# Phase behavior of rounded hard-squares (Supplementary Information) 

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## 1 Simulation details and order parameters

The phase behavior of rounded-corner hard-squares (RCHS) was obtained using Monte Carlo (MC) simulations in the canonical $N V T,{ }^{1,2}$ isobaric-isothermal $N P T^{2-5}$ and isothermal-isostress $N \sigma_{P} T^{6}$ ensembles. In the $N \sigma_{P} T$ ensemble the shape of the box is allowed to change, which makes it specially attractive for simulations of systems at high-densities in order to stabilize crystalline phases that might not be commensurable with square simulation cells. Compression and expansion runs were used to map out the EoS of RCHS as a function of the roundness of the system $\zeta$, which is defined as $\zeta=\sigma /(L+\sigma)$. The compression runs were started from a low density isotropic state, and the pressure was increased in a sequential manner. Expansion runs were started from perfect crystal structures, which were determined using the method of Filio et al. ${ }^{7}$ In our simulations, a cycle is defined as $N$ Monte Carlo moves, where $N$ is the total number of particles. For the systems of $N=400$ and 1600 particles, particle translations, re-orientations, and box volume changes were chosen with probabilities of $47.5 \%, 47.5 \%$, and $5 \%$, respectively. Equal probabilities were used for isotropic and anisotropic changes of volume when required, i.e., $2.5 \%$ each. For the larger system of $N=4096$ particles, each cycle consists of 4096 particles translation or re-orientations, and approximately four box volume changes. $2.5 \times 10^{5} \mathrm{MC}$ cycles were used to equilibrate the system, followed by $1 \times 10^{6}$ production cycles to obtain ensemble averages. In the case of $N V T$ simulations, translation and rotations moves were chosen with equal probability ( $50 \%$ each one). $N V T$ simulations were only used for systems of 5625 particles, hence longer simulations were required in order to equilibrate the system. In this case $1 \times 10^{6}$ cycles were used to stabilize the system, followed by $2 \times 10^{6}$ cycles to obtain ensemble averages. In all cases, the allowed displacements, re-orientations, and volume changes were adjusted to get acceptance probabilities between 30-40\% (with the exception of the results presented in Fig. S15, where the re-orientation

[^0]moves were restricted to be less than $5^{\circ}$ ). In order to characterize the system, several order parameters (that have been defined in the main article) were calculated. We also report the results for the isothermal compressibility $\kappa_{T}^{*}=\kappa_{T} k_{B} T / A_{p}$ calculated from fluctuations of the total area of the system. ${ }^{8}$

In the figures shown below, we have used the following acronyms for the different phases: I=isotropic, RHX=hexagonal rotator crystal, $\mathrm{RB}=$ rhombic, $\mathrm{T}=$ tetratic, and $\mathrm{PC}=$ polycrystalline.

## 2 Results for perfect hard squares using $N=196$ particles



Figure S1: Equation of state for 196 RCHS with $\zeta=0.01$ obtained by compression $(\diamond)$ and expansion ( $\triangle$ ) runs. The results are compared with the simulations results of the system of 196 perfect hard-squares reported by Wojciechowski and Frenkel ${ }^{9}$ obtained by compression (o) and expansion ( $\square$ ) runs .

|  |  | $N=196$ |  |
| ---: | :---: | :---: | :---: |
| $P^{*}$ | $\eta$ (compression) | $\eta$ (expansion) | $\eta$ (reference 9 ) |
| 20.0 | $0.8715 \pm 0.0023$ | $0.8716 \pm 0.0018$ | 0.8715 |
| 15.0 | $0.8365 \pm 0.0033$ | $0.8370 \pm 0.0021$ | 0.8362 |
| 12.0 | $0.8019 \pm 0.0030$ | $0.8020 \pm 0.0024$ | 0.8010 |
| 1.0 | $0.7699 \pm 0.0044$ | $0.7649 \pm 0.0048$ | 0.7689 |
| 9.0 | $0.7478 \pm 0.0046$ | $0.7448 \pm 0.0054$ | 0.7444 |
| 8.5 | $0.7251 \pm 0.0066$ | $0.7187 \pm 0.0111$ | 0.7030 |
| 8.0 | $0.7052 \pm 0.0082$ | $0.7002 \pm 0.0063$ | 0.6926 |
| 7.8 | $0.7022 \pm 0.0087$ | $0.6951 \pm 0.0060$ | 0.6857 |
| 7.6 | $0.6865 \pm 0.0047$ | $0.6857 \pm 0.0098$ | 0.6772 |
| 7.4 | $0.6781 \pm 0.0042$ | $0.6789 \pm 0.0077$ | 0.6660 |
| 7.0 | $0.6670 \pm 0.0043$ | $0.6643 \pm 0.0073$ | 0.6379 |
| 6.0 | $0.6380 \pm 0.0030$ | $0.6378 \pm 0.0030$ | 0.5725 |
| 4.0 | $0.5734 \pm 0.0028$ | $0.5742 \pm 0.0018$ | 0.5027 |
| 2.5 | $0.5008 \pm 0.0021$ | - |  |

Table S1: Monte Carlo simulation results for 196 RCHS with $\zeta=0.01$ obtained by compression and expansion runs. The results are compared with the simulations results of the system of 196 perfect hard-squares reported by Wojciechowski and Frenkel. ${ }^{9}$

## 3 Results for RCHS with $L^{*}=0.25(\zeta=0.8)$



Figure S2: Equation of state for 400 RCHS with $L^{*}=0.25(\zeta=0.8)$ obtained by compression (left panel) and expansion (right panel) runs. (Top panel) The pressure, $P^{*}$, and the isothermal compressibility, $\kappa_{T}^{*}$, as a function of the packing fraction $\eta$. (Bottom panel) Bond orientational order parameters, $\Psi_{4}$ and $\Psi_{6}$, orientational order parameter, $\Phi_{4}$, and susceptibilities of the bond-order parameters, $\chi_{4}$ and $\chi_{6}$, as a function of $\eta$. Vertical dashedlines are used to delimit the different phases.

## 4 Results for RCHS with $L^{*}=0.50(\zeta=0.667)$





Figure S3: Equation of state for 400 RCHS with $L^{*}=0.50(\zeta=0.667)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.


Figure S4: Equation of state for 1600 RCHS with $L^{*}=0.50(\zeta=0.667)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.


Figure S5: Equation of state for 4096 RCHS with $L^{*}=0.50(\zeta=0.667)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.

## 5 Results for RCHS with $L^{*}=0.75(\zeta=0.571)$





Figure S6: Equation of state for 400 RCHS with $L^{*}=0.75(\zeta=0.571)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.


Figure S7: Equation of state for 1600 RCHS with $L^{*}=0.75(\zeta=0.571)$ obtained by compression runs. Legend as in Fig. S2.

## 6 Results for RCHS with $L^{*}=1.00(\zeta=0.5)$






Figure S8: Equation of state for 400 RCHS with $L^{*}=1.00(\zeta=0.5)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.

## 7 Results for RCHS with $L^{*}=1.25(\zeta=0.444)$



Figure S9: Equation of state for 400 RCHS with $L^{*}=1.25(\zeta=0.444)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.

## 8 Results for RCHS with $L^{*}=1.50(\zeta=0.400)$






Figure S10: Equation of state for 400 RCHS with $L^{*}=1.50(\zeta=0.400)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.

## 9 Results for RCHS with $L^{*}=1.75$



Figure S11: Equation of state for 400 RCHS with $L^{*}=1.75(\zeta=0.364)$ obtained by compression runs. Legend as in Fig. S2.

## 10 Results for RCHS with $L^{*}=2.00$



Figure S12: Equation of state for 400 RCHS with $L^{*}=2.00(\zeta=0.333)$ obtained by compression runs. Legend as in Fig. S2.


Figure S13: Equation of state for 4096 RCHS with $L^{*}=2.00(\zeta=0.333)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.

## 11 Results for RCHS with $L^{*}=2.25(\zeta=0.308)$



Figure S14: Equation of state for 400 RCHS with $L^{*}=2.25(\zeta=0.308)$ obtained by compression runs. Legend as in Fig. S2.


Figure S15: Equation of state for 400 RCHS with $L^{*}=2.25(\zeta=0.308)$ obtained by compression runs. During the simulations, only re-orientations of less than $5^{\circ}$ were allowed. The EoS for the system without restrictions during the rotational moves (S14) is shown (continuous curve) for comparison. Legend as in Fig. S2.

## 12 Results for RCHS with $L^{*}=2.50(\zeta=0.286)$





Figure S16: Equation of state for 400 RCHS with $L^{*}=2.50(\zeta=0.286)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.


Figure S17: Equation of state for 1600 RCHS with $L^{*}=2.50(\zeta=0.286)$ obtained by compression runs. Legend as in Fig. S2.



Figure S18: Equation of state for 4096 RCHS with $L^{*}=2.50(\zeta=0.286)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.

## 13 Results for RCHS with $L^{*}=3.00(\zeta=0.25)$





Figure S19: Equation of state for 400 RCHS with $L^{*}=3.0(\zeta=0.25)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.

## 14 Results for RCHS with $L^{*}=5.00$



Figure S20: Equation of state for 400 RCHS with $L^{*}=5.0(\zeta=0.167)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.

## 15 Results for RCHS with $L^{*}=10.00(\zeta=0.09)$





Figure S21: Equation of state for 400 RCHS with $L^{*}=10.0(\zeta=0.09)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.

16 Results for RCHS with $L^{*}=100.00(\zeta=0.01)$





Figure S22: Equation of state for 400 RCHS with $L^{*}=100.0(\zeta=0.01)$ obtained by compression (left panel) and expansion (right panel) runs. Legend as in Fig. S2.

## 17 Lattice angles for the densest rhombic phase



Figure S23: Lattice angle of the densest rhombic phase as a function of $L^{*}(\zeta)$, obtained from the simulations of RCHS using the method of Filio et al. ${ }^{7}$ employing four particles.

## References

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