

7. Supplementary Information

Theoretical Modeling Procedure:

Theoretical modeling based upon the so-called quasi-static approximation [41-42] was applied here to describe the temperature dependence of LSRP absorption in a single Au nanoparticle much smaller than the wavelength of the incident electromagnetic radiation. The simple theory was also applied to explain the experimentally observed shift in LSPR absorption peak. An approach described in previous publications was followed using the materials parameters for Au and SiO₂ presented in **Table S1** [36-37, 43]. Equations S1 – S3 presented below describe the absorption cross-section (Q_{Abs}), the dielectric constant of Au (ϵ_{Au}), and the plasmon resonance frequency (ω_p) as a function of various material, temperature, wavelength, and particle size dependent parameters:

$$(Q_{Abs} = \frac{4\pi^2 a^3 \sqrt{\epsilon_m} \text{Im} \left[\frac{\epsilon_{Au} - \epsilon_m}{\epsilon_{Au} + 2\epsilon_m} \right]) \quad (S1)$$

$$(\epsilon_{Au} = \epsilon_{AuFree} + \epsilon_{AuIB} = \left(1 - \frac{\omega_p^2}{\omega^2 + i\Gamma\omega}\right) + \epsilon_{AuIB}) \quad (S2)$$

$$(\omega_p = \sqrt{\frac{Ne^2}{m^* \epsilon_0}}) \quad (S3)$$

In Eqs. S1-S3, a is the radius of the nanoparticle, ϵ_m is the dielectric constant of the matrix phase, ϵ_{AuFree} and ϵ_{AuIB} are the contributions to the dielectric constant of Au associated with free carriers and interband electronic transitions, N is the free electron density of Au, e is the charge of an electron, m^* is the effective mass of free electrons, ϵ_0 is the permittivity of free space, and Γ is a characteristic damping frequency for free carriers. In the context of this model, the temperature dependence of the optical absorption cross-section (Q_{Abs}) of a Au nanoparticle is expected to depend upon the temperature dependence of the optical constants of Au (ϵ_{Au}) and the matrix phase (ϵ_m). For simplicity it is assumed that the refractive index of SiO₂ is approximately constant over the wavelength range of interest ($n=1.45$ at room temperature) and the contribution

due to ϵ_{Au} associated with interband electronic transitions (ϵ_{AuIB}) was assumed to be temperature independent using the models and parameters published by P. Etchegoin [44].

We have employed the theoretical approach described previously for modeling of monolithic Au films deposited on optical fibers to the nanocomposite films under investigation here [36-37, 43]. In our case the matrix phase is SiO₂ which exhibits a weak and roughly linear dependence of refractive index on temperature over the temperature range of interest and hence it is assumed to be described by a single thermo-optic coefficient of $dn_m/dT \sim 1.28 \times 10^{-5}$ RIU/K. In the case of Au, we make the same assumption as previous authors that the primary effect of increasing temperature is to decrease the density of free electrons due to thermal expansion and to increase the effective damping frequency of free carriers due to the increased scattering with increasing temperature. Table S1 below presents a complete table of the various parameters employed in all calculations.

Parameter	Value	Source
a (nm)	5	Typical Au Nanoparticle Radius
n_m	1.45	Typical for Dense SiO ₂
dn_m/dT (Fixed)	$1.28 \times 10^{-5} \text{ K}^{-1}$	[43, 45]
ω_p (rad/s)	$1.314 \times 10^{16} \text{ s}^{-1}$ @ 273K, Depends on T	[43-45]
Γ (rad/s)	Depends on T	[43, 45]
ϵ_{AuIB}	Depends on λ	[44]
v_{Fermi}	$1.4 \times 10^{15} \text{ nm/s}$	[43-45]

Table S1. List of parameters used in this work and/or the reference from which the parameters were taken.

The expected reduction in free electron density, N, associated with the thermal expansion of Au translates directly into a reduction in the bulk plasmon frequency, ω_p , according to Eq. S4.

$$(\omega_p(T) = \omega_p(T_0) * (1 + 3\alpha(T - T_0))^{-1/2}) \quad (\text{S4})$$

The linear thermal expansion coefficient of Au can be utilized for the value of α for the case of Au nanoparticles in free space or loosely bound to a surface. Prior authors have made a correction to the linear thermal expansion coefficient of Au for monolithic Au films to account for an expansion in only one dimension along the film normal [43]. This particular correction is not relevant to the Au nanoparticle incorporated films and hence it was not employed as in our prior work [37].

The temperature dependence of the effective damping frequency, Γ , can be modeled by assuming a contribution associated with both electron-electron (Γ_e) and electron-phonon (Γ_p) scattering. A size dependent surface scattering term ($\Gamma_s = V_F/a$, where V_F is Fermi velocity) assumed to be temperature independent has also been included to account for the finite particle size [36-37, 43].

$$(\Gamma = \Gamma_e + \Gamma_p + \Gamma_s = \Gamma_e + \Gamma_p + \frac{V_F}{a}) \quad (\text{S5})$$

We have employed the same analytical expressions for the temperature dependence of Γ_e and Γ_p utilized by prior authors which are not reproduced here for brevity [36-37, 43, 46]. The simulated results of the LSPR absorption for a Au nanoparticle embedded in SiO₂ according to the assumptions outlined above are presented in Figure 3. A monotonic decrease in LSPR absorption peak height and an increase in peak wavelength is observed with increasing temperatures. As discussed in previous work, the former is primarily associated with the increasing resistivity of Au while the latter results from the small, positive thermo-optic coefficient of SiO₂ as well as the thermal expansion of Au nanoparticles [37]. The reduction in absorptance for the simulated absorption cross section for a temperature of 800°C as compared to 600°C is plotted in Figure 3c to illustrate the wavelength dependence of temperature sensitivity for the range of temperatures relevant for solid oxide fuel cell applications.

As discussed in prior publications [4, 37], the simple quasi-static model of Eq. S1 suggests that the origin of a gas sensing response of LSPR absorption can be attributed to changes in one or more of the following material parameters assuming that no change in Au particle size, shape, or distribution occurs: (1) the dielectric constant of the matrix phase (ϵ_m), (2) the damping frequency of free carriers in the Au nanoparticles (Γ), or (3) the density of free carriers in the Au nanoparticles (N). The possibility of a change in Γ as the primary origin of the gas sensing response can be ruled out as it would cause a broadening or sharpening of the LSPR absorption peak instead of a shift as experimentally observed (see Figure 2b) [4, 47]. A contribution associated with a change in refractive index of SiO₂ cannot be ruled out but we assume that this effect is negligible for the reasons described above. As a result, we simulate the gas sensing response in the quasi-static approximation using the simple derivative approach of Eq. S6 accounting for changes in free electron density.

$$(\Delta Q_{Abs}(\lambda) \approx \left. \frac{\partial Q_{Abs}}{\partial N} \right|_{\lambda} \Delta N) \quad (S6)$$

In Figure 3b, we plot the negative of the simulated $\Delta Q_{Abs}(\lambda)$ normalized to the peak value assuming a 1% increase in free electron density (N). The strong asymmetry about the original LSPR absorption peak position is associated with the dampening of the LSPR absorption peak by interband electronic transitions in Au.

Experimental Gas Sensing Response of Films on Planar Substrates:

Here we present gas sensing results that elucidate the wavelength dependence of the response to the reducing gases H₂ and CO for comparison with the theoretical modeling of Figure 3 for Au / SiO₂ films deposited on planar substrates. Simulated optical gas sensing tests were performed by monitoring the transmittance of Au / SiO₂ films in gas mixtures consisting of

flowing N₂, O₂, and H₂ or CO at a temperature of 850°C. For the film deposited on a planar substrate, we report sensing responses to H₂ only as the response to CO was observed to be relatively weak in comparison and difficult to resolve within experimental error.

The H₂ sensing experiment in N₂ or low O₂ content (~1%, 2% or 3% by volume) balance N₂ background gases are presented in **Figure S1**. These experiments consisted of 30 minute cycles of the background gas indicated and 30 minute cycles in which H₂ levels of 0.04, 0.2, 0.4, 1, 2, 3, and 4 volume % were introduced into the background. The 0.04% H₂ level was the lowest limit confidently distributed by the gas sensor testing facility. Figure S1a illustrates the film transmittance response at $\lambda=550\text{nm}$ to H₂ up to 4% by volume in N₂ as well as dilute O₂ (~1% by volume) / balance N₂ backgrounds. The 0.4 volume % H₂ cycle for the N₂ background shows a higher response than the 1 volume % H₂ cycle but the difference is within our experimental error. As such, the data suggests a monotonic response to H₂ over the range experimentally investigated here for the N₂ and dilute O₂ / balance N₂ backgrounds. The total change in transmittance relative to the background baseline (see horizontal dashed lines) is enhanced for the dilute O₂ background test. For tests conducted with larger contents of O₂ present (e.g. 2% and 3% O₂ by volume), the transmittance response to H₂ is suppressed suggesting that O₂ may not be necessary for a measurable sensing response but that it can play a role in the sensing mechanism. In N₂ or a dilute O₂ (~1% by volume) background the transmittance response (ΔT) illustrated in Figure S1b can be fitted to a power law in terms of the H₂ volume fraction (vol% H₂) of the following form:

$$(\Delta T = \Delta T_0 \cdot \text{vol}\% \text{H}_2^n) \quad (\text{S7})$$

Estimated values of ΔT_0 and n obtained through the fit are $\Delta T_0=1.27\pm 0.04$, $n=0.12\pm 0.03$ and $\Delta T_0=1.94\pm 0.02$, $n=0.11\pm 0.01$ for the N₂ and dilute O₂ (~1% by volume) background,

respectively. Similar fits to the data at higher O₂ contents yield larger exponents of roughly 0.8-1.2 approximating a linear relationship between transmittance and vol% H₂ if a single point measured for the vol% H₂ = 4%, vol% O₂ = 2% gas mixture with a relatively large response is excluded but are also subject to a large absolute error (see Figure S1a). Further investigations are required to fully elucidate the mechanistic origins of the gas sensing responses observed.

A reduction in baseline transmittance at $\lambda=550\text{nm}$ (see horizontal dashed lines) is observed for the O₂ containing background tests as compared to the N₂ background test suggesting that the presence of O₂ can also impact the LSPR absorption peak. By comparing the corresponding response at other wavelengths the change in baseline with O₂ can be attributed to a shift in LSPR absorption peak position opposite that which occurs during a H₂ exposure. These observations are consistent with a gas sensing response that is dictated by charge transfer to and from Au nanoparticles as oxidizing species such as O₂ would promote interactions that extract free electrons from Au while reducing species such as H₂ would tend to donate them effectively shifting the LSPR absorption peak in opposite directions and causing a transmission response change of opposite sign.

A H₂ sensing response for Au / SiO₂ films at 850°C in a 1% O₂ / balance N₂ background and the transmittance as a function of temperature in a 20% O₂ / balance N₂ background normalized to the value at T=500°C are presented in **Figure S2**. A summary of the wavelength dependence of the experimentally measured temperature response is also presented illustrating the unique wavelength dependences of the H₂ and temperature sensing responses. The wavelength dependences are reasonably consistent with theoretical calculations presented in Figure 3 as the peak H₂ response is observed near the inflection point of the LSPR absorption peak ($\lambda\sim 550\text{-}600\text{nm}$) while the peak temperature sensitivity is observed near the LSPR

absorption peak maximum ($\lambda \sim 525\text{-}540\text{nm}$). A zero-crossing in temperature sensitivity is also observed in the expected wavelength range. As observed for the fiber sensor, the H_2 response for the highest levels of H_2 investigated do not exhibit a zero-crossing in the wavelength range expected based upon Figure 3b. Nevertheless, unique wavelength dependences of the H_2 and temperature sensing responses may still potentially be exploited for simultaneous gas and temperature sensing through multiple or broadband wavelength interrogation. For the films synthesized here, $\lambda_{\text{Temp}} \sim 510\text{-}525\text{nm}$ and $\lambda_{\text{Gas}} \sim 565\text{-}575\text{nm}$ would be optimal wavelength interrogation choices to maximize the relative response to the temperature or H_2 content of the gas stream, respectively.

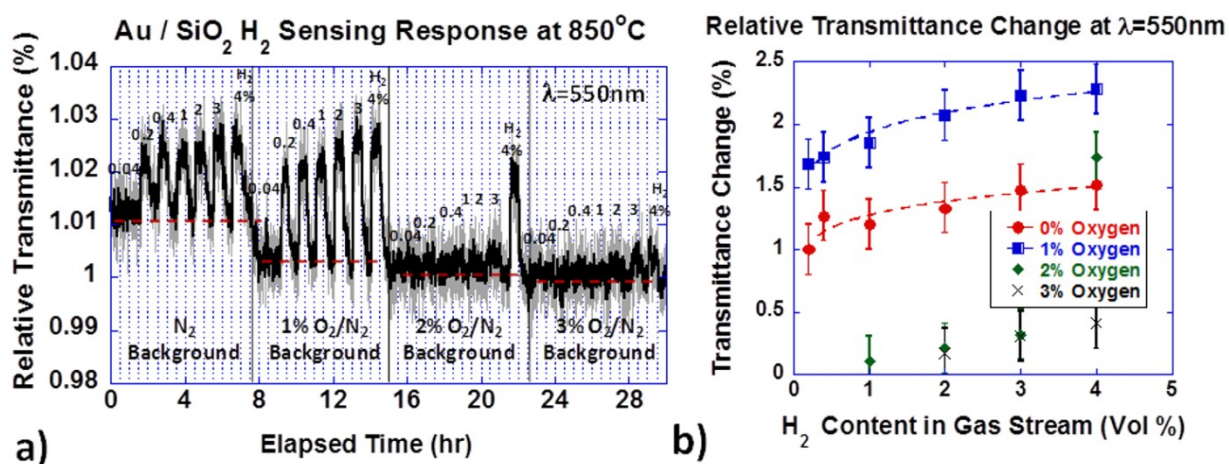


Figure S1. (a) Transmittance sensing response ($\lambda=550\text{nm}$) of Au / SiO₂ film to varying levels of H₂ (0.04%, 0.2%, 0.4%, 1%, 2%, 3% and 4% by volume) in a N₂, 1%O₂/N₂, 2%O₂/N₂, or 3%O₂/N₂ background at T=850°C with 30 minute cycles for each gas exposure. (b) Peak transmittance change relative to the baseline with varying levels of H₂ in different O₂ backgrounds at $\lambda=550\text{nm}$ with the dashed lines representing the power law fits described in the text. The assumed baseline used to calculate the results of (b) for each O₂/N₂ background level is illustrated by horizontal dashed lines. The solid dark line in (a) illustrates the result of smoothing the raw data to reduce detector noise.

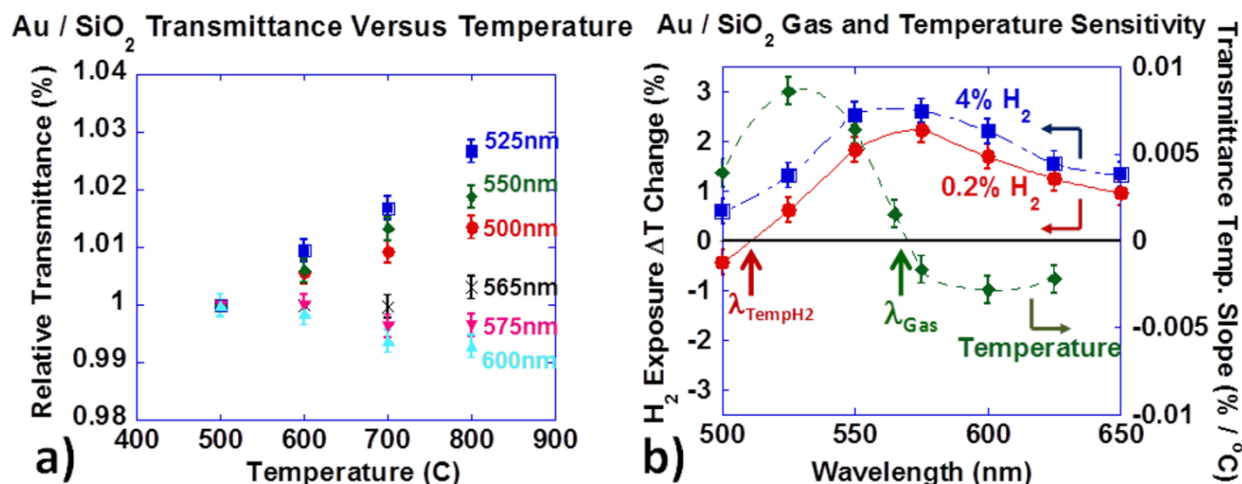


Figure S2. (a) Relative transmittance normalized to the value at 500°C as a function of temperature in an air atmosphere for a range of different wavelengths. (b) Summary of the wavelength dependence of the temperature and gas sensing response using the estimated slopes from a linear fit to data such as that presented in (a) over the range 600-800°C and the gas sensing results for vol% H₂=0.2%, 4% in a 1%O₂ balance N₂ background at T=850°C from measurements such as those presented in Figure S1.