

## SUPPORTING INFORMATION

# Optimization of inkjet-printed PEDOT:PSS electrodes on plasma-modified PDMS composites

*Alessandro Chiolerio\*<sup>1</sup>, Paola Rivolo<sup>2</sup>, Samuele Porro<sup>1</sup>, Stefano Stassi<sup>1,2</sup>, Serena Ricciardi<sup>2</sup>, Pietro Mandracci<sup>2</sup>, Giancarlo Canavese<sup>1</sup>, Katarzyna Bejtko<sup>1</sup> and Candido Fabrizio Pirri<sup>1,2</sup>*

<sup>1</sup> Istituto Italiano di Tecnologia, Center for Space Human Robotics, Corso Trento 21, 10129 Torino

<sup>2</sup> Politecnico di Torino, Applied Science and Technology Department, Corso Duca degli Abruzzi 24, 10129 Torino

### **Description of Surface Energy estimation**

An insight into the interactions between liquid and solid surfaces is possible through the Owens and Wendt geometric mean approach [Owens, D. K.; Wendt, R. C. Estimation of the surface free energy of polymers. *J. Appl. Polym. Sci.* 1969, 13, 1741-1747]. These authors developed the idea that both the solid superficial energy (defined both as  $\sigma$  or  $\sigma_s$ ) and the liquid surface tension (defined both as  $\gamma$  or  $\sigma_l$ ) can be separated into two terms: i) a polar contribution, due to Coulomb interactions between

permanent or induced dipoles; ii) a dispersive contribution, due to van der Waals forces, as described by:

$$\sigma_l = \sigma_l^d + \sigma_l^p \quad \text{and} \quad \sigma_s = \sigma_s^d + \sigma_s^p \quad \text{eqn (1)}$$

where  $\sigma_l^d$  and  $\sigma_l^p$  represent the dispersive and polar parts of the liquid, while  $\sigma_s^d$  and  $\sigma_s^p$  stand for the respective dispersive and polar contributions of the solid. The interfacial energy from the contributions of the liquid and solid ( $\sigma_{s,l}$ ) is given by :

$$\sigma_{s,l} = \sigma_s + \sigma_l - 2 \left[ \sqrt{(\sigma_s^d \sigma_l^d)} + \sqrt{(\sigma_s^p \sigma_l^p)} \right] \quad \text{eqn (2)}$$

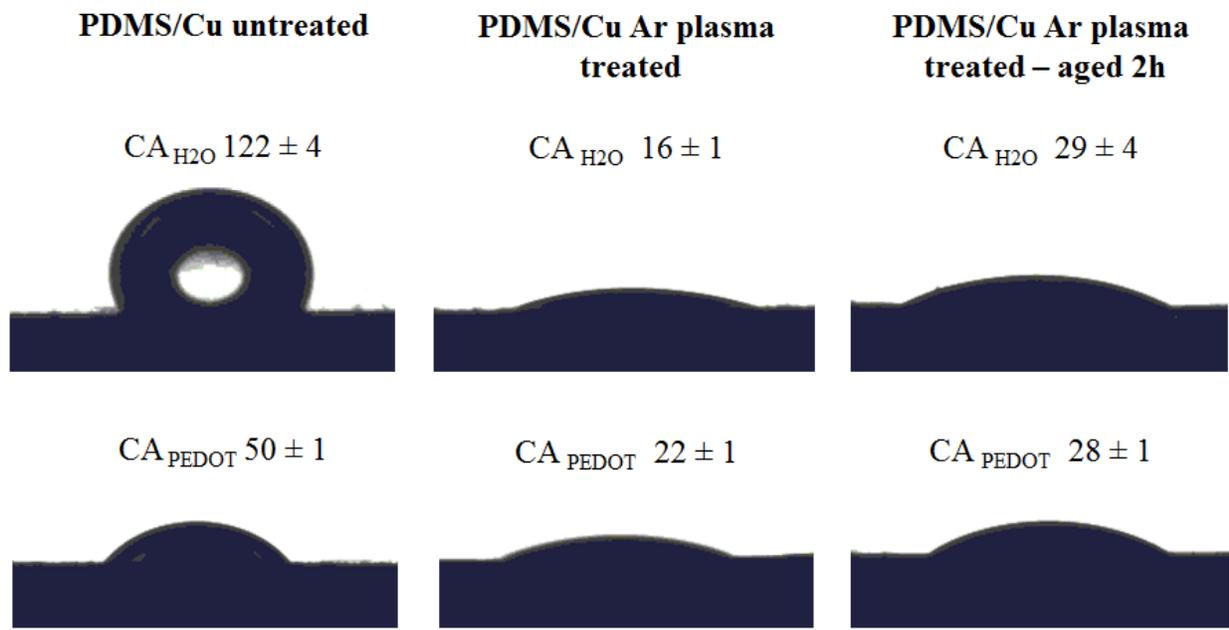
Taking into account Young's formula (coming from the equilibrium of the forces at the edge of a drop on a solid surface):

$$\sigma_s = \sigma_{l,s} + \sigma_l \cos \theta \quad \text{eqn(3)}$$

an equation in the following form is obtained:

$$y = a x + b, \text{ with } y = \frac{1 + \cos \theta}{2} \cdot \frac{\sigma_l}{\sqrt{\sigma_l^d}}, \quad x = \sqrt{\sigma_l^p / \sigma_l^d}, \quad a = \sqrt{\sigma_s^p} \quad \text{and} \quad b = \sqrt{\sigma_s^d} \quad \text{eqn (4)}$$

It should be noticed that both entities  $x$  and  $y$  depend only on the liquid, while the entities  $a$  and  $b$  depend on the solid. Considering a series of different liquids, plotting  $y$  versus  $x$  allows calculating  $\sigma_s^p$  from the slope of the fitted line and  $\sigma_s^d$  from the intersection with  $y$  axis.



**Figure S1:** Comparison of water and PEDOT:PSS Contact Angles on untreated, APP-freshly-treated and 2h aged Cu-PDMS substrates.

**Table S2** containing all experimental data:

**Table S2 part A** Sample experimental data: APP parameters, IjP parameters, IA statistical parameters.

APP power (J s <sup>-2</sup> )	APP # passes	Time elapsed since treatment (min)	APP hardness (J)	IjP # passes	Printing density (dpi)
0	0	1	0	3	157.48
0	0	1	0	5	157.48
0	0	1	0	10	157.48
400	3	735	1.632653061	1	78.74
400	3	737	1.628222524	1	157.48
400	3	742	1.617250674	1	314.96
550	4	720	3.055555556	1	78.74
550	4	722	3.047091413	1	157.48

550	4	727	3.026134801	1	314.96
1100	5	60	91.66666667	1	78.74
1100	5	62	88.70967742	1	157.48
1100	5	65	84.61538462	1	236.22
1100	5	69	79.71014493	1	314.96
1100	5	75	73.33333333	2	59.055
1100	5	77	71.42857143	2	78.740
1100	5	79	69.62025316	2	157.480
1100	5	140	39.28571429	1	78.740
1100	5	142	38.73239437	1	157.480
1100	5	145	37.93103448	1	236.220
1100	5	149	36.91275168	1	314.960

**Table S2 part B** (continued) Sample experimental data: APP parameters, IjP parameters, IA statistical parameters.

Engineering volume (in <sup>-1</sup> )	Fill factor	IA Peak #1 width (px)	IA Peak #1 height (-)	IA Peak #2 width (px)	IA Peak #2 height (-)
472.44	0.268837	N/A	N/A	N/A	N/A
787.4	0.485287	N/A	N/A	N/A	N/A
1574.8	0.577513	N/A	N/A	N/A	N/A
78.74	1.000000	1.02922	0.51501	N/A	N/A
157.48	1.000000	23.09119	0.14565	N/A	N/A
314.96	1.000000	73.68934	0.15750	N/A	N/A
78.74	1.000000	22.11744	0.11846	N/A	N/A
157.48	1.000000	6.56777	0.10247	N/A	N/A

314.96	1.000000	15.22623	0.09958	5.37597	0.66963
78.74	1.000000	2.60774	0.19554	2.62196	0.15238
157.48	1.000000	28.94776	0.08152	N/A	N/A
236.22	1.000000	5.03222	0.75280	N/A	N/A
314.96	1.000000	48.47230	0.33863	N/A	N/A
118.11	1.000000	11.89332	0.05854	N/A	N/A
157.48	1.000000	6.65318	0.12446	99.71703	0.92144
314.96	1.000000	7.36850	0.09738	5.71885	0.11907
78.74	1.000000	8.21996	0.39893	N/A	N/A
157.48	1.000000	0.53899	0.33977	3.56253	0.23941
236.22	1.000000	4.75590	0.20900	7.83212	0.10216
314.96	1.000000	2.96163	0.13138	6.18320	0.09578

**Table S2 part C** (continued) Sample experimental data: APP parameters, IjP parameters, IA statistical parameters.

Fit R <sup>2</sup>	IA Peak #1 broadness	IA Peak #2 broadness
N/A	N/A	N/A
N/A	N/A	N/A
N/A	N/A	N/A
0.73255	1.99845	N/A
0.85412	158.53889	N/A
0.60800	467.86883	N/A
0.69580	186.70809	N/A
0.47281	64.09456	N/A
0.79416	152.90450	8.028269343
0.88123	13.33609	17.20672004

0.53308	355.10010	N/A
0.57376	6.68467	N/A
0.43611	143.14237	N/A
0.49883	203.16570	N/A
0.64124	53.45637	108.2186903
0.74956	75.66749	48.02931049
0.97989	20.60502	N/A
0.94397	1.58634	14.88045612
0.92472	22.75550	76.66523101
0.86606	22.54247	64.5562748