

Electronic Supplementary Information

On the Electronic Structure and Conflicting d-Orbital Aromaticity in the Re_3O_3^- Cluster

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Molecular Orbital Analyses for the high-lying $\text{Re}_3\text{O}_3^- D_{3h}$ structures.

Figures S1-S2. Alternative optimized structures for Re_3O_3^- and Re_3O_3 at the

B3LYP/Re/Stuttgart+2f1g/O/aug-cc-pVTZ level.

Figure S3. Molecular orbital pictures for the $\text{Re}_3\text{O}_3^- D_{3h}$ (${}^3\text{A}_1'$) structure, which lies 3.06 eV above the global minimum at B3LYP/Re/Stuttgart+2f1g/O/aug-cc-pVTZ level.

Figure S4. Molecular orbital pictures for the $\text{Re}_3\text{O}_3^- D_{3h}$ (${}^1\text{A}_1'$) structure, which lies 5.36 eV above the global minimum at B3LYP/Re/Stuttgart+2f1g/O/aug-cc-pVTZ level.

Table S1. Cartesian coordinates for all optimized structures for Re_3O_3^- and Re_3O_3 at B3LYP/Re/Stuttgart+2f1g/O/aug-cc-pVTZ level.

Molecular Orbital Analyses for the High-Lying $\text{Re}_3\text{O}_3^- D_{3h}$ Structures

The highly symmetric $\text{Re}_3\text{O}_3^- D_{3h}$ (${}^3\text{A}_1'$) and D_{3h} (${}^1\text{A}_1'$) structures (Figures S3 and S4) seem to be tempting candidates to account for the vibrationally-resolved photoelectron spectrum (Figure 1a), which hints relatively high symmetry for both the anion and neutral clusters. This hypothesis turns out to be wrong, in terms of both their energetics and their simulated PES spectra (Figure 3d and 3e). Thus a critical question arises: Why are these D_{3h} structures so much higher in energy relative to the C_{2v} (${}^1\text{A}_1$) global minimum (Figure 2a)?

A three-center transition metal system in principle is capable of forming four completely bonding (two σ -, one π -, and one δ -) MOs.^{S1,S2} Ideally all these MOs need to be filled in order for a Re_3O_3^- structure to be stable. However, the D_{3h} structures each possess only three completely bonding MOs, and the two additional electrons that are supposed to occupy the missing σ -MO are forced to occupy the antibonding MOs instead.

To be specific, HOMO–5 ($1\text{a}_1'$) and HOMO–1 ($1\text{e}'$) of the D_{3h} (${}^3\text{A}_1'$) structure (Figure S3) represent the σ/σ^* combination and HOMO–2 ($1\text{a}_2''$) and HOMO–3 ($1\text{e}''$) represent the π/π^* combination. These MOs can be roughly localized as three (albeit weak) Re=Re double bonds. The remaining HOMO–4 ($2\text{a}_1'$) and half-occupied HOMO ($2\text{e}'$) collectively render δ aromaticity for this species, according to the reversed $4n$ Hückel aromaticity rule for triplet coupled electrons. Overall, the Re-Re bonding (2.424 Å) in D_{3h} (${}^3\text{A}_1'$) is slightly weaker than typical Re=Re double bonds (2.38 Å).^{S3}

For the D_{3h} (${}^1\text{A}_1'$) structure (Figure S4), the HOMO–5 ($1\text{a}_1'$) and HOMO–2 ($1\text{e}'$) form the σ framework and may be considered as three Re-Re σ -bonds, which are largely canceled by the net antibonding nature of the π framework: HOMO–4 ($1\text{a}_2''$), HOMO–1 ($1\text{e}''$), and HOMO ($1\text{a}_1''$). The remaining completely bonding HOMO–3 ($2\text{a}_1'$) renders δ -aromaticity to this species. Not surprisingly, the net Re-Re bonding (2.699 Å) in D_{3h} (${}^1\text{A}_1'$) is even weaker than typical Re-Re single bonds (2.62 Å),^{S3} commensurate with its energetic instability.

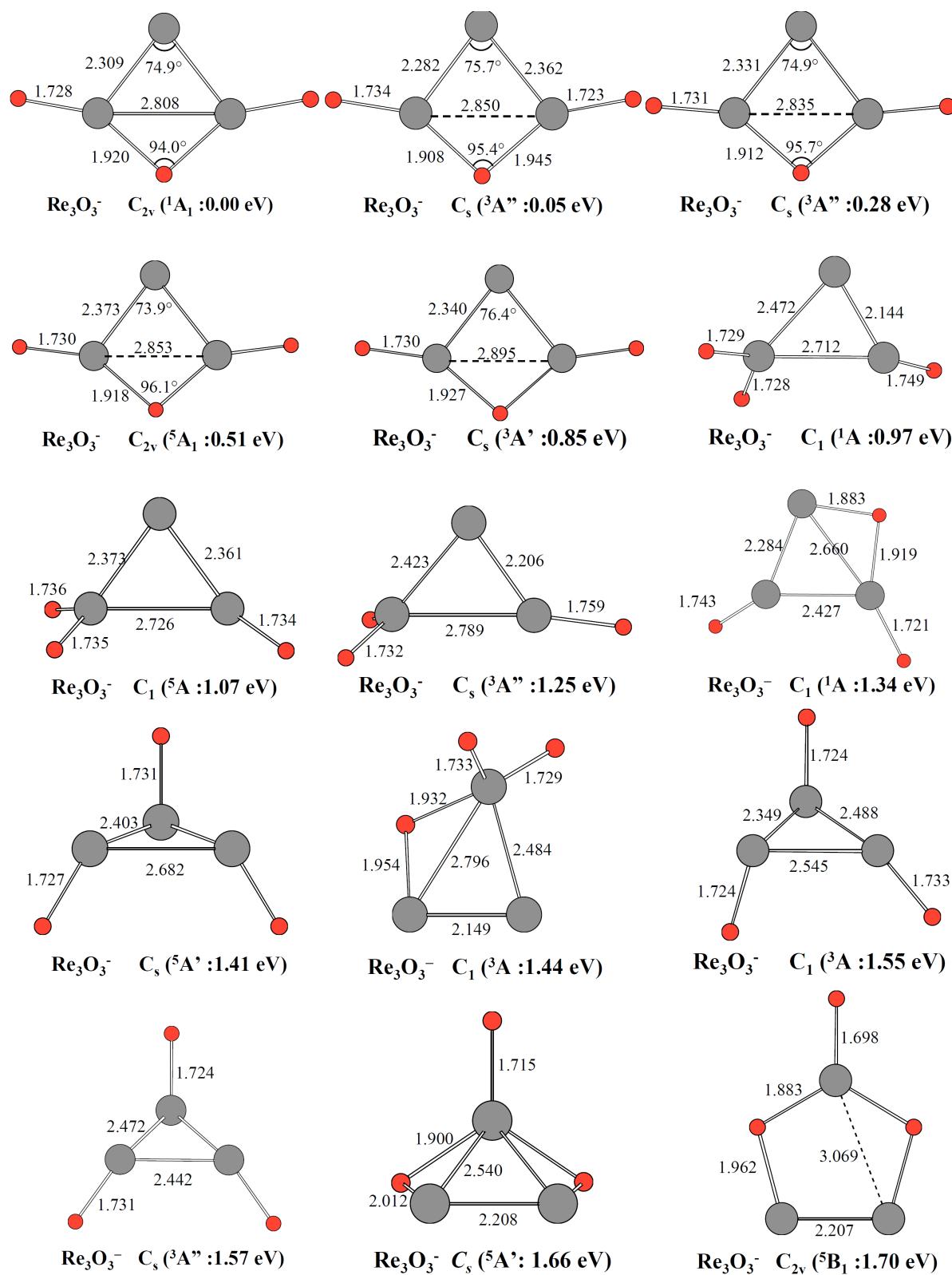
In contrast to these high-lying D_{3h} structures, all four bonding MOs are fully occupied in the C_{2v} (${}^1\text{A}_1$) global minimum, and in addition the structural distortion to C_{2v} poses extra

stabilization to the corresponding σ^* and π^* MOs.

References:

- (S1) Averkiev, B. B.; Boldyrev, A. I. Hf₃ Cluster Is Triply (σ -, π -, and δ -) Aromatic in the Lowest D_{3h} , ${}^1\text{A}_1'$ State. *J. Phys. Chem. A* **2007**, *111*, 12864–12866.
- (S2) Zhai, H. J.; Wang, B.; Huang, X.; Wang, L. S. Structural Evolution, Sequential Oxidation, and Chemical Bonding in Tritantalum Oxide Clusters: Ta₃O_n[−] and Ta₃O_n ($n = 1$ –8). *J. Phys. Chem. A* **2009**, *113*, 9804–9813.
- (S3) Pyykkö, P.; Atsumi, M. Molecular Double-Bond Covalent Radii for Elements Li–E112. *Chem. Eur. J.* **2009**, *15*, 12770–12779.

Figure S1. Optimized structures (distances in angstroms and angles in degrees) and their relative energies for Re_3O_3^- cluster.



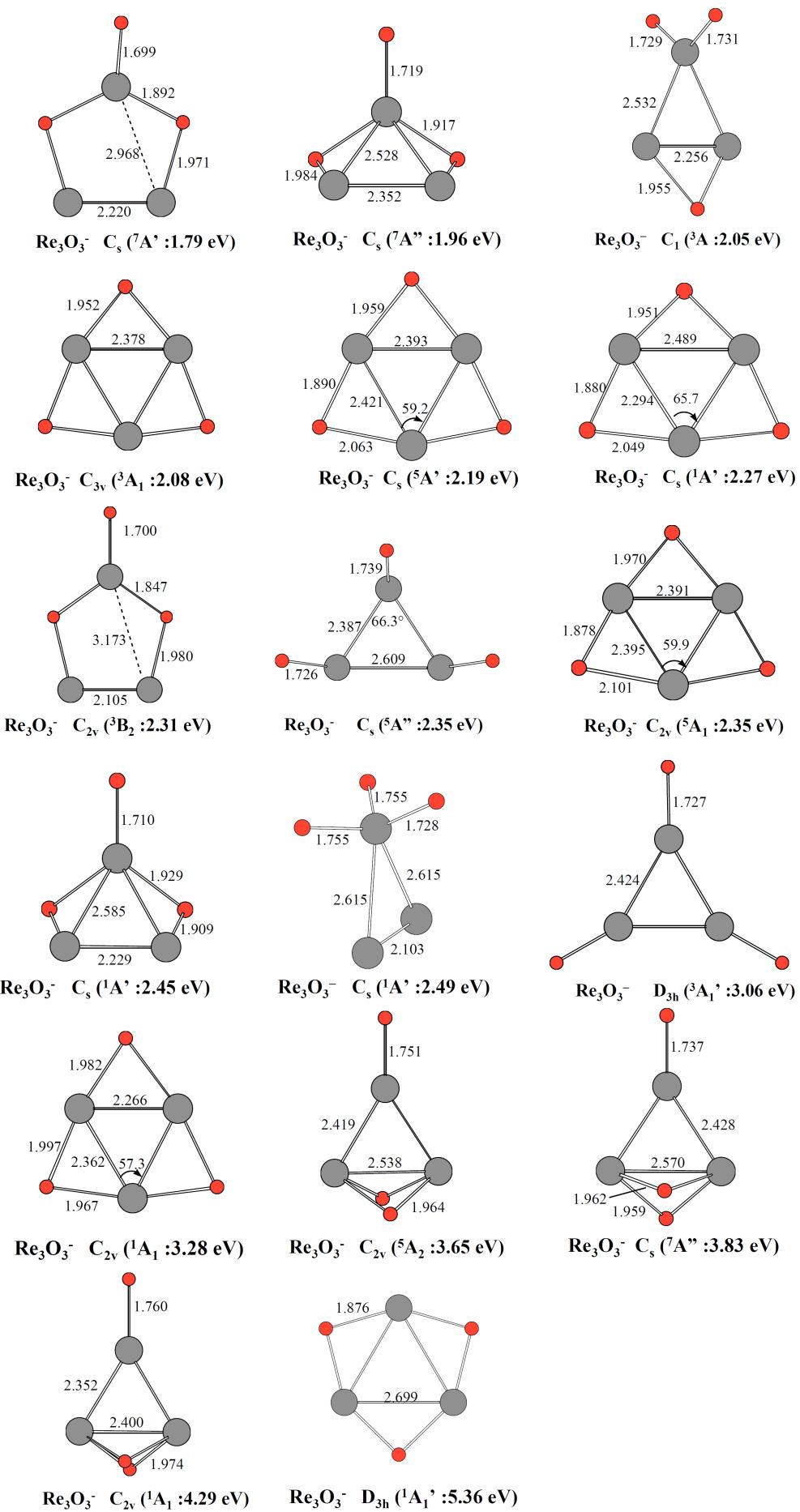


Figure S2. Optimized structures (distances in angstroms and angles in degrees) and their relative energies for Re_3O_3 cluster.

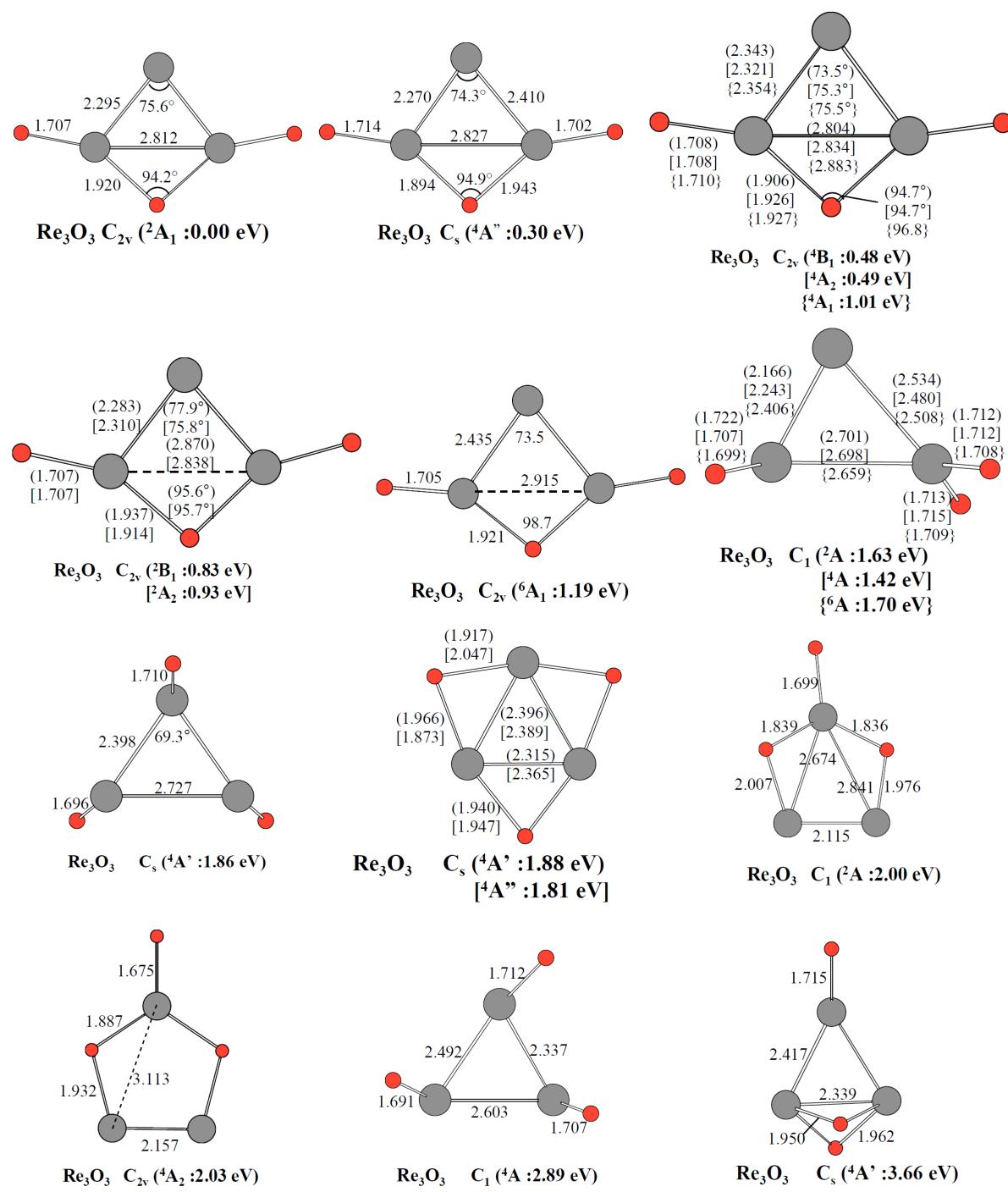


Figure S3. Molecular orbital pictures for the $\text{Re}_3\text{O}_3^- D_{3h} (^3\text{A}_1')$ structure, which lies 3.06 eV above the global minimum at B3LYP/Re/Stuttgart+2f1g/O/aug-cc-pVTZ level.

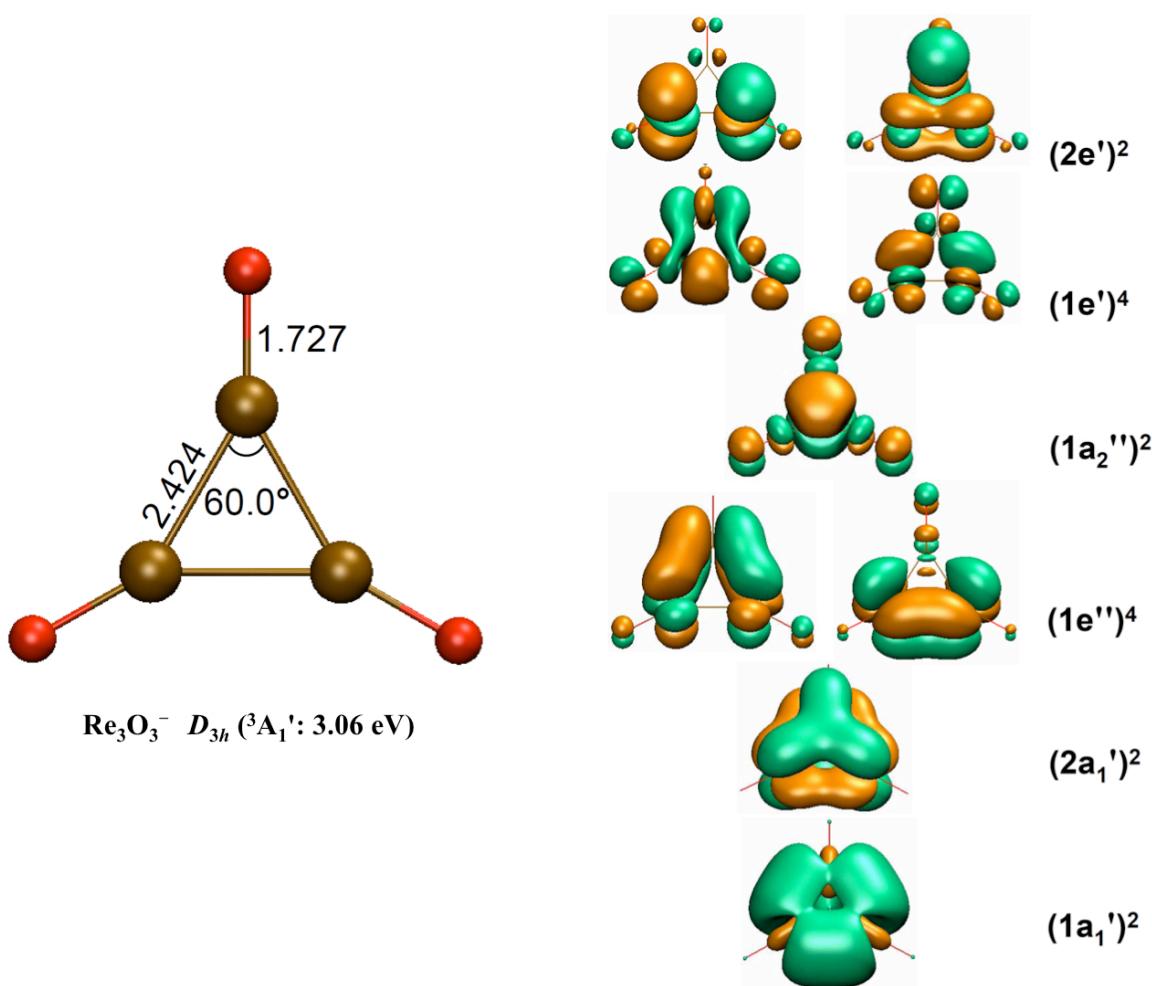


Figure S4. Molecular orbital pictures for the $\text{Re}_3\text{O}_3^- D_{3h} (^1\text{A}_1')$ structure, which lies 5.36 eV above the global minimum at B3LYP/Re/Stuttgart+2f1g/O/aug-cc-pVTZ level.

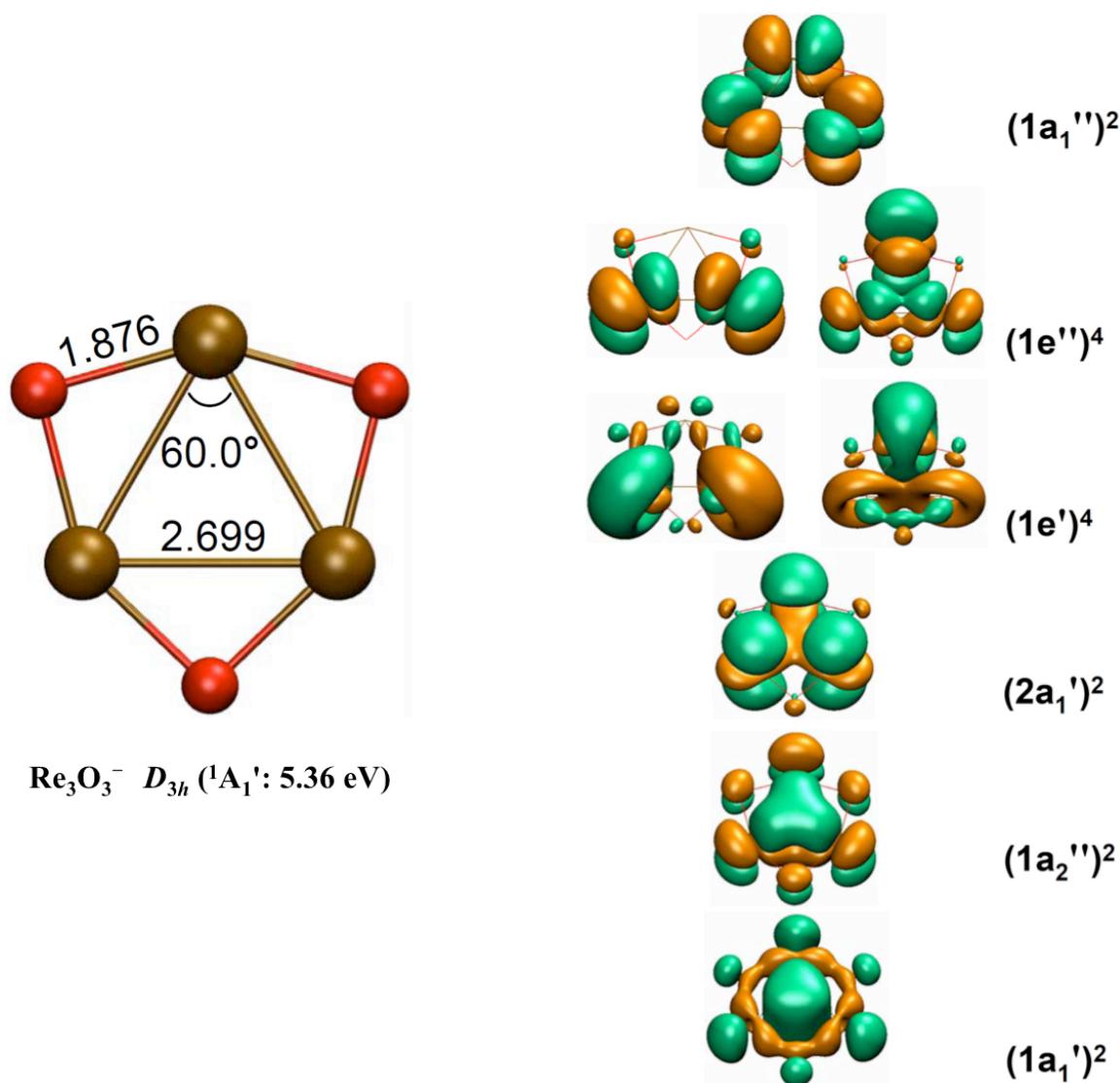


Table S1. Cartesian Coordinates for All Optimized Structures for Re_3O_3^- and Re_3O_3 at B3LYP/Re/Stuttgart+2f1g/O/aug-cc-pVTZ Level.

(a) Re_3O_3^-

	x	y	z		x	y	z
Re_3O_3^- ($\text{C}_{2v}^1 \text{A}_1$ 0.00 eV)				O	-3.161163	-0.289897	0.000000
Re	0.000000	1.403968	-0.530269	O	3.161165	-0.289914	0.000000
Re	0.000000	0.000000	1.302774				
Re	0.000000	-1.403968	-0.530269	Re_3O_3^- ($\text{C}_1^1 \text{A}$ 0.97 eV)			
O	0.000000	0.000000	-1.839219	Re	-0.470287	1.264645	0.134883
O	0.000000	3.103265	-0.215868	Re	1.452673	-0.283574	0.016967
O	0.000000	-3.103265	-0.215868	Re	-1.212081	-0.706957	-0.261339
				O	-2.351042	-1.415603	0.860504
Re_3O_3^- ($\text{C}_s^3 \text{A}''$ 0.05 eV)				O	1.847366	-1.411683	1.264570
Re	-1.421112	-0.481522	0.000000	O	2.657062	0.257466	-1.098615
Re	0.000000	1.303898	0.000000				
Re	1.427331	-0.578406	0.000000	Re_3O_3^- ($\text{C}_1^5 \text{A}$ 1.07 eV)			
O	-0.066257	-1.824300	0.000000	Re	-1.338828	-0.468467	0.018076
O	-3.122358	-0.147669	0.000000	Re	1.376670	-0.602294	-0.173536
O	3.130307	-0.315257	0.000000	Re	0.133185	1.392349	0.052840
				O	-2.218265	-0.727672	-1.456399
Re_3O_3^- ($\text{C}_s^3 \text{A}''$ 0.28 eV)				O	-1.959280	-0.976834	1.556340
Re	0.451255	-0.270984	1.417659	O	2.574165	-1.310382	0.862119
Re	-1.144063	0.666436	0.000000				
Re	0.451255	-0.270984	-1.417659	Re_3O_3^- ($\text{C}_s^3 \text{A}''$ 1.25 eV)			
O	1.362050	-1.173570	0.000000	Re	-0.811076	1.060054	0.000000
O	0.451255	0.003340	3.126534	Re	1.344133	0.587820	0.000000
O	0.451255	0.003340	-3.126534	Re	-0.653789	-1.357718	0.000000
				O	-0.811076	-2.179861	1.515888
Re_3O_3^- ($\text{C}_{2v}^5 \text{A}_1$ 0.51 eV)				O	-0.811076	-2.179861	-1.515888
Re	0.000000	1.426503	-0.544321	O	2.754023	1.639511	0.000000
Re	0.000000	0.000000	1.352087				
Re	0.000000	-1.426503	-0.544321	Re_3O_3^- ($\text{C}_1^1 \text{A}$ 1.34 eV)			
O	0.000000	0.000000	-1.826916	Re	-0.596135	1.136863	-0.175702
O	0.000000	3.142620	-0.321443	Re	-1.077716	-1.083283	0.065582
O	0.000000	-3.142620	-0.321443	Re	1.426319	-0.184616	0.058328
				O	0.586282	-1.861898	-0.347943
Re_3O_3^- ($\text{C}_s^3 \text{A}'$ 0.85 eV)				O	-1.198126	2.443608	0.808479
Re	-1.447446	-0.528157	0.000000	O	2.932461	0.646760	0.025015
Re	0.000000	1.310229	0.000000				
Re	1.447445	-0.528157	0.000000				
O	0.000001	-1.800639	0.000000				

Re ₃ O ₃ ⁻ (C _s ⁵ A' 1.41 eV)							
Re	0.626165	-0.214533	1.341095	o	0.000000	-1.614716	0.763657
Re	-1.214662	0.551493	0.000000	o	0.000000	1.614716	0.763657
Re	0.626165	-0.214533	-1.341095	o	0.000000	0.000000	3.430433
o 0.626165 -1.692650 2.234621				Re ₃ O ₃ ⁻ (C _s ⁷ A' 1.79 eV)			
o	0.626165	-1.692650	-2.234621	Re	-0.232511	1.646780	0.000000
o	-1.605476	2.237534	0.000000	Re	0.153093	-1.079040	1.109981
Re ₃ O ₃ ⁻ (C ₁ ³ A 1.44 eV)				Re	0.153093	-1.079040	-1.109981
Re	-1.415711	-0.207770	-0.002278	o	0.153093	0.814659	-1.654747
Re	0.623095	1.210083	0.030519	o	0.153093	0.814659	1.654747
Re	1.311376	-0.825871	0.001013	o	-0.996877	3.164114	0.000000
O	-1.995948	-0.647474	1.570394	Re ₃ O ₃ ⁻ (C _s ⁷ A" 1.96 eV)			
O	-2.561382	0.564593	-1.041485	Re	-0.680542	1.159643	0.000000
O	-0.306056	-1.571255	-0.803166	Re	0.420134	-0.789182	1.175867
Re ₃ O ₃ ⁻ (C ₁ ³ A 1.55 eV)				Re	0.420134	-0.789182	-1.175867
Re	-0.877177	-1.050805	0.268888	o	0.420134	1.155136	-1.569584
Re	-0.651127	1.240941	-0.194502	o	0.420134	1.155136	1.569584
Re	1.429560	-0.224486	-0.162576	o	-2.337689	1.615249	0.000000
o	-1.530557	-2.019108	-0.999691	Re ₃ O ₃ ⁻ (C ₁ ³ A 2.05eV)			
o	2.895011	-0.036256	0.742118	Re	1.433994	0.000000	0.022366
o	-0.438738	2.377397	1.084366	Re	-0.831774	1.127915	-0.035621
Re ₃ O ₃ ⁻ (C _s ³ A" 1.57 eV)				Re	-0.831774	-1.127915	-0.035621
Re	1.167437	0.870382	0.000000	O	2.264141	-0.000001	-1.494456
Re	-0.579372	-0.381874	1.220937	O	2.254404	0.000001	1.546973
Re	-0.579372	-0.381874	-1.220937	O	-2.366468	0.000000	0.405691
O	1.077241	2.591912	0.000000	Re ₃ O ₃ ⁻ (C _{3v} ³ A ₁ 2.08 eV)			
O	-0.579372	-1.795798	-2.220404	Re	0.000000	1.373175	-0.033261
O	-0.579372	-1.795798	2.220404	Re	-1.189205	-0.686588	-0.033261
Re ₃ O ₃ ⁻ (C _s ⁵ A' 1.66 eV)				Re	1.189205	-0.686588	-0.033261
Re	-0.659568	1.207394	0.000000	o	1.901356	1.097749	0.311819
Re	0.409164	-0.815395	1.103831	o	0.000000	-2.195497	0.311819
Re	0.409164	-0.815395	-1.103831	o	-1.901356	1.097749	0.311819
o	0.409164	1.142068	-1.569627	Re ₃ O ₃ ⁻ (C _s ⁵ A' 2.19 eV)			
o	0.409164	1.142068	1.569627	Re	-0.053829	-0.691450	1.196394
o	-2.306704	1.685206	0.000000	Re	0.157218	1.403012	0.000000
Re ₃ O ₃ ⁻ (C _{2v} ⁵ B ₁ 1.70 eV)				Re	-0.053829	-0.691450	-1.196394
Re	0.000000	0.000000	1.732931	o	-0.356982	-2.212616	0.000000
Re	0.000000	1.103673	-1.130879	o	-0.053829	1.012033	-2.014944
Re	0.000000	-1.103673	-1.130879	o	-0.053829	1.012033	2.014944

Re ₃ O ₃ ⁻ (C _s ¹ A' 2.27 eV)				O	0.297036	2.071552	1.410430
Re	-0.085768	1.276017	0.000000	O	0.297036	2.071552	-1.410430
Re	-0.001144	-0.649271	1.244528	O	-2.148590	1.483261	0.000000
Re	-0.001144	-0.649271	-1.244528	Re ₃ O ₃ ⁻ (D _{3h} ³ A ₁ ' 3.06 eV)			
o	-0.001144	1.056587	-2.035880	Re	0.000000	1.399206	0.000000
o	0.827810	-1.902002	0.000000	Re	1.211748	-0.699603	0.000000
o	-0.001144	1.056587	2.035880	Re	-1.211748	-0.699603	0.000000
Re ₃ O ₃ ⁻ (C _{2v} ³ B ₂ 2.31 eV)				o	0.000000	3.126660	0.000000
Re	0.000000	0.000000	1.817455	o	-2.707767	-1.563330	0.000000
Re	0.000000	1.052293	-1.176329	o	2.707767	-1.563330	0.000000
Re	0.000000	-1.052293	-1.176329	Re ₃ O ₃ ⁻ (C _{2v} ¹ A ₁ 3.28 eV)			
o	0.000000	-1.507770	0.750071	Re	0.000000	0.000000	1.383503
o	0.000000	1.507770	0.750071	Re	0.000000	1.132912	-0.689097
o	0.000000	0.000000	3.517379	Re	0.000000	-1.132912	-0.689097
Re ₃ O ₃ ⁻ (C _s ⁵ A" 2.35 eV)				o	0.000000	-1.950984	1.132741
Re	1.300609	0.042268	0.000000	o	0.000000	0.000000	-2.315255
Re	-0.683760	-0.200754	1.304654	o	0.000000	1.950984	1.132741
Re	-0.683760	-0.200754	-1.304654	Re ₃ O ₃ ⁻ (C _{2v} ⁵ A ₂ 3.65 eV)			
O	1.994805	1.636828	0.000000	Re	0.000000	1.268869	-0.688691
O	-0.683760	0.865524	-2.661830	Re	0.000000	0.000000	1.371110
O	-0.683760	0.865524	2.661830	Re	0.000000	-1.268869	-0.688691
Re ₃ O ₃ ⁻ (C _{2v} ⁵ A ₁ 2.35 eV)				o	-1.240393	0.000000	-1.531606
Re	0.000000	0.000000	1.393391	o	1.240393	0.000000	-1.531606
Re	0.000000	1.195497	-0.681868	o	0.000000	0.000000	3.122020
Re	0.000000	-1.195497	-0.681868	Re ₃ O ₃ ⁻ (C _s ⁷ A" 3.83 eV)			
o	0.000000	-2.061057	0.984800	Re	-0.155951	-0.663624	1.285141
o	0.000000	0.000000	-2.247625	Re	0.406010	1.318069	0.000000
o	0.000000	2.061057	0.984800	Re	-0.155951	-0.663624	-1.285141
Re ₃ O ₃ ⁻ (C _s ¹ A' 2.45 eV)				o	0.840471	-1.755068	0.000000
Re	-0.748127	1.194124	0.000000	o	-1.566776	-1.120664	0.000000
Re	0.450824	-0.807148	1.114338	o	-0.155951	2.961787	0.000000
Re	0.450824	-0.807148	-1.114338	Re ₃ O ₃ ⁻ (C _{2v} ¹ A ₁ 4.29 eV)			
o	0.450824	1.061950	-1.505050	Re	0.000000	1.199939	-0.677833
o	0.450824	1.061950	1.505050	Re	0.000000	0.000000	1.345203
o	-2.340905	1.815208	0.000000	Re	0.000000	-1.199939	-0.677833
Re ₃ O ₃ ⁻ (C _s ¹ A' 2.49 eV)				o	-1.331727	0.000000	-1.503500
Re	-0.428256	1.321165	0.000000	o	1.331727	0.000000	-1.503500
Re	0.297036	-0.960655	1.051710	o	0.000000	0.000000	3.105083
Re	0.297036	-0.960655	-1.051710				

Re₃O₃⁻ (D_{3h} ¹A₁, 5.36 eV)

Re	0.000000	1.558476	0.000000
Re	1.349679	-0.779238	0.000000
Re	-1.349679	-0.779238	0.000000
O	-1.802856	1.040879	0.000000
O	0.000000	-2.081759	0.000000
O	1.802856	1.040879	0.000000

(b) Re₃O₃

	x	y	z		x	y	z
Re ₃ O ₃ (C _{2v} ² A ₁ 0.00 eV)				O	0.000000	-3.086394	-0.175211
Re	0.000000	1.406000	-0.525145	Re ₃ O ₃ (C _{2v} ⁴ A ₁ 1.01 eV)			
Re	0.000000	0.000000	1.288476	Re	0.000000	1.441400	-0.533688
Re	0.000000	-1.406000	-0.525145	Re	0.000000	0.000000	1.327260
O	0.000000	0.000000	-1.832466	Re	0.000000	-1.441400	-0.533688
O	0.000000	3.081623	-0.200262	O	0.000000	0.000000	-1.813079
O	0.000000	-3.081623	-0.200262	O	0.000000	3.136665	-0.311667
Re ₃ O ₃ (C _s ⁴ A" 0.30 eV)				O	0.000000	-3.136665	-0.311667
Re	-1.406889	-0.453066	0.000000	Re ₃ O ₃ (C _{2v} ² B ₁ 0.83 eV)			
Re	0.000000	1.327910	0.000000	Re	0.000000	1.434753	-0.519306
Re	1.415142	-0.623222	0.000000	Re	0.000000	0.000000	1.256809
O	-0.106570	-1.830974	0.000000	Re	0.000000	-1.434753	-0.519306
O	-3.079309	-0.078438	0.000000	O	0.000000	0.000000	-1.819969
O	3.108510	-0.449547	0.000000	O	0.000000	3.093323	-0.112813
Re ₃ O ₃ (C _{2v} ⁴ B ₁ 0.48 eV)				O	0.000000	-3.093323	-0.112813
Re	0.000000	1.401998	-0.539216	Re ₃ O ₃ (C _{2v} ² A ₂ 0.93 eV)			
Re	0.000000	0.000000	1.338106	Re	0.000000	1.419047	-0.523395
Re	0.000000	-1.401998	-0.539216	Re	0.000000	0.000000	1.299482
O	0.000000	0.000000	-1.830578	Re	0.000000	-1.419047	-0.523395
O	0.000000	3.093576	-0.301932	O	0.000000	0.000000	-1.807975
O	0.000000	-3.093576	-0.301932	O	0.000000	3.108654	-0.280505
Re ₃ O ₃ (C _{2v} ⁴ A ₂ 0.49 eV)				O	0.000000	-3.108654	-0.280505
Re	0.000000	1.417064	-0.534708	Re ₃ O ₃ (C _{2v} ⁶ A ₁ 1.19 eV)			
Re	0.000000	0.000000	1.302951	Re	0.000000	1.457350	-0.560025
Re	0.000000	-1.417064	-0.534708				
O	0.000000	0.000000	-1.838965				
O	0.000000	3.086394	-0.175211				

Re	0.000000	0.000000	1.390707	O	0.117973	1.151095	1.848650
Re	0.000000	-1.457350	-0.560025	$\text{Re}_3\text{O}_3 (\text{C}_s \text{ }^4\text{A}'' \text{ 1.81 eV})$			
O	0.000000	0.000000	-1.811565	Re	-0.248178	1.369447	0.000000
O	0.000000	3.151060	-0.362924	Re	0.078959	-0.680357	1.182501
O	0.000000	-3.151060	-0.362924	Re	0.078959	-0.680357	-1.182501
$\text{Re}_3\text{O}_3 (\text{C}_1 \text{ }^2\text{A} \text{ 1.63 eV})$				O	0.078959	1.010310	-1.988715
Re	-0.560699	1.275027	0.008553	O	0.688276	-2.102487	0.000000
Re	1.476960	-0.230299	0.029988	O	0.078959	1.010310	1.988715
Re	-1.155747	-0.800416	-0.164550	$\text{Re}_3\text{O}_3 (\text{C}_1 \text{ }^2\text{A} \text{ 2.00 eV})$			
O	-2.263035	-1.415897	1.001300	Re	1.527182	-0.109708	0.011984
O	2.156788	-0.362801	1.595548	Re	-0.848245	1.111968	-0.117091
O	2.351425	-0.511719	-1.415513	Re	-1.179918	-0.966418	0.097130
$\text{Re}_3\text{O}_3 (\text{C}_1 \text{ }^4\text{A} \text{ 1.42 eV})$				O	0.573007	-1.553231	-0.601933
Re	-0.472312	1.314751	0.053682	O	0.906410	1.429311	0.805145
Re	1.425890	-0.280779	0.020997	O	3.217282	-0.212090	-0.128427
Re	-1.213929	-0.785785	-0.211926	$\text{Re}_3\text{O}_3 (\text{C}_{2v} \text{ }^4\text{A}_2 \text{ 2.03 eV})$			
O	-2.006718	-1.364421	1.184984	Re	0.000000	0.000000	1.773045
O	2.122041	-0.649579	1.540749	Re	0.000000	1.078546	-1.147404
O	2.325466	-0.312748	-1.439040	Re	0.000000	-1.078546	-1.147404
$\text{Re}_3\text{O}_3 (\text{C}_1 \text{ }^6\text{A} \text{ 1.70 eV})$				O	0.000000	-1.567134	0.721686
Re	-0.351194	1.455962	0.075068	O	0.000000	1.567134	0.721686
Re	1.362655	-0.374433	0.006156	O	0.000000	0.000000	3.448156
Re	-1.260536	-0.754656	-0.198295	$\text{Re}_3\text{O}_3 (\text{C}_1 \text{ }^4\text{A} \text{ 2.89 eV})$			
O	-1.922870	-1.758043	1.002543	Re	0.429365	1.249965	-0.163039
O	1.977161	-0.849625	1.527410	Re	1.032562	-1.007948	-0.135590
O	2.280789	-0.456771	-1.432410	Re	-1.484182	-0.343810	-0.083071
$\text{Re}_3\text{O}_3 (\text{C}_s \text{ }^4\text{A}' \text{ 1.86 eV})$				O	1.379314	2.008947	1.041667
Re	0.627875	-0.170080	1.363721	O	-2.527334	0.360019	1.046695
Re	-1.233774	0.482957	0.000000	O	1.356661	-1.414650	1.490074
Re	0.627875	-0.170080	-1.363721	$\text{Re}_3\text{O}_3 (\text{C}_s \text{ }^4\text{A}' \text{ 3.66 eV})$			
O	0.627875	-1.758122	1.957737	Re	0.160198	-0.681889	1.169324
O	0.627875	-1.758122	-1.957737	Re	-0.435097	1.347930	0.000000
O	-1.461772	2.177513	0.000000	Re	0.160198	-0.681889	-1.169324
$\text{Re}_3\text{O}_3 (\text{C}_s \text{ }^4\text{A}' \text{ 1.88 eV})$				O	1.709370	-0.872661	0.000000
Re	-0.345518	1.356314	0.000000	O	-0.794239	-1.935426	0.000000
Re	0.117973	-0.689303	1.157623	O	0.160198	2.956667	0.000000
Re	0.117973	-0.689303	-1.157623				
O	0.117973	1.151095	-1.848650				
O	0.791292	-2.093209	0.000000				