	0.058 (2)	0.0482 (19)	0.0552 (19)	-0.0073 (15)	0.0060 (15)	-0.0120 (15)
N4	0.071 (2)	0.0414 (18)	0.0468 (17)	-0.0119 (15)	0.0033 (15)	-0.0006 (14)
N5	0.136 (4)	0.061 (3)	0.070 (3)	-0.018 (2)	-0.007 (3)	-0.011 (2)
N6	0.081 (2)	0.0415 (18)	0.0475 (18)	-0.0148 (16)	0.0035 (16)	-0.0002 (14)
C1	0.040 (2)	0.043 (2)	0.050 (2)	-0.0013 (16)	-0.0017 (16)	0.0018 (17)
C2	0.043 (2)	0.043 (2)	0.049 (2)	-0.0083 (16)	0.0015 (16)	0.0009 (16)
C3	0.060 (2)	0.056 (2)	0.051 (2)	-0.0129 (19)	0.0100 (18)	-0.0020 (18)
C4	0.067 (3)	0.052 (2)	0.064 (3)	-0.014 (2)	0.004 (2)	-0.0107 (19)
C5	0.052 (2)	0.044 (2)	0.059 (2)	-0.0149 (17)	-0.0033 (18)	0.0057 (18)
C6	0.065 (3)	0.059 (3)	0.055 (2)	-0.010 (2)	0.014 (2)	0.0003 (19)
C7	0.062 (2)	0.048 (2)	0.055 (2)	-0.0082 (18)	0.0097 (19)	-0.0066 (17)

C8	0.045 (2)	0.045 (2)	0.050 (2)	-0.0009 (17)	-0.0025 (16)	-0.0016 (17)
C9	0.081 (3)	0.065 (3)	0.075 (3)	-0.010 (2)	0.023 (2)	-0.023 (2)
C10	0.115 (4)	0.113 (4)	0.075 (3)	-0.002 (3)	0.023 (3)	-0.004 (3)
C11	0.138 (6)	0.134 (6)	0.113 (5)	0.006 (4)	0.031 (4)	-0.001 (4)
C12	0.199 (8)	0.128 (6)	0.099 (5)	0.015 (5)	0.008 (5)	0.017 (4)
C13	0.064 (3)	0.058 (3)	0.055 (2)	-0.009 (2)	-0.0028 (19)	-0.0196 (19)
C14	0.066 (3)	0.051 (2)	0.073 (3)	-0.001 (2)	-0.006 (2)	-0.015 (2)
C15	0.078 (3)	0.062 (3)	0.071 (3)	-0.015 (2)	0.001 (2)	-0.012 (2)
C16	0.118 (4)	0.063 (3)	0.083 (3)	-0.016 (3)	-0.001 (3)	-0.007 (2)
C17	0.050 (2)	0.046 (2)	0.049 (2)	-0.0060 (17)	0.0020 (17)	-0.0028 (17)
C18	0.047 (2)	0.040 (2)	0.048 (2)	-0.0070 (16)	-0.0008 (16)	-0.0022 (15)
C19	0.064 (3)	0.049 (2)	0.045 (2)	-0.0109 (19)	0.0009 (18)	0.0017 (17)
C20	0.083 (3)	0.042 (2)	0.059 (2)	-0.016 (2)	-0.006 (2)	0.0046 (18)
C21	0.079 (3)	0.046 (2)	0.059 (2)	-0.012 (2)	-0.004 (2)	-0.0111 (18)
C22	0.114 (4)	0.062 (3)	0.047 (2)	-0.026 (3)	0.012 (2)	-0.009 (2)
C23	0.103 (3)	0.050 (2)	0.052 (2)	-0.026 (2)	0.015 (2)	-0.0021 (19)
C24	0.055 (2)	0.040 (2)	0.052 (2)	-0.0087 (17)	0.0080 (17)	0.0008 (16)
C25	0.098 (4)	0.051 (2)	0.049 (2)	-0.020 (2)	0.003 (2)	0.0039 (18)
C26	0.110 (4)	0.060 (3)	0.065 (3)	-0.008 (3)	-0.012 (3)	0.005 (2)
C27	0.119 (5)	0.128 (5)	0.095 (4)	-0.003 (4)	-0.027 (4)	0.003 (4)
C28	0.146 (7)	0.183 (8)	0.129 (6)	-0.031 (6)	-0.035 (5)	0.018 (5)
C29	0.097 (3)	0.043 (2)	0.062 (3)	-0.015 (2)	0.012 (2)	-0.0021 (18)
C30	0.096 (4)	0.076 (3)	0.074 (3)	-0.028 (3)	0.016 (3)	-0.005 (2)
C31	0.086 (6)	0.086 (6)	0.077 (5)	-0.031 (5)	0.011 (4)	-0.005 (4)
C32	0.192 (12)	0.073 (6)	0.099 (6)	-0.057 (6)	0.007 (6)	0.005 (4)
C30'	0.096 (4)	0.076 (3)	0.074 (3)	-0.028 (3)	0.016 (3)	-0.005 (2)
C31'	0.077 (13)	0.077 (13)	0.083 (12)	-0.011 (9)	-0.001 (9)	-0.004 (9)
C32'	0.08 (3)	0.18 (3)	0.13 (2)	-0.06 (2)	0.011 (18)	0.01 (2)

### Geometric parameters (Å, °)

Cu1—O1	1.919 (2)	C14—C15	1.517 (5)
Cu1—O4	1.949 (2)	C14—H14A	0.9700
Cu1—S1	2.2448 (11)	C14—H14B	0.9700
Cu1—S2	2.2610 (10)	C15—C16	1.519 (6)
S1—C8	1.731 (4)	C15—H15A	0.9700
S2—C24	1.715 (4)	C15—H15B	0.9700
O1—C1	1.262 (4)	C16—H16A	0.9600
O2—N2	1.212 (4)	C16—H16B	0.9600
O3—N2	1.212 (4)	C16—H16C	0.9600
O4—C17	1.260 (4)	C17—C18	1.498 (5)
O5—N5	1.190 (5)	C18—C23	1.380 (5)
O6—N5	1.192 (5)	C18—C19	1.391 (5)
N1—C1	1.316 (4)	C19—C20	1.376 (5)
N1—C8	1.335 (4)	C19—H19	0.9300
N2—C5	1.480 (5)	C20—C21	1.366 (5)
N3—C8	1.351 (4)	C20—H20	0.9300
N3—C13	1.459 (5)	C21—C22	1.372 (5)
N3—C9	1.472 (5)	C22—C23	1.370 (5)
N4—C17	1.324 (4)	C22—H22	0.9300
N4—C24	1.350 (4)	C23—H23	0.9300
N5—C21	1.482 (5)	C25—C26	1.493 (6)
N6—C24	1.346 (4)	C25—H25A	0.9700
N6—C29	1.462 (5)	C25—H25B	0.9700
N6—C25	1.468 (5)	C26—C27	1.526 (6)
C1—C2	1.509 (5)	C26—H26A	0.9700
C2—C3	1.380 (5)	C26—H26B	0.9700
C2—C7	1.383 (5)	C27—C28	1.451 (8)
C3—C4	1.380 (5)	C27—H27A	0.9700
C3—H3	0.9300	C27—H27B	0.9700
C4—C5	1.378 (5)	C28—H28A	0.9600
C4—H4	0.9300	C28—H28B	0.9600

C5—C6	1.367 (5)	C28—H28C	0.9600
C6—C7	1.385 (5)	C29—C30	1.522 (6)
C6—H6	0.9300	C29—H29A	0.9700
C7—H7	0.9300	C29—H29B	0.9700
C9—C10	1.576 (6)	C30—C31	1.510 (8)
C9—H9A	0.9700	C30—H30A	0.9700
C9—H9B	0.9700	C30—H30B	0.9700
C10—C11	1.434 (7)	C31—C32	1.494 (16)
C10—H10A	0.9700	C31—H31A	0.9700
C10—H10B	0.9700	C31—H31B	0.9700
C11—C12	1.510 (8)	C32—H32A	0.9600
C11—H11A	0.9700	C32—H32B	0.9600
C11—H11B	0.9700	C32—H32C	0.9600
C12—H12A	0.9600	C31'—C32'	1.52 (5)
C12—H12B	0.9600	C31'—H31C	0.9700
C12—H12C	0.9600	C31'—H31D	0.9700
C13—C14	1.521 (5)	C32'—H32D	0.9600
C13—H13A	0.9700	C32'—H32E	0.9600
C13—H13B	0.9700	C32'—H32F	0.9600
O1—Cu1—O4	84.88 (10)	H15A—C15—H15B	107.7
O1—Cu1—S1	93.14 (8)	C15—C16—H16A	109.5
O4—Cu1—S1	176.40 (9)	C15—C16—H16B	109.5
O1—Cu1—S2	176.75 (9)	H16A—C16—H16B	109.5
O4—Cu1—S2	92.89 (8)	C15—C16—H16C	109.5
S1—Cu1—S2	88.96 (4)	H16A—C16—H16C	109.5
C8—S1—Cu1	107.78 (13)	H16B—C16—H16C	109.5
C24—S2—Cu1	104.65 (12)	O4—C17—N4	129.9 (3)
C1—O1—Cu1	132.5 (2)	O4—C17—C18	116.1 (3)
C17—O4—Cu1	130.7 (2)	N4—C17—C18	114.0 (3)
C1—N1—C8	124.2 (3)	C23—C18—C19	118.5 (3)
O3—N2—O2	123.1 (4)	C23—C18—C17	121.7 (3)

O3—N2—C5	118.0 (4)	C19—C18—C17	119.8 (3)
O2—N2—C5	118.9 (4)	C20—C19—C18	120.4 (3)
C8—N3—C13	122.7 (3)	C20—C19—H19	119.8
C8—N3—C9	120.5 (3)	C18—C19—H19	119.8
C13—N3—C9	116.4 (3)	C21—C20—C19	119.1 (3)
C17—N4—C24	124.6 (3)	C21—C20—H20	120.5
O5—N5—O6	122.8 (4)	C19—C20—H20	120.5
O5—N5—C21	117.6 (4)	C20—C21—C22	122.0 (4)
O6—N5—C21	119.6 (4)	C20—C21—N5	119.6 (4)
C24—N6—C29	123.6 (3)	C22—C21—N5	118.3 (4)
C24—N6—C25	120.7 (3)	C23—C22—C21	118.3 (4)
C29—N6—C25	115.8 (3)	C23—C22—H22	120.9
O1—C1—N1	131.3 (3)	C21—C22—H22	120.9
O1—C1—C2	114.3 (3)	C22—C23—C18	121.6 (4)
N1—C1—C2	114.5 (3)	C22—C23—H23	119.2
C3—C2—C7	119.7 (3)	C18—C23—H23	119.2
C3—C2—C1	119.5 (3)	N6—C24—N4	113.6 (3)
C7—C2—C1	120.8 (3)	N6—C24—S2	118.6 (3)
C4—C3—C2	121.0 (3)	N4—C24—S2	127.7 (3)
C4—C3—H3	119.5	N6—C25—C26	113.6 (3)
C2—C3—H3	119.5	N6—C25—H25A	108.8
C3—C4—C5	117.9 (4)	C26—C25—H25A	108.8
C3—C4—H4	121.1	N6—C25—H25B	108.8
C5—C4—H4	121.1	C26—C25—H25B	108.8
C6—C5—C4	122.6 (3)	H25A—C25—H25B	107.7
C6—C5—N2	118.9 (3)	C25—C26—C27	111.5 (4)
C4—C5—N2	118.5 (4)	C25—C26—H26A	109.3
C5—C6—C7	118.7 (3)	C27—C26—H26A	109.3
C5—C6—H6	120.6	C25—C26—H26B	109.3
C7—C6—H6	120.6	C27—C26—H26B	109.3
C2—C7—C6	120.1 (4)	H26A—C26—H26B	108.0
C2—C7—H7	120.0	C28—C27—C26	114.6 (6)

C6—C7—H7	120.0	C28—C27—H27A	108.6
N1—C8—N3	114.8 (3)	C26—C27—H27A	108.6
N1—C8—S1	129.2 (3)	C28—C27—H27B	108.6
N3—C8—S1	116.0 (3)	C26—C27—H27B	108.6
N3—C9—C10	110.2 (4)	H27A—C27—H27B	107.6
N3—C9—H9A	109.6	C27—C28—H28A	109.5
C10—C9—H9A	109.6	C27—C28—H28B	109.5
N3—C9—H9B	109.6	H28A—C28—H28B	109.5
C10—C9—H9B	109.6	C27—C28—H28C	109.5
H9A—C9—H9B	108.1	H28A—C28—H28C	109.5
C11—C10—C9	114.7 (5)	H28B—C28—H28C	109.5
C11—C10—H10A	108.6	N6—C29—C30	112.2 (3)
C9—C10—H10A	108.6	N6—C29—H29A	109.2
C11—C10—H10B	108.6	C30—C29—H29A	109.2
C9—C10—H10B	108.6	N6—C29—H29B	109.2
H10A—C10—H10B	107.6	C30—C29—H29B	109.2
C10—C11—C12	111.4 (6)	H29A—C29—H29B	107.9
C10—C11—H11A	109.3	C31—C30—C29	118.2 (5)
C12—C11—H11A	109.3	C31—C30—H30A	107.8
C10—C11—H11B	109.3	C29—C30—H30A	107.8
C12—C11—H11B	109.3	C31—C30—H30B	107.8
H11A—C11—H11B	108.0	C29—C30—H30B	107.8
C11—C12—H12A	109.5	H30A—C30—H30B	107.1
C11—C12—H12B	109.5	C32—C31—C30	112.0 (8)
H12A—C12—H12B	109.5	C32—C31—H31A	109.2
C11—C12—H12C	109.5	C30—C31—H31A	109.2
H12A—C12—H12C	109.5	C32—C31—H31B	109.2
H12B—C12—H12C	109.5	C30—C31—H31B	109.2
N3—C13—C14	115.2 (3)	H31A—C31—H31B	107.9
N3—C13—H13A	108.5	C31—C32—H32A	109.5
C14—C13—H13A	108.5	C31—C32—H32B	109.5
N3—C13—H13B	108.5	H32A—C32—H32B	109.5

C14—C13—H13B	108.5	C31—C32—H32C	109.5
H13A—C13—H13B	107.5	H32A—C32—H32C	109.5
C15—C14—C13	111.3 (3)	H32B—C32—H32C	109.5
C15—C14—H14A	109.4	C32'—C31'—H31C	110.9
C13—C14—H14A	109.4	C32'—C31'—H31D	110.9
C15—C14—H14B	109.4	H31C—C31'—H31D	108.9
C13—C14—H14B	109.4	C31'—C32'—H32D	109.5
H14A—C14—H14B	108.0	C31'—C32'—H32E	109.5
C14—C15—C16	113.3 (4)	H32D—C32'—H32E	109.5
C14—C15—H15A	108.9	C31'—C32'—H32F	109.5
C16—C15—H15A	108.9	H32D—C32'—H32F	109.5
C14—C15—H15B	108.9	H32E—C32'—H32F	109.5

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TITL wt2335w-SS-MU-14Cu_SohailSaeed_10-April-2012
CELL 0.71073 8.58490 12.34710 17.32640 85.325 89.305 87.573
ZERR 2 0.00210 0.00290 0.00410 0.004 0.004 0.004
LATT 1
SFAC N O C H CU S
UNIT 12 12 64 88 2 4
SHEL 8.000000 0.84
OMIT -2 5 2
OMIT 1 -4 3
OMIT 0 8 5
OMIT 1 -5 9
OMIT -7 -3 9
OMIT 7 6 4
OMIT -5 10 10
OMIT -1 -14 11
OMIT -9 -2 15
OMIT -8 -2 17
OMIT 10 -5 5
OMIT 7 0 9
OMIT -6 -11 2
OMIT 0 -12 9
OMIT 4 -5 15
OMIT -4 6 17
L.S. 6
FMAP 2
PLAN -20
BOND $H
HTAB
TEMP 27.0
EADP C30 C30'
EXYZ C30 C30'
ISOR 0.01 0.02 C31'
MPLA 3 N2 O2 O3
MPLA 6 C2 C3 C4 C5 C6 C7
MPLA 6 Cu1 S1 C8 N1 C1 O1
MPLA 6 Cu1 S2 C24 N4 C17 O4
MPLA 6 C18 C19 C20 C21 C22 C23
MPLA 3 N5 O5 O6
ACTA
SIZE 0.500 0.100 0.080
LIST 4
WGHT 0.041100 1.354400
FVAR 0.34457 0.78228
CU1 5 0.137004 0.460838 0.084659 11.00000 0.05604
0.04594 =
0.04559 -0.00487 0.00761 -0.01450
S1 6 0.105367 0.358342 -0.014773 11.00000 0.06151
0.05259 =
0.06066 -0.01494 0.01322 -0.02126
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S2	6	-0.021492	0.350948	0.157281	11.00000	0.06787
0.05703	=					
		0.05106	0.00180	0.00170	-0.02466	
O1	2	0.279900	0.553167	0.027728	11.00000	0.06518
0.05483	=					
		0.04906	-0.00931	0.01261	-0.02451	
O2	2	0.644444	1.012824	-0.103167	11.00000	0.13605
0.06512	=					
		0.12487	-0.02044	0.04015	-0.04435	
O3	2	0.736184	0.934661	-0.200181	11.00000	0.11626
0.07580	=					
		0.08815	0.00989	0.03131	-0.03356	
O4	2	0.178505	0.547700	0.170606	11.00000	0.08687
0.05427	=					
		0.04586	-0.00785	0.01441	-0.02879	
O5	2	0.256401	0.979408	0.387929	11.00000	0.32923
0.05896	=					
		0.09083	-0.00983	-0.01121	-0.05510	
O6	2	0.170277	0.891231	0.486291	11.00000	0.23050
0.09959	=					
		0.08393	-0.04538	0.03568	-0.04976	
N1	1	0.338602	0.476768	-0.089490	11.00000	0.04914
0.04528	=					
		0.04868	-0.00234	0.00364	-0.00702	
N2	1	0.661088	0.934178	-0.140443	11.00000	0.07206
0.05571	=					
		0.07846	0.00602	0.00543	-0.02012	
N3	1	0.260669	0.326835	-0.142748	11.00000	0.05808
0.04822	=					
		0.05524	-0.01196	0.00602	-0.00732	
N4	1	0.097533	0.444244	0.281955	11.00000	0.07057
0.04145	=					
		0.04681	-0.00060	0.00327	-0.01189	
N5	1	0.205981	0.898918	0.419430	11.00000	0.13581
0.06060	=					
		0.06970	-0.01142	-0.00702	-0.01796	
N6	1	0.020980	0.271639	0.301875	11.00000	0.08130
0.04155	=					
		0.04749	-0.00025	0.00350	-0.01481	
C1	3	0.340900	0.550426	-0.038751	11.00000	0.04046
0.04338	=					
		0.04991	0.00180	-0.00165	-0.00134	
C2	3	0.432815	0.648748	-0.064383	11.00000	0.04346
0.04255	=					
		0.04892	0.00086	0.00147	-0.00833	
C3	3	0.432088	0.735416	-0.018827	11.00000	0.05975
0.05570	=					
		0.05101	-0.00203	0.00995	-0.01288	
AFIX	43					
H3	4	0.379863	0.730665	0.028592	11.00000	-1.20000
AFIX	0					
C4	3	0.507627	0.828991	-0.042533	11.00000	0.06747
0.05171	=					
		0.06401	-0.01069	0.00353	-0.01400	

AFIX	43					
H4	4	0.506602	0.887586	-0.012010	11.00000	-1.20000
AFIX	0					
C5	3	0.584615	0.832840	-0.112869	11.00000	0.05172
0.04443	=					
		0.05928	0.00568	-0.00326	-0.01494	
C6	3	0.590328	0.747719	-0.158694	11.00000	0.06521
0.05932	=					
		0.05459	0.00026	0.01397	-0.01003	
AFIX	43					
H6	4	0.644716	0.752312	-0.205515	11.00000	-1.20000
AFIX	0					
C7	3	0.513559	0.654461	-0.134071	11.00000	0.06194
0.04821	=					
		0.05470	-0.00658	0.00972	-0.00821	
AFIX	43					
H7	4	0.516318	0.595652	-0.164424	11.00000	-1.20000
AFIX	0					
C8	3	0.245324	0.392583	-0.084230	11.00000	0.04546
0.04527	=					
		0.04956	-0.00165	-0.00249	-0.00089	
C9	3	0.377579	0.347688	-0.204407	11.00000	0.08100
0.06513	=					
		0.07519	-0.02294	0.02272	-0.00992	
AFIX	23					
H9A	4	0.411051	0.279706	-0.225037	11.00000	-1.20000
H9B	4	0.467985	0.378878	-0.183206	11.00000	-1.20000
AFIX	0					
C10	3	0.306622	0.428273	-0.271332	11.00000	0.11466
0.11254	=					
		0.07541	-0.00396	0.02317	-0.00224	
AFIX	23					
H10A	4	0.213578	0.397550	-0.290190	11.00000	-1.20000
H10B	4	0.275218	0.496127	-0.249948	11.00000	-1.20000
AFIX	0					
C11	3	0.409998	0.451511	-0.335658	11.00000	0.13781
0.13418	=					
		0.11289	-0.00098	0.03116	0.00558	
AFIX	23					
H11A	4	0.447202	0.383853	-0.355590	11.00000	-1.20000
H11B	4	0.499546	0.487934	-0.318277	11.00000	-1.20000
AFIX	0					
C12	3	0.329707	0.522576	-0.399567	11.00000	0.19925
0.12800	=					
		0.09905	0.01713	0.00796	0.01512	
AFIX	137					
H12A	4	0.397000	0.528973	-0.444219	11.00000	-1.50000
H12B	4	0.306370	0.593417	-0.382257	11.00000	-1.50000
H12C	4	0.234705	0.490519	-0.412855	11.00000	-1.50000
AFIX	0					
C13	3	0.152884	0.241300	-0.153783	11.00000	0.06422
0.05826	=					
		0.05522	-0.01962	-0.00275	-0.00856	
AFIX	23					

H13A	4	0.144137	0.234019	-0.208867	11.00000	-1.20000
H13B	4	0.050735	0.263918	-0.134930	11.00000	-1.20000
AFIX	0					
C14	3	0.198017	0.130327	-0.113826	11.00000	0.06555
0.05127 =						
		0.07298	-0.01470	-0.00590	-0.00077	
AFIX	23					
H14A	4	0.293789	0.102622	-0.136730	11.00000	-1.20000
H14B	4	0.216980	0.137638	-0.059457	11.00000	-1.20000
AFIX	0					
C15	3	0.070826	0.050261	-0.121203	11.00000	0.07781
0.06179 =						
		0.07060	-0.01230	0.00078	-0.01544	
AFIX	23					
H15A	4	0.053073	0.042928	-0.175678	11.00000	-1.20000
H15B	4	-0.025126	0.079246	-0.099251	11.00000	-1.20000
AFIX	0					
C16	3	0.109423	-0.061509	-0.081120	11.00000	0.11781
0.06259 =						
		0.08340	-0.00655	-0.00077	-0.01631	
AFIX	137					
H16A	4	0.020295	-0.105708	-0.082425	11.00000	-1.50000
H16B	4	0.136844	-0.054295	-0.028287	11.00000	-1.50000
H16C	4	0.195524	-0.095162	-0.107314	11.00000	-1.50000
AFIX	0					
C17	3	0.146006	0.532376	0.241672	11.00000	0.05005
0.04586 =						
		0.04875	-0.00281	0.00203	-0.00597	
C18	3	0.167830	0.626557	0.289219	11.00000	0.04743
0.03984 =						
		0.04799	-0.00222	-0.00079	-0.00703	
C19	3	0.211389	0.725681	0.253303	11.00000	0.06445
0.04940 =						
		0.04462	0.00173	0.00095	-0.01088	
AFIX	43					
H19	4	0.230975	0.732209	0.200255	11.00000	-1.20000
AFIX	0					
C20	3	0.225703	0.814152	0.295715	11.00000	0.08252
0.04178 =						
		0.05939	0.00465	-0.00625	-0.01598	
AFIX	43					
H20	4	0.254840	0.880445	0.271707	11.00000	-1.20000
AFIX	0					
C21	3	0.196528	0.803272	0.373568	11.00000	0.07924
0.04620 =						
		0.05873	-0.01115	-0.00359	-0.01177	
C22	3	0.156224	0.706178	0.411163	11.00000	0.11414
0.06198 =						
		0.04652	-0.00900	0.01220	-0.02616	
AFIX	43					
H22	4	0.139085	0.699859	0.464412	11.00000	-1.20000
AFIX	0					
C23	3	0.141888	0.618774	0.368204	11.00000	0.10287
0.05049 =						

		0.05222	-0.00211	0.01468	-0.02614	
AFIX	43					
H23	4	0.113996	0.552598	0.392881	11.00000	-1.20000
AFIX	0					
C24	3	0.039257	0.358130	0.250582	11.00000	0.05535
0.04020	=					
		0.05227	0.00080	0.00804	-0.00868	
C25	3	0.069451	0.274236	0.382658	11.00000	0.09835
0.05110	=					
		0.04949	0.00393	0.00337	-0.01988	
AFIX	23					
H25A	4	0.012306	0.221045	0.414668	11.00000	-1.20000
H25B	4	0.041680	0.345396	0.399863	11.00000	-1.20000
AFIX	0					
C26	3	0.240025	0.251214	0.394529	11.00000	0.11048
0.05980	=					
		0.06530	0.00451	-0.01237	-0.00828	
AFIX	23					
H26A	4	0.297505	0.309996	0.368827	11.00000	-1.20000
H26B	4	0.271376	0.184735	0.371286	11.00000	-1.20000
AFIX	0					
C27	3	0.280493	0.239283	0.480401	11.00000	0.11897
0.12786	=					
		0.09525	0.00299	-0.02707	-0.00267	
AFIX	23					
H27A	4	0.252785	0.307246	0.502519	11.00000	-1.20000
H27B	4	0.217285	0.183630	0.506113	11.00000	-1.20000
AFIX	0					
C28	3	0.443221	0.211116	0.496665	11.00000	0.14621
0.18280	=					
		0.12883	0.01833	-0.03509	-0.03070	
AFIX	137					
H28A	4	0.460304	0.209722	0.551397	11.00000	-1.50000
H28B	4	0.507376	0.264259	0.470054	11.00000	-1.50000
H28C	4	0.469670	0.140727	0.479306	11.00000	-1.50000
AFIX	0					
C29	3	-0.051184	0.172113	0.282917	11.00000	0.09662
0.04338	=					
		0.06206	-0.00212	0.01172	-0.01456	
AFIX	23					
H29A	4	0.000945	0.110117	0.311158	11.00000	-1.20000
H29B	4	-0.037338	0.163833	0.228034	11.00000	-1.20000
AFIX	0					
PART	1					
C30	3	-0.224338	0.172959	0.302775	21.00000	0.09596
0.07577	=					
		0.07387	-0.00478	0.01614	-0.02817	
AFIX	23					
H30A	4	-0.235693	0.184076	0.357369	21.00000	-1.20000
H30B	4	-0.273962	0.235640	0.274162	21.00000	-1.20000
AFIX	0					
C31	3	-0.314081	0.074431	0.287502	21.00000	0.08639
0.08631	=					
		0.07714	-0.00518	0.01112	-0.03063	

```
AFIX 23
H31A 4 -0.423986 0.089143 0.297662 21.00000 -1.20000
H31B 4 -0.302284 0.060686 0.233371 21.00000 -1.20000
AFIX 0
C32 3 -0.259269 -0.024432 0.336743 21.00000 0.19249
0.07277 =
0.09942 0.00533 0.00699 -0.05704
AFIX 33
H32A 4 -0.319475 -0.084983 0.325651 21.00000 -1.50000
H32B 4 -0.271899 -0.011451 0.390384 21.00000 -1.50000
H32C 4 -0.151201 -0.040407 0.325845 21.00000 -1.50000
AFIX 0
PART 2
C30' 3 -0.224338 0.172959 0.302775 -21.00000 0.09596
0.07577 =
0.07387 -0.00478 0.01614 -0.02817
AFIX 23
H30C 4 -0.287244 0.211971 0.262589 -21.00000 -1.20000
H30D 4 -0.247113 0.202077 0.352197 -21.00000 -1.20000
AFIX 0
C31' 3 -0.244489 0.037899 0.306267 -21.00000 0.07702
0.07744 =
0.08347 -0.00444 -0.00085 -0.01094
AFIX 23
H31C 4 -0.218887 0.010387 0.256603 -21.00000 -1.20000
H31D 4 -0.177689 0.000430 0.345509 -21.00000 -1.20000
AFIX 0
C32' 3 -0.415393 0.023058 0.326647 -21.00000 0.08385
0.18100 =
0.12583 0.00677 0.01066 -0.05634
AFIX 33
H32D 4 -0.438557 -0.052155 0.325353 -21.00000 -1.50000
H32E 4 -0.479278 0.066369 0.289837 -21.00000 -1.50000
H32F 4 -0.436278 0.045587 0.377623 -21.00000 -1.50000
PART 0
HKLF 4
```

```
REM wt2335w-SS-MU-14Cu_SohailSaeed_10-April-2012
REM R1 = 0.0486 for 4382 Fo > 4sig(Fo) and 0.0740 for all 6286 data
REM 446 parameters refined using 6 restraints
```

END

```
WGHT 0.0368 1.3930
REM Highest difference peak 0.411, deepest hole -0.374, 1-sigma level
0.053
```

```
Q1 1 0.3899 0.3586 -0.2819 11.00000 0.05 0.41
Q2 1 0.1764 0.4041 0.0421 11.00000 0.05 0.39
Q3 1 -0.0007 0.4862 0.0403 11.00000 0.05 0.32
Q4 1 0.0346 0.3160 -0.0162 11.00000 0.05 0.31
Q5 1 0.2616 0.4434 0.1365 11.00000 0.05 0.30
Q6 1 0.2080 0.3805 -0.0334 11.00000 0.05 0.29
Q7 1 0.0368 0.4216 0.1214 11.00000 0.05 0.29
Q8 1 0.2026 0.4675 0.1585 11.00000 0.05 0.28
```

Q9	1	0.2727	0.4067	-0.3300	11.00000	0.05	0.26
Q10	1	0.0849	0.5170	0.1401	11.00000	0.05	0.25
Q11	1	0.0372	0.5425	0.0268	11.00000	0.05	0.23
Q12	1	-0.0046	0.4843	0.0834	11.00000	0.05	0.23
Q13	1	0.2785	0.4400	0.0815	11.00000	0.05	0.23
Q14	1	0.5030	0.3185	-0.1609	11.00000	0.05	0.23
Q15	1	0.3136	0.1807	0.5372	11.00000	0.05	0.22
Q16	1	0.0126	0.2890	0.1951	11.00000	0.05	0.21
Q17	1	0.1745	0.5255	0.1220	11.00000	0.05	0.21
Q18	1	0.0858	0.3910	0.0524	11.00000	0.05	0.21
Q19	1	0.1763	0.3830	0.1169	11.00000	0.05	0.21
Q20	1	-0.0885	0.4242	0.1652	11.00000	0.05	0.20

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  'C' 'C' 0.0033 0.0016
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Refinement of  $F^2$  against ALL reflections. The weighted R-factor wR and goodness of fit S are based on  $F^2$ , conventional R-factors R are based on F, with F set to zero for negative  $F^2$ . The threshold expression of  $F^2 > 2\sigma(F^2)$  is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on  $F^2$  are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger.

The structure was solved by Patterson methods (*DIRDIF-99* (Beurskens et al., 1999)) and expanded using Fourier techniques. All non-H atoms were refined anisotropically.

The C-bound H atoms are all placed at geometrical positions with C---H = 0.93 Å and 0.97 Å for phenyl, methyl and methylene H-atoms respectively. The C-bound methylene and phenyl H-atoms were refined using riding model with  $U_{iso}(H) = 1.2U_{eq}(Carrier)$ . The methyl H-atoms were refined using riding model with  $U_{iso}(H) = 1.5U_{eq}(Carrier)$ .

One of the n-butyl groups were found to be disordered in two positions at occupancies of 0.782(16) and 0.218(16) respectively. A total of six restraints have been used in the refinement. They are relating to the anisotropic refinement of atom C31' using the isotropic restraints of standard uncertainty of 0.01., six restraints for each atom.

The refinement command used was:

```
ISOR 0.01 0.02 C31'
```

The command is needed to restrain the thermal parameters of the atom C31' within reasonable range.

Highest peak is 0.41 at (0.3899, 0.3586, 0.7181) [1.12 Å from C10]

Deepest hole is -0.37 at (0.1563, 0.5255, 0.0791) [0.82 Å from Cu1]

```
;
```

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_refine_ls_matrix_type full
_refine_ls_weighting_scheme calc
_refine_ls_weighting_details
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_atom_sites_solution_secondary    difmap  
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Cu1 Cu 0.13700(5) 0.46084(3) 0.08466(2) 0.04884(15) Uani 1 1 d . . .  
S1 S 0.10537(12) 0.35834(8) -0.01477(6) 0.0573(3) Uani 1 1 d . . .  
S2 S -0.02149(12) 0.35095(8) 0.15728(5) 0.0584(3) Uani 1 1 d . . .  
O1 O 0.2799(3) 0.55317(19) 0.02773(14) 0.0556(7) Uani 1 1 d . . .  
O2 O 0.6444(5) 1.0128(3) -0.1032(2) 0.1072(13) Uani 1 1 d . . .  
O3 O 0.7362(4) 0.9347(3) -0.2002(2) 0.0937(11) Uani 1 1 d . . .  
O4 O 0.1785(3) 0.5477(2) 0.17061(14) 0.0615(7) Uani 1 1 d . . .  
O5 O 0.2564(7) 0.9794(3) 0.3879(2) 0.158(2) Uani 1 1 d . . .  
O6 O 0.1703(6) 0.8912(3) 0.4863(2) 0.1350(17) Uani 1 1 d . . .  
N1 N 0.3386(3) 0.4768(2) -0.08949(16) 0.0477(7) Uani 1 1 d . . .  
N2 N 0.6611(4) 0.9342(3) -0.1404(2) 0.0689(10) Uani 1 1 d . . .  
N3 N 0.2607(4) 0.3268(2) -0.14275(17) 0.0533(8) Uani 1 1 d . . .  
N4 N 0.0975(4) 0.4442(2) 0.28196(16) 0.0529(8) Uani 1 1 d . . .  
N5 N 0.2060(6) 0.8989(3) 0.4194(2) 0.0879(12) Uani 1 1 d . . .  
N6 N 0.0210(4) 0.2716(2) 0.30187(17) 0.0566(8) Uani 1 1 d . B .  
C1 C 0.3409(4) 0.5504(3) -0.0388(2) 0.0449(8) Uani 1 1 d . . .  
C2 C 0.4328(4) 0.6487(3) -0.06438(19) 0.0451(8) Uani 1 1 d . . .  
C3 C 0.4321(4) 0.7354(3) -0.0188(2) 0.0554(10) Uani 1 1 d . . .  
H3 H 0.3799 0.7307 0.0286 0.066 Uiso 1 1 calc R . .  
C4 C 0.5076(5) 0.8290(3) -0.0425(2) 0.0604(10) Uani 1 1 d . . .  
H4 H 0.5066 0.8876 -0.0120 0.073 Uiso 1 1 calc R . .
```

C5 C 0.5846(4) 0.8328(3) -0.1129(2) 0.0520(9) Uani 1 1 d . . . .  
C6 C 0.5903(5) 0.7477(3) -0.1587(2) 0.0599(10) Uani 1 1 d . . . .  
H6 H 0.6447 0.7523 -0.2055 0.072 Uiso 1 1 calc R . . .  
C7 C 0.5136(4) 0.6545(3) -0.1341(2) 0.0547(10) Uani 1 1 d . . . .  
H7 H 0.5163 0.5957 -0.1644 0.066 Uiso 1 1 calc R . . .  
C8 C 0.2453(4) 0.3926(3) -0.0842(2) 0.0469(9) Uani 1 1 d . . . .  
C9 C 0.3776(5) 0.3477(3) -0.2044(2) 0.0728(12) Uani 1 1 d . . . .  
H9A H 0.4111 0.2797 -0.2250 0.087 Uiso 1 1 calc R . . .  
H9B H 0.4680 0.3789 -0.1832 0.087 Uiso 1 1 calc R . . .  
C10 C 0.3066(7) 0.4283(5) -0.2713(3) 0.1013(17) Uani 1 1 d . . . .  
H10A H 0.2136 0.3976 -0.2902 0.122 Uiso 1 1 calc R . . .  
H10B H 0.2752 0.4961 -0.2499 0.122 Uiso 1 1 calc R . . .  
C11 C 0.4100(8) 0.4515(6) -0.3357(4) 0.129(2) Uani 1 1 d . . . .  
H11A H 0.4472 0.3839 -0.3556 0.155 Uiso 1 1 calc R . . .  
H11B H 0.4995 0.4879 -0.3183 0.155 Uiso 1 1 calc R . . .  
C12 C 0.3297(9) 0.5226(5) -0.3996(3) 0.144(3) Uani 1 1 d . . . .  
H12A H 0.3970 0.5290 -0.4442 0.216 Uiso 1 1 calc R . . .  
H12B H 0.3064 0.5934 -0.3823 0.216 Uiso 1 1 calc R . . .  
H12C H 0.2347 0.4905 -0.4129 0.216 Uiso 1 1 calc R . . .  
C13 C 0.1529(5) 0.2413(3) -0.1538(2) 0.0582(10) Uani 1 1 d . . . .  
H13A H 0.1441 0.2340 -0.2089 0.070 Uiso 1 1 calc R . . .  
H13B H 0.0507 0.2639 -0.1349 0.070 Uiso 1 1 calc R . . .  
C14 C 0.1980(5) 0.1303(3) -0.1138(2) 0.0627(11) Uani 1 1 d . . . .  
H14A H 0.2938 0.1026 -0.1367 0.075 Uiso 1 1 calc R . . .  
H14B H 0.2170 0.1376 -0.0595 0.075 Uiso 1 1 calc R . . .  
C15 C 0.0708(5) 0.0503(3) -0.1212(3) 0.0693(11) Uani 1 1 d . . . .  
H15A H 0.0531 0.0429 -0.1757 0.083 Uiso 1 1 calc R . . .  
H15B H -0.0251 0.0792 -0.0993 0.083 Uiso 1 1 calc R . . .  
C16 C 0.1094(6) -0.0615(4) -0.0811(3) 0.0875(15) Uani 1 1 d . . . .  
H16A H 0.0203 -0.1057 -0.0824 0.131 Uiso 1 1 calc R . . .  
H16B H 0.1368 -0.0543 -0.0283 0.131 Uiso 1 1 calc R . . .  
H16C H 0.1955 -0.0952 -0.1073 0.131 Uiso 1 1 calc R . . .  
C17 C 0.1460(4) 0.5324(3) 0.2417(2) 0.0482(9) Uani 1 1 d . . . .  
C18 C 0.1678(4) 0.6266(3) 0.28922(19) 0.0450(8) Uani 1 1 d . . . .  
C19 C 0.2114(4) 0.7257(3) 0.2533(2) 0.0529(9) Uani 1 1 d . . . .  
H19 H 0.2310 0.7322 0.2003 0.063 Uiso 1 1 calc R . . .  
C20 C 0.2257(5) 0.8142(3) 0.2957(2) 0.0613(11) Uani 1 1 d . . . .  
H20 H 0.2548 0.8804 0.2717 0.074 Uiso 1 1 calc R . . .  
C21 C 0.1965(5) 0.8033(3) 0.3736(2) 0.0607(10) Uani 1 1 d . . . .  
C22 C 0.1562(6) 0.7062(3) 0.4112(2) 0.0734(13) Uani 1 1 d . . . .  
H22 H 0.1391 0.6999 0.4644 0.088 Uiso 1 1 calc R . . .  
C23 C 0.1419(5) 0.6188(3) 0.3682(2) 0.0681(12) Uani 1 1 d . . . .  
H23 H 0.1140 0.5526 0.3929 0.082 Uiso 1 1 calc R . . .  
C24 C 0.0393(4) 0.3581(3) 0.2506(2) 0.0494(9) Uani 1 1 d . . . .  
C25 C 0.0695(5) 0.2742(3) 0.3827(2) 0.0663(12) Uani 1 1 d . . . .  
H25A H 0.0123 0.2210 0.4147 0.080 Uiso 1 1 calc R . . .  
H25B H 0.0417 0.3454 0.3999 0.080 Uiso 1 1 calc R . . .  
C26 C 0.2400(6) 0.2512(4) 0.3945(2) 0.0788(13) Uani 1 1 d . . . .  
H26A H 0.2975 0.3100 0.3688 0.095 Uiso 1 1 calc R . . .  
H26B H 0.2714 0.1847 0.3713 0.095 Uiso 1 1 calc R . . .  
C27 C 0.2805(8) 0.2393(5) 0.4804(3) 0.115(2) Uani 1 1 d . . . .  
H27A H 0.2528 0.3072 0.5025 0.137 Uiso 1 1 calc R . . .  
H27B H 0.2173 0.1836 0.5061 0.137 Uiso 1 1 calc R . . .  
C28 C 0.4432(9) 0.2111(6) 0.4967(4) 0.153(3) Uani 1 1 d . . . .

H28A H 0.4603 0.2097 0.5514 0.230 Uiso 1 1 calc R . .  
H28B H 0.5074 0.2643 0.4701 0.230 Uiso 1 1 calc R . .  
H28C H 0.4697 0.1407 0.4793 0.230 Uiso 1 1 calc R . .  
C29 C -0.0512(5) 0.1721(3) 0.2829(2) 0.0672(12) Uani 1 1 d . . .  
H29A H 0.0009 0.1101 0.3112 0.081 Uiso 1 1 calc R A 1  
H29B H -0.0373 0.1638 0.2280 0.081 Uiso 1 1 calc R A 1  
C30 C -0.2243(6) 0.1730(4) 0.3028(3) 0.0814(14) Uani 0.782(16) 1 d P B 1  
H30A H -0.2357 0.1841 0.3574 0.098 Uiso 0.782(16) 1 calc PR B 1  
H30B H -0.2740 0.2356 0.2742 0.098 Uiso 0.782(16) 1 calc PR B 1  
C31 C -0.3141(11) 0.0744(7) 0.2875(5) 0.083(3) Uani 0.782(16) 1 d P B 1  
H31A H -0.4240 0.0891 0.2977 0.099 Uiso 0.782(16) 1 calc PR B 1  
H31B H -0.3023 0.0607 0.2334 0.099 Uiso 0.782(16) 1 calc PR B 1  
C32 C -0.2593(15) -0.0244(7) 0.3367(5) 0.121(5) Uani 0.782(16) 1 d P B 1  
H32A H -0.3195 -0.0850 0.3257 0.181 Uiso 0.782(16) 1 calc PR B 1  
H32B H -0.2719 -0.0115 0.3904 0.181 Uiso 0.782(16) 1 calc PR B 1  
H32C H -0.1512 -0.0404 0.3258 0.181 Uiso 0.782(16) 1 calc PR B 1  
C30' C -0.2243(6) 0.1730(4) 0.3028(3) 0.0814(14) Uani 0.218(16) 1 d P B 2  
H30C H -0.2872 0.2120 0.2626 0.098 Uiso 0.218(16) 1 calc PR B 2  
H30D H -0.2471 0.2021 0.3522 0.098 Uiso 0.218(16) 1 calc PR B 2  
C31' C -0.244(4) 0.038(3) 0.3063(19) 0.079(10) Uani 0.218(16) 1 d PU B 2  
H31C H -0.2189 0.0104 0.2566 0.095 Uiso 0.218(16) 1 calc PR B 2  
H31D H -0.1777 0.0004 0.3455 0.095 Uiso 0.218(16) 1 calc PR B 2  
C32' C -0.415(4) 0.023(3) 0.3266(18) 0.130(15) Uani 0.218(16) 1 d P B 2  
H32D H -0.4386 -0.0522 0.3254 0.195 Uiso 0.218(16) 1 calc PR B 2  
H32E H -0.4793 0.0664 0.2898 0.195 Uiso 0.218(16) 1 calc PR B 2  
H32F H -0.4363 0.0456 0.3776 0.195 Uiso 0.218(16) 1 calc PR B 2

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Cu1 0.0560(3) 0.0459(3) 0.0456(3) -0.00487(19) 0.0076(2) -0.0145(2)  
S1 0.0615(6) 0.0526(6) 0.0607(6) -0.0149(5) 0.0132(5) -0.0213(5)  
S2 0.0679(7) 0.0570(6) 0.0511(6) 0.0018(4) 0.0017(5) -0.0247(5)  
O1 0.0652(17) 0.0548(16) 0.0491(15) -0.0093(12) 0.0126(13) -0.0245(13)  
O2 0.136(3) 0.065(2) 0.125(3) -0.020(2) 0.040(2) -0.044(2)  
O3 0.116(3) 0.076(2) 0.088(2) 0.0099(17) 0.031(2) -0.0336(19)  
O4 0.087(2) 0.0543(16) 0.0459(15) -0.0078(12) 0.0144(13) -0.0288(14)  
O5 0.329(7) 0.059(2) 0.091(3) -0.010(2) -0.011(3) -0.055(3)  
O6 0.230(5) 0.100(3) 0.084(3) -0.045(2) 0.036(3) -0.050(3)  
N1 0.0491(18) 0.0453(18) 0.0487(17) -0.0023(14) 0.0036(14) -0.0070(14)  
N2 0.072(2) 0.056(2) 0.078(3) 0.0060(19) 0.005(2) -0.0201(18)  
N3 0.058(2) 0.0482(19) 0.0552(19) -0.0120(15) 0.0060(15) -0.0073(15)  
N4 0.071(2) 0.0414(18) 0.0468(17) -0.0006(14) 0.0033(15) -0.0119(15)  
N5 0.136(4) 0.061(3) 0.070(3) -0.011(2) -0.007(3) -0.018(2)  
N6 0.081(2) 0.0415(18) 0.0475(18) -0.0002(14) 0.0035(16) -0.0148(16)  
C1 0.040(2) 0.043(2) 0.050(2) 0.0018(17) -0.0017(16) -0.0013(16)  
C2 0.043(2) 0.043(2) 0.049(2) 0.0009(16) 0.0015(16) -0.0083(16)  
C3 0.060(2) 0.056(2) 0.051(2) -0.0020(18) 0.0100(18) -0.0129(19)  
C4 0.067(3) 0.052(2) 0.064(3) -0.0107(19) 0.004(2) -0.014(2)

C5 0.052(2) 0.044(2) 0.059(2) 0.0057(18) -0.0033(18) -0.0149(17)  
C6 0.065(3) 0.059(3) 0.055(2) 0.0003(19) 0.014(2) -0.010(2)  
C7 0.062(2) 0.048(2) 0.055(2) -0.0066(17) 0.0097(19) -0.0082(18)  
C8 0.045(2) 0.045(2) 0.050(2) -0.0016(17) -0.0025(16) -0.0009(17)  
C9 0.081(3) 0.065(3) 0.075(3) -0.023(2) 0.023(2) -0.010(2)  
C10 0.115(4) 0.113(4) 0.075(3) -0.004(3) 0.023(3) -0.002(3)  
C11 0.138(6) 0.134(6) 0.113(5) -0.001(4) 0.031(4) 0.006(4)  
C12 0.199(8) 0.128(6) 0.099(5) 0.017(4) 0.008(5) 0.015(5)  
C13 0.064(3) 0.058(3) 0.055(2) -0.0196(19) -0.0028(19) -0.009(2)  
C14 0.066(3) 0.051(2) 0.073(3) -0.015(2) -0.006(2) -0.001(2)  
C15 0.078(3) 0.062(3) 0.071(3) -0.012(2) 0.001(2) -0.015(2)  
C16 0.118(4) 0.063(3) 0.083(3) -0.007(2) -0.001(3) -0.016(3)  
C17 0.050(2) 0.046(2) 0.049(2) -0.0028(17) 0.0020(17) -0.0060(17)  
C18 0.047(2) 0.040(2) 0.048(2) -0.0022(15) -0.0008(16) -0.0070(16)  
C19 0.064(3) 0.049(2) 0.045(2) 0.0017(17) 0.0009(18) -0.0109(19)  
C20 0.083(3) 0.042(2) 0.059(2) 0.0046(18) -0.006(2) -0.016(2)  
C21 0.079(3) 0.046(2) 0.059(2) -0.0111(18) -0.004(2) -0.012(2)  
C22 0.114(4) 0.062(3) 0.047(2) -0.009(2) 0.012(2) -0.026(3)  
C23 0.103(3) 0.050(2) 0.052(2) -0.0021(19) 0.015(2) -0.026(2)  
C24 0.055(2) 0.040(2) 0.052(2) 0.0008(16) 0.0080(17) -0.0087(17)  
C25 0.098(4) 0.051(2) 0.049(2) 0.0039(18) 0.003(2) -0.020(2)  
C26 0.110(4) 0.060(3) 0.065(3) 0.005(2) -0.012(3) -0.008(3)  
C27 0.119(5) 0.128(5) 0.095(4) 0.003(4) -0.027(4) -0.003(4)  
C28 0.146(7) 0.183(8) 0.129(6) 0.018(5) -0.035(5) -0.031(6)  
C29 0.097(3) 0.043(2) 0.062(3) -0.0021(18) 0.012(2) -0.015(2)  
C30 0.096(4) 0.076(3) 0.074(3) -0.005(2) 0.016(3) -0.028(3)  
C31 0.086(6) 0.086(6) 0.077(5) -0.005(4) 0.011(4) -0.031(5)  
C32 0.192(12) 0.073(6) 0.099(6) 0.005(4) 0.007(6) -0.057(6)  
C30' 0.096(4) 0.076(3) 0.074(3) -0.005(2) 0.016(3) -0.028(3)  
C31' 0.077(13) 0.077(13) 0.083(12) -0.004(9) -0.001(9) -0.011(9)  
C32' 0.08(3) 0.18(3) 0.13(2) 0.01(2) 0.011(18) -0.06(2)

\_geom\_special\_details

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All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic)

treatment of cell esds is used for estimating esds involving l.s. planes.

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loop\_

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Cu1 O4 1.949(2) . ?

Cu1 S1 2.2448(11) . ?

Cu1 S2 2.2610(10) . ?

S1 C8 1.731(4) . ?

S2 C24 1.715(4) . ?  
O1 C1 1.262(4) . ?  
O2 N2 1.212(4) . ?  
O3 N2 1.212(4) . ?  
O4 C17 1.260(4) . ?  
O5 N5 1.190(5) . ?  
O6 N5 1.192(5) . ?  
N1 C1 1.316(4) . ?  
N1 C8 1.335(4) . ?  
N2 C5 1.480(5) . ?  
N3 C8 1.351(4) . ?  
N3 C13 1.459(5) . ?  
N3 C9 1.472(5) . ?  
N4 C17 1.324(4) . ?  
N4 C24 1.350(4) . ?  
N5 C21 1.482(5) . ?  
N6 C24 1.346(4) . ?  
N6 C29 1.462(5) . ?  
N6 C25 1.468(5) . ?  
C1 C2 1.509(5) . ?  
C2 C3 1.380(5) . ?  
C2 C7 1.383(5) . ?  
C3 C4 1.380(5) . ?  
C3 H3 0.9300 . ?  
C4 C5 1.378(5) . ?  
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C5 C6 1.367(5) . ?  
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C6 H6 0.9300 . ?  
C7 H7 0.9300 . ?  
C9 C10 1.576(6) . ?  
C9 H9A 0.9700 . ?  
C9 H9B 0.9700 . ?  
C10 C11 1.434(7) . ?  
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C11 C12 1.510(8) . ?  
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C12 H12A 0.9600 . ?  
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C13 H13B 0.9700 . ?  
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C14 H14A 0.9700 . ?  
C14 H14B 0.9700 . ?  
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C15 H15A 0.9700 . ?  
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C16 H16A 0.9600 . ?  
C16 H16B 0.9600 . ?  
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C18 C23 1.380(5) . ?  
C18 C19 1.391(5) . ?  
C19 C20 1.376(5) . ?  
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C20 H20 0.9300 . ?  
C21 C22 1.372(5) . ?  
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C22 H22 0.9300 . ?  
C23 H23 0.9300 . ?  
C25 C26 1.493(6) . ?  
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C25 H25B 0.9700 . ?  
C26 C27 1.526(6) . ?  
C26 H26A 0.9700 . ?  
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C27 C28 1.451(8) . ?  
C27 H27A 0.9700 . ?  
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C28 H28B 0.9600 . ?  
C28 H28C 0.9600 . ?  
C29 C30 1.522(6) . ?  
C29 H29A 0.9700 . ?  
C29 H29B 0.9700 . ?  
C30 C31 1.510(8) . ?  
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C31 C32 1.494(16) . ?  
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C31 H31B 0.9700 . ?  
C32 H32A 0.9600 . ?  
C32 H32B 0.9600 . ?  
C32 H32C 0.9600 . ?  
C31' C32' 1.52(5) . ?  
C31' H31C 0.9700 . ?  
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C32' H32D 0.9600 . ?  
C32' H32E 0.9600 . ?  
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loop\_

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O1 Cu1 S1 93.14(8) . . ?  
O4 Cu1 S1 176.40(9) . . ?  
O1 Cu1 S2 176.75(9) . . ?

O4 Cu1 S2 92.89(8) . . ?  
S1 Cu1 S2 88.96(4) . . ?  
C8 S1 Cu1 107.78(13) . . ?  
C24 S2 Cu1 104.65(12) . . ?  
C1 O1 Cu1 132.5(2) . . ?  
C17 O4 Cu1 130.7(2) . . ?  
C1 N1 C8 124.2(3) . . ?  
O3 N2 O2 123.1(4) . . ?  
O3 N2 C5 118.0(4) . . ?  
O2 N2 C5 118.9(4) . . ?  
C8 N3 C13 122.7(3) . . ?  
C8 N3 C9 120.5(3) . . ?  
C13 N3 C9 116.4(3) . . ?  
C17 N4 C24 124.6(3) . . ?  
O5 N5 O6 122.8(4) . . ?  
O5 N5 C21 117.6(4) . . ?  
O6 N5 C21 119.6(4) . . ?  
C24 N6 C29 123.6(3) . . ?  
C24 N6 C25 120.7(3) . . ?  
C29 N6 C25 115.8(3) . . ?  
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O1 C1 C2 114.3(3) . . ?  
N1 C1 C2 114.5(3) . . ?  
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C7 C2 C1 120.8(3) . . ?  
C4 C3 C2 121.0(3) . . ?  
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C2 C3 H3 119.5 . . ?  
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C5 C4 H4 121.1 . . ?  
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C6 C5 N2 118.9(3) . . ?  
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C6 C7 H7 120.0 . . ?  
N1 C8 N3 114.8(3) . . ?  
N1 C8 S1 129.2(3) . . ?  
N3 C8 S1 116.0(3) . . ?  
N3 C9 C10 110.2(4) . . ?  
N3 C9 H9A 109.6 . . ?  
C10 C9 H9A 109.6 . . ?  
N3 C9 H9B 109.6 . . ?  
C10 C9 H9B 109.6 . . ?  
H9A C9 H9B 108.1 . . ?  
C11 C10 C9 114.7(5) . . ?  
C11 C10 H10A 108.6 . . ?  
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C11 C10 H10B 108.6 . . ?

C9 C10 H10B 108.6 . . ?  
H10A C10 H10B 107.6 . . ?  
C10 C11 C12 111.4(6) . . ?  
C10 C11 H11A 109.3 . . ?  
C12 C11 H11A 109.3 . . ?  
C10 C11 H11B 109.3 . . ?  
C12 C11 H11B 109.3 . . ?  
H11A C11 H11B 108.0 . . ?  
C11 C12 H12A 109.5 . . ?  
C11 C12 H12B 109.5 . . ?  
H12A C12 H12B 109.5 . . ?  
C11 C12 H12C 109.5 . . ?  
H12A C12 H12C 109.5 . . ?  
H12B C12 H12C 109.5 . . ?  
N3 C13 C14 115.2(3) . . ?  
N3 C13 H13A 108.5 . . ?  
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N4 C17 C18 114.0(3) . . ?  
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N6 C24 S2 118.6(3) . . ?  
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C25 C26 C27 111.5(4) . . ?  
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C25 C26 H26B 109.3 . . ?  
C27 C26 H26B 109.3 . . ?  
H26A C26 H26B 108.0 . . ?  
C28 C27 C26 114.6(6) . . ?  
C28 C27 H27A 108.6 . . ?  
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H28A C28 H28B 109.5 . . ?  
C27 C28 H28C 109.5 . . ?  
H28A C28 H28C 109.5 . . ?  
H28B C28 H28C 109.5 . . ?  
N6 C29 C30 112.2(3) . . ?  
N6 C29 H29A 109.2 . . ?  
C30 C29 H29A 109.2 . . ?  
N6 C29 H29B 109.2 . . ?  
C30 C29 H29B 109.2 . . ?  
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C31 C30 C29 118.2(5) . . ?  
C31 C30 H30A 107.8 . . ?  
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C31 C30 H30B 107.8 . . ?  
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C32 C31 H31A 109.2 . . ?  
C30 C31 H31A 109.2 . . ?  
C32 C31 H31B 109.2 . . ?  
C30 C31 H31B 109.2 . . ?  
H31A C31 H31B 107.9 . . ?  
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C31 C32 H32B 109.5 . . ?  
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C31 C32 H32C 109.5 . . ?

H32A C32 H32C 109.5 . . ?  
H32B C32 H32C 109.5 . . ?  
C32' C31' H31C 110.9 . . ?  
C32' C31' H31D 110.9 . . ?  
H31C C31' H31D 108.9 . . ?  
C31' C32' H32D 109.5 . . ?  
C31' C32' H32E 109.5 . . ?  
H32D C32' H32E 109.5 . . ?  
C31' C32' H32F 109.5 . . ?  
H32D C32' H32F 109.5 . . ?  
H32E C32' H32F 109.5 . . ?

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# start Validation Reply Form

\_vrf\_PLAT003\_wt2335w-shelxl

;

PROBLEM: Number of Uiso or Uij Restrained Atom Sites .... 1  
RESPONSE: Atom C31' was refined with the isotropic restrains  
of standard uncertainty of 0.01., six restraints for each atom.

;

\_vrf\_PLAT860\_wt2335w-shelxl

;

PROBLEM: Note: Number of Least-Squares Restraints ..... 6  
RESPONSE: Atom C31' was refined with the isotropic restrains  
of standard uncertainty of 0.01, six restraints for each atom.

;

\_vrf\_PLAT154\_wt2335w-shelxl

;

PROBLEM: The su's on the Cell Angles are Equal ..... 0.00400 Deg.  
RESPONSE: It was accidental that The su's on the cell angles are equal.

;

\_vrf\_PLAT301\_wt2335w-shelxl

;

PROBLEM: Note: Main Residue Disorder ..... 6 Perc.  
RESPONSE: One of the n-butyl groups were found to be disordered in two  
positions at occupancies of 0.782(16) and 0.218(16) respectively.

;

# End Validation Reply Form

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2012-Apr-11

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# PROCESSING SUMMARY (IUCr Office Use Only)

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# SUBMISSION DETAILS

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_publ_contact_author_email          'Sohail262001@yahoo.com'
_publ_contact_author_fax            '092-51-925-0081'
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# TITLE AND AUTHOR LIST

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# copper (II) complex,
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Department of Chemistry, Research Complex,  
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Islamabad-44000,  
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'sohail262002@yahoo.com'  
'Wong, Wing-Tak'  
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Hong Kong SAR,  
P. R. CHINA  
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There are two molecules of the copper(II) complex,  
C~32~H~44~CuN~6~O~6~S~2~, in  
the unit cell.
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One of the butyl groups was found to be disordered in two positions  
at occupancies of 0.782(16) and 0.218(16) respectively.

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_publ_section_references
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Fig. 1. The title molecule was shown at 50% probability thermal ellipsoids with the atom numbering scheme (only the major component was shown).

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The crystal of the copper complex,  $C_{32}H_{44}CuN_6O_6S_2$ , a dark-brown block, having approximate dimensions of 0.08 mm *x* 0.10 mm *x* 0.50 mm was mounted on glass fiber. All measurements were made on a Bruker *SMART 1000* CCD detector with graphite monochromated Mo-K $\alpha$  radiation. The crystal-to-detector distance was 50.00 mm.

Indexing was performed from 60 images that were exposed for 10 s for a preliminary unit cell determination. Of which, 52 out of total of 65 reflections were successfully indexed. The crystal-to-detector distance was 50.00 mm.

Cell constants and an orientation matrix for data collection corresponded to a primitive monoclinic cell with dimensions:  $a = 8.585(2)$  Å,  $b = 12.347(3)$  Å,  $c = 17.326(4)$  Å,  $V = 1828.8(8)$  Å<sup>3</sup>,  $a = 85.325(4)$ °,  $b = 89.305(4)$ °,  $\gamma = 87.573(4)$ °.

For  $Z = 2$  and F.W. = 736.40, the calculated density is 1.337 g/cm<sup>3</sup>.

Based on a statistical analysis of intensity distribution, and the successful solution and refinement of the structure, the space group was determined to be:  $P-1$  (#2).

The data were collected at a temperature of 27(1)°C to a maximum  $2\theta$  value of 50.0°. A total of 1421 oscillation images were collected in 4 runs. A sweep of data was done using  $\omega$  scans from 330.0 to 148.2° in 0.3° step, at  $\chi = 54.7$ ° and  $\phi = 0.0$ °. The exposure rate was 35.0 [sec./°]. The detector swing angle was -30.00°. A second sweep was performed using  $\omega$  scans from 330.0 to 199.5° in 0.3° step, at  $\chi = 54.7$ ° and  $\phi = 90.0$ °. The exposure rate was 35.0 [sec./°]. The detector swing angle was -30.00°. A third sweep was performed using  $\omega$  scans from 330.0 to 261.0° in 0.3° step, at  $\chi = 54.7$ ° and  $\phi = 180.0$ °. The exposure rate was 35.0 [sec./°]. The detector swing angle was -30.00°. A last sweep was performed using  $\omega$  scans from 330.0 to 285.0° in 0.3° step, at  $\chi = 54.7$ ° and  $\phi = 270.0$ °. The exposure rate was 35.0 [sec./°]. The detector swing angle was -30.00°. The crystal-to-detector distance was 50.00 mm.

Of the 10157 reflections that were collected, 6286 reflections were unique.

$R_{int} = 0.0211$ ; equivalent reflections were merged.

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The structure was solved by Patterson methods (*DIRDIF-99* (Beurskens et al., 1999)) and expanded using Fourier techniques. All non-H atoms were refined anisotropically.

The C-bound H atoms are all placed at geometrical positions with C-H = 0.93

0.96 and 0.97 Å for phenyl, methyl and methylene H-atoms respectively.

The C-bound methylene and phenyl H-atoms were refined using riding model with  $U_{iso}(H) = 1.2U_{eq}(\text{Carrier})$ . The methyl H-atoms were refined using riding model with  $U_{iso}(H) = 1.5U_{eq}(\text{Carrier})$ .

One of the n-butyl groups were found to be disordered in two positions at occupancies of 0.782(16) and 0.218(16) respectively. A total of six restraints have been used in the refinement. They are relating to the anisotropic refinement of atom C31' using the isotropic restrains of standard uncertainty of 0.01., six restraints for each atom.

Highest peak is 0.41 at (0.3899, 0.3586, 0.7181) [1.12\%A from C10]  
Deepest hole is -0.37 at (0.1563, 0.5255, 0.0791) [0.82\%A from Cu1]

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