## Supplementary data

Shape-Memory Capability of Binary Multiblock Copolymer Blends with Hard and Switching Domains Provided by Different Components<br>Marc Behl, Ute Ridder ${ }^{1}$, Yakai Feng ${ }^{2}$, Steffen Kelch ${ }^{3}$, Andreas Lendlein ${ }^{*}$<br>Institute of Polymer Research, GKSS Research Center Geesthacht GmbH, 14513 Teltow, Germany<br>*To whom correspondence should be addressed. Email: andreas.lendlein@gkss.de, Fax: (+49) 3328-352452<br>${ }^{1}$ present address: Freudenberg Forschungsdienste KG, 69465 Weinheim, Germany<br>${ }^{2}$ present address: Department of Polymer Science and Technology, Tianjin University, 92<br>Weijin Road, Tianjin 300072, People Republic of China<br>${ }^{3}$ present address: Sika Technology AG, Tüffenwies 16, CH-8048 Zürich, Switzerland

Table S1a. Mechanical properties of polymer blends obtained by co-precipitation method determined in tensile tests. E: E-Modulus, $\sigma_{y}$ : stress at yield, $\varepsilon_{y}$ : elongation at yield, $\sigma_{b}$ : stress at break, $\varepsilon_{b}$ : elongation at break.

| Polymer blend ID ${ }^{\text {a) }}$ | $\begin{gathered} \mathrm{E}^{\mathrm{b}} \\ (\mathrm{MPa}) \\ \hline \end{gathered}$ | $\begin{gathered} \sigma_{\mathrm{y}}{ }^{\mathrm{b})} \\ (\mathrm{MPa}) \\ \hline \end{gathered}$ | $\begin{aligned} & \varepsilon_{\mathrm{y}}{ }^{\mathrm{b})} \\ & (\%) \\ & \hline \end{aligned}$ | $\begin{gathered} \sigma_{\mathrm{b}}{ }^{\mathrm{b})} \\ (\mathrm{MPa}) \\ \hline \end{gathered}$ | $\begin{aligned} & \varepsilon_{b}{ }^{\text {b) }} \\ & (\%) \\ & \hline \end{aligned}$ | $\begin{gathered} E^{\mathrm{c})} \\ (\mathrm{MPa}) \\ \hline \end{gathered}$ | $\begin{gathered} \sigma_{\mathrm{b}}{ }^{\mathrm{c})} \\ (\mathrm{MPa}) \\ \hline \end{gathered}$ | $\begin{aligned} & \varepsilon_{b}{ }^{\text {c) }} \\ & (\%) \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PDA(42)/PCA(47)[21/24/42] | $15.5 \pm 1.3$ | - | - | $12.5 \pm 3.5$ | 1,295 $\pm 335$ | $2.3 \pm 0.4$ | $1.1 \pm 0.2$ | $240 \pm 40$ |
| PDA(42)/PCA(47)[28/16/42] | $23.3 \pm 3.6$ | - | - | $9.5 \pm 2.1$ | $1,070 \pm 30$ | $4.5 \pm 0.4$ | $1.9 \pm 0.2$ | $270 \pm 20$ |
| PDA(42)/PCA(47)[34/10/44] | $16.8 \pm 2.2$ | - | - | $5.5 \pm 0.7$ | $445 \pm 105$ | $7.2 \pm 1.5$ | $2.5 \pm 0.1$ | $210 \pm 70$ |
| PDA(42)/PCA(68)[14/45/28] | $32.7 \pm 1.3$ | $4.3 \pm 0.8$ | $35 \pm 7$ | $12.5 \pm 0.2$ | $860 \pm 95$ | $0.7 \pm 0.5$ | $0.8 \pm 0.2$ | $1,055 \pm 385$ |
| PDA(42)/PCA(68)[21/34/32] | $25.6 \pm 0.8$ | $5.1 \pm 0.2$ | $58 \pm 11$ | $9.6 \pm 3.0$ | $795 \pm 270$ | $2.6 \pm 0.1$ | $1.0 \pm 0.1$ | $325 \pm 60$ |
| PDA(42)/PCA(68)[28/22/36] | $24.5 \pm 2.1$ | - | - | $8.9 \pm 1.6$ | $925 \pm 180$ | $4.1 \pm 0.6$ | $2.0 \pm 0.2$ | $320 \pm 105$ |
| PDA(42)/PCA(68)[34/14/40] | $16.9 \pm 0.8$ | - | - | $10.5 \pm 0.7$ | 1,280 $\pm 1$ | $5.9 \pm 0.1$ | $1.9 \pm 0.1$ | $75 \pm 1$ |
| PDA(50)/PCA(47)[25/24/37] | $15.9 \pm 2.4$ | $4.9 \pm 0.0$ | $51 \pm 3$ | $9.8 \pm 0.8$ | $750 \pm 110$ | $6.5 \pm 0.8$ | $2.3 \pm 0.1$ | $410 \pm 15$ |
| PDA(50)/PCA(47)[33/16/37] | $20.5 \pm 4.6$ | $5.6 \pm 0.4$ | $51 \pm 10$ | $10.6 \pm 1.1$ | $705 \pm 160$ | $10.0 \pm 1.7$ | $2.7 \pm 0.0$ | $340 \pm 10$ |
| PDA(50)/PCA(47)[40/9/37] | $32.0 \pm 2.0$ | $6.3 \pm 0.2$ | $58 \pm 6$ | $11.8 \pm 0.6$ | $845 \pm 90$ | $14.9 \pm 2.8$ | $5.0 \pm 0.2$ | $575 \pm 90$ |
| PDA(50)/PCA(68)[17/45/25] | $33.9 \pm 1.8$ | - | - | $9.1 \pm 0.2$ | $970 \pm 100$ | $1.7 \pm 0.1$ | $1.2 \pm 0.0$ | $550 \pm 95$ |
| PDA(50)/PCA(68)[25/34/28] | $36.0 \pm 2.0$ | - | - | $13.6 \pm 1.2$ | $1,130 \pm 150$ | $4.9 \pm 0.5$ | $2.2 \pm 0.1$ | $460 \pm 70$ |
| PDA(50)/PCA(68)[34/22/31] | $37.0 \pm 2.1$ | $5.1 \pm 0.3$ | $78 \pm 9$ | $13.8 \pm 1.8$ | 1,055 $\pm 25$ | $7.1 \pm 1.0$ | $3.0 \pm 0.1$ | $465 \pm 65$ |
| PDA(50)/PCA(68)[40/14/34] | $41.7 \pm 3.1$ | $5.8 \pm 0.3$ | $72 \pm 12$ | $15.5 \pm 1.6$ | 1,510 $\pm 20$ | $17.6 \pm 3.1$ | $5.0 \pm 0.2$ | $480 \pm 40$ |

a) The three numbers in squared brackets of the sample ID give the content in $w t \%$ of PPDO, PCL and PADOH in the binary polymer blends.
b) determined at $20^{\circ} \mathrm{C}$
c) determined at $50^{\circ} \mathrm{C}$

Table S1b. Mechanical properties of polymer blends obtained by co-extrusion method determined in tensile tests. E: E-Modulus, $\sigma_{y}$ : stress at yield,
$\varepsilon_{\mathrm{y}}$ : elongation at yield, $\sigma_{\mathrm{b}}$ : stress at break, $\varepsilon_{\mathrm{b}}$ : elongation at break.

| Polymer blend $\mathrm{ID}^{\text {a) }}$ | $\begin{gathered} E^{b)} \\ (\mathrm{MPa}) \\ \hline \end{gathered}$ | $\begin{gathered} \sigma_{\mathrm{y}}{ }^{\mathrm{b})} \\ (\mathrm{MPa}) \\ \hline \end{gathered}$ | $\begin{aligned} & \varepsilon_{\mathrm{y}}{ }^{\mathrm{b})} \\ & (\%) \\ & \hline \end{aligned}$ | $\begin{gathered} \sigma_{\mathrm{b}}{ }^{\mathrm{b})} \\ (\mathrm{MPa}) \\ \hline \end{gathered}$ | $\begin{aligned} & \varepsilon_{b}{ }^{\text {b) }} \\ & (\%) \\ & \hline \end{aligned}$ | $\begin{gathered} \mathrm{E}^{\mathrm{c})} \\ (\mathrm{MPa}) \\ \hline \end{gathered}$ | $\begin{gathered} \sigma_{\mathrm{b}}{ }^{\mathrm{c})} \\ (\mathrm{MPa}) \\ \hline \end{gathered}$ | $\begin{aligned} & \varepsilon_{b}{ }^{\text {c) }} \\ & (\%) \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PDA(42)/PCA(47)[21/24/42] | $23.8 \pm 2.4$ | - | - | $8.8 \pm 0.8$ | $735 \pm 60$ | $2.4 \pm 0.6$ | $0.7 \pm 0.1$ | $300 \pm 70$ |
| PDA(42)/PCA(47)[28/16/42] | $24.2 \pm 1.1$ | - | - | $6.6 \pm 0.7$ | $460 \pm 35$ | $7.0 \pm 0.8$ | $1.9 \pm 0.2$ | $240 \pm 75$ |
| PDA(42)/PCA(47)[34/10/44] | $27.3 \pm 2.4$ | - | - | $7.6 \pm 0.7$ | $530 \pm 65$ | $4.9 \pm 0.6$ | $1.9 \pm 0.5$ | $315 \pm 15$ |
| PDA(42)/PCA(68)[14/45/28] | $36.8 \pm 3.7$ | $4.5 \pm 0.2$ | $33 \pm 2$ | $16.4 \pm 1.6$ | $820 \pm 40$ | $0.3 \pm 0.3$ | $0.1 \pm 0.05$ | $360 \pm 60$ |
| PDA(42)/PCA(68)[21/34/32] | $39.4 \pm 1.2$ | $4.7 \pm 0.1$ | $39 \pm 2$ | $11.9 \pm 0.4$ | $705 \pm 20$ | $1.7 \pm 0.2$ | $0.5 \pm 0.1$ | $375 \pm 15$ |
| PDA(42)/PCA(68)[28/22/36] | $37.2 \pm 1.6$ | - | - | $8.0 \pm 0.4$ | $450 \pm 40$ | $3.4 \pm 0.9$ | $1.6 \pm 0.1$ | $375 \pm 45$ |
| PDA(42)/PCA(68)[34/14/40] | $38.4 \pm 4.1$ | - | - | $6.9 \pm 0.3$ | $305 \pm 20$ | $6.8 \pm 1.5$ | $2.5 \pm 0.5$ | $255 \pm 30$ |
| PDA(50)/PCA(47)[25/24/37] | $38.0 \pm 4.5$ | - | - | $12.4 \pm 0.8$ | $690 \pm 50$ | $8.1 \pm 4.1$ | $2.9 \pm 0.5$ | $320 \pm 95$ |
| PDA(50)/PCA(47)[33/16/37] | $39.4 \pm 4.6$ | - | - | $14.8 \pm 0.8$ | $820 \pm 40$ | $7.3 \pm 0.6$ | $3.0 \pm 0.2$ | $465 \pm 55$ |
| PDA(50)/PCA(47)[40/9/37] | $54.1 \pm 4.0$ | - | - | $13.1 \pm 0.4$ | $605 \pm 40$ | $12.7 \pm 0.7$ | $5.0 \pm 0.3$ | $525 \pm 10$ |
| PDA(50)/PCA(68)[17/45/25] | $40.5 \pm 9.4$ | $4.1 \pm 0.6$ | $29 \pm 3$ | $16.7 \pm 0.7$ | $780 \pm 35$ | $4.1 \pm 1.3$ | $1.2 \pm 0.6$ | $310 \pm 125$ |
| PDA(50)/PCA(68)[25/34/28] | $45.2 \pm 4.9$ | $5.2 \pm 0.2$ | $35 \pm 3$ | $17.6 \pm 0.4$ | $755 \pm 15$ | $4.7 \pm 0.7$ | $2.0 \pm 0.1$ | $535 \pm 115$ |
| PDA(50)/PCA(68)[34/22/31] | $49.6 \pm 3.1$ | $6.0 \pm 0.1$ | $37 \pm 7$ | $13.5 \pm 1.0$ | $615 \pm 40$ | $9.0 \pm 1.4$ | $3.0 \pm 0.2$ | $410 \pm 65$ |
| PDA(50)/PCA(68)[40/14/34] | $60.3 \pm 5.9$ | $6.7 \pm 0.02$ | $33 \pm 6$ | $13.7 \pm 0.9$ | $640 \pm 1$ | $15.4 \pm 4.2$ | $5.4 \pm 0.1$ | $590 \pm 135$ |

a) The three numbers in squared brackets of the sample ID give the content in wt $\%$ of PPDO, PCL and PADOH in the polymer blends.
b) determined at $20^{\circ} \mathrm{C}$
c) determined at $50^{\circ} \mathrm{C}$

Table S2. Shape-memory properties of binary polymer blends obtained by co-precipitation and co-extrusion method determined in strain-controlled cyclic, thermomechanical tests. $\mathrm{T}_{\text {low }}=0^{\circ} \mathrm{C}, \mathrm{T}_{\text {high }}=50^{\circ} \mathrm{C}, \varepsilon_{\mathrm{m}}=100 \%, R_{f}(N)$ : strain fixity rate, $R_{r}(N)$ : strain recovery rate, $N$ : cycle number, $\bar{R}_{f, 1-5}$ : average of $R_{f}$ from $1^{\text {st }}$ to $5^{\text {th }}$ cycle, $\bar{R}_{\mathrm{r}, 2-4}$ : average of $R_{r}$ from $2^{\text {nd }}$ to $4^{\text {th }}$ cycle.

|  | co-precipitation |  |  |  | co-extrusion |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Polymer blend ID ${ }^{\text {a) }}$ | $\bar{R}_{f, 1-5}$ <br> (\%) | $\begin{gathered} R_{r}(1) \\ (\%) \end{gathered}$ | $\begin{gathered} R_{r}(2) \\ (\%) \end{gathered}$ | $\begin{gathered} \bar{R}_{r, 2-4} \\ (\%) \end{gathered}$ | $\bar{R}_{f, 1-5}$ <br> (\%) | $\begin{gathered} R_{r}(1) \\ (\%) \end{gathered}$ | $\begin{gathered} R_{r}(2) \\ (\%) \end{gathered}$ | $\bar{R}_{r, 2-4}$ <br> (\%) |
| PDA(42)/PCA(47)[21/24/42] | $81.9 \pm 0.8$ | 80.3 | 97.1 | $97.3 \pm 0.2$ | $86.6 \pm 0.5$ | 63.8 | 91.7 | $95.2 \pm 2.8$ |
| PDA(42)/PCA(47)[28/16/42] | $68.1 \pm 0.3$ | 73.9 | 96.3 | $98.1 \pm 1.6$ | $75.8 \pm 3.1$ | 67.7 | 93.9 | $95.1 \pm 1.3$ |
| PDA(42)/PCA(47)[34/10/44] | $66.9 \pm 1.0$ | 84.7 | 96.8 | $98.9 \pm 2.0$ | $73.2 \pm 2.7$ | 70.1 | 92.8 | $95.2 \pm 2.1$ |
| PDA(42)/PCA(68)[14/45/28] | $93.7 \pm 0.5$ | 76.6 | 94.5 | $97.4 \pm 3.9$ | $98.4 \pm 0.4$ | 59.5 | 82.2 | $84.0 \pm 3.1$ |
| PDA(42)/PCA(68)[21/34/32] | $92.2 \pm 0.3$ | 73.3 | 96.6 | $98.6 \pm 3.6$ | $95.7 \pm 0.3$ | 58.9 | 90.1 | $92.4 \pm 2.0$ |
| PDA(42)/PCA(68)[28/22/36] | $84.5 \pm 0.3$ | 72.8 | 97.2 | $98.2 \pm 0.9$ | $89.8 \pm 1.2$ | 68.2 | 92.2 | $96.1 \pm 3.5$ |
| PDA(42)/PCA(68)[34/14/40] | $72.8 \pm 0.3$ | 76.8 | 95.9 | $97.2 \pm 1.6$ | $87.4 \pm 0.3$ | 63.9 | 94.5 | $96.6 \pm 3.0$ |
| PDA(50)/PCA(47)[25/24/37] | $85.4 \pm 2.1$ | 63.8 | 95.1 | $95.1 \pm 3.0$ | $86.3 \pm 5.1$ | 62.5 | 96.2 | $96.6 \pm 0.9$ |
| PDA(50)/PCA(47)[33/16/37] | $80.9 \pm 0.3$ | 55.0 | 91.0 | $94.6 \pm 3.2$ | $79.6 \pm 0.6$ | 71.5 | 97.3 | $98.7 \pm 3.6$ |
| PDA(50)/PCA(47)[40/9/37] | $77.8 \pm 2.9$ | 63.8 | 92.0 | $95.1 \pm 3.0$ | $73.8 \pm 5.4$ | 67.7 | 93.9 | $95.8 \pm 3.5$ |
| PDA(50)/PCA(68)[17/45/25] | $96.3 \pm 0.8$ | 58.6 | 95.7 | $94.6 \pm 3.3$ | $99.1 \pm 1.2$ | 58.6 | 83.4 | $88.9 \pm 4.8$ |
| PDA(50)/PCA(68)[25/34/28] | $90.8 \pm 0.6$ | 55.3 | 94.4 | $94.0 \pm 1.5$ | $92.9 \pm 0.1$ | 61.6 | 93.6 | $95.0 \pm 1.7$ |
| PDA(50)/PCA(68)[34/22/31] | $86.4 \pm 1.1$ | 57.1 | 91.8 | $96.5 \pm 5.4$ | $89.7 \pm 1.8$ | 60.0 | 94.2 | $96.0 \pm 2.3$ |

a) The three numbers in squared brackets of the sample ID give the content in $\omega t \%$ of PPDO, PCL and PADOH in the polymer blends according to calculation.


Fig. S1. Comparison of the initially weighted quantity and the composition determined by ${ }^{1} \mathrm{H}$-NMRspectroscopy of polymer blends. The initially weighted quantity of the PDA-polymer and the PCA-polymer vary between $10: 1,6: 1,4: 1,2: 1,1: 1,1: 2$ and $1: 4$. (a) Polymer blends from solution and (b) polymer blends from extrusion.
$!\quad \mathrm{PDA}(42) / \mathrm{PCA}(47)$ (weight in quantity), $\exists \mathrm{PDA}(42) / \mathrm{PCA}(47)\left({ }^{1} \mathrm{H}-\mathrm{NMR}\right.$-spectroscopy),
( $\operatorname{PDA}(42) / \mathrm{PCA}(68)$ (weight in quantity), $\forall \mathrm{PDA}(42) / \mathrm{PCA}(68)\left({ }^{1} \mathrm{H}-\mathrm{NMR}\right.$-spectroscopy),
, $\mathrm{PDA}(50) / \mathrm{PCA}(47)$ (weight in quantity), / $\mathrm{PDA}(50) / \mathrm{PCA}(47)\left({ }^{1} \mathrm{H}-\mathrm{NMR}\right.$-spectroscopy),
$3 \mathrm{PDA}(50) / \mathrm{PCA}(68)$ (weight in quantity), $-\mathrm{PDA}(50) / \mathrm{PCA}(68)\left({ }^{1} \mathrm{H}-\mathrm{NMR}\right.$-spectroscopy)
(a)

(b)

(c)


Fig. S2. Glass transition temperatures $\mathrm{T}_{\mathrm{g}}$ of binary polymer blends from PDA and PCA as a function of weight content in blends. Filled symbols: polymer blends from co-precipitation: ! $\mathrm{T}_{\mathrm{g} 1} ;, \mathrm{T}_{\mathrm{g} 2} ; 7 \mathrm{~T}_{\mathrm{g} 3} ;$ hollow symbols: polymer blends from co-extrusion $\forall \mathrm{T}_{\mathrm{g} 1} ;-\mathrm{T}_{\mathrm{g} 2} ; 8 \mathrm{~T}_{\mathrm{g} 3}$. The error bars show the range of $\mathrm{T}_{\mathrm{g}}$. The color indexes the different series: black PDA(42)/PCA(47), red $\mathrm{PDA}(42) / \mathrm{PCA}(68)$, green $\mathrm{PDA}(50) / \mathrm{PCA}(47)$, blue $\mathrm{PDA}(50) / \mathrm{PCA}(68)$. a) $\mathrm{T}_{\mathrm{g} 1}$ denoted to PPDO; b) $\mathrm{T}_{\mathrm{g} 2}$ denoted to $\mathrm{PADOH} ; \mathrm{T}_{\mathrm{g} 3}$ denoted to PCL


Fig. S3. Stress-Strain diagrams of extruded polymer blends at room temperature: solid line = $\operatorname{PDA}(42) / \mathrm{PCA}(47)[21 / 24 / 42]$, dashed line $=\mathrm{PDA}(42) / \mathrm{PCA}(68)[14 / 45 / 28]$, dotted line $=$ $\operatorname{PDA}(50) / \mathrm{PCA}(47)[25 / 24 / 37]$, dash-dotted line $=\mathrm{PDA}(50) / \mathrm{PCA}(68)[25 / 34 / 28]$.


Fig. S4. AFM phase image of multiblock copolymers PDA(50) and PCA(47) as well as polymer blend PDA(50)/PCA(47)[25/24/37] surfaces at different temperatures. a: room temperature, b: $60{ }^{\circ} \mathrm{C}, \mathrm{c}$ : room temperature after cooling from $60^{\circ} \mathrm{C}$. Dark area $=$ soft phase, and bright area $=$ stiff phase. (phase image, scan size $10.0 \mu \mathrm{~m}$, scan rate 1 Hz , samples per line 512 , z range $60^{\circ}$ )


Fig. S5. WAXS diffractogram of multiblock copolymers (a) PCA(47) and (b) PDA(50) as well as polymer blend (c,d) PDA(50)/PCA(47)[25/24/37].

## Video S1

The video displays programming and recovery applied to two different multi-block copolymers and a binary polymer blend. Left: the PCL-based multiblock copolymer PCA(47); middle: binary blend $\operatorname{PDA}(50) / \mathrm{PCA}(47)[25 / 24 / 37]$ and right: the PPDO-based multi-block copolymer PDA(50). In part 1 of the video the permanent shape at $25^{\circ} \mathrm{C}$ is shown. In part 2 the temporary shape was programmed to each sample at $50^{\circ} \mathrm{C}$ and is shown at an environmental temperature of $25^{\circ} \mathrm{C}$ (part 2). In part 3 the thermally-induced shape-memory effect was triggered by heating to $50^{\circ} \mathrm{C}$ (part 3). Only the binary blend of the multi-block copolymers shows a shape-memory effect (sample in the middle).

