

## Supporting information

### Membrane elastic energy

We assume that the membrane elastic energy is minimized at zero curvature. The membrane elastic energy is then expressed by

$$E_{bound} = \kappa_{bound} H_{bound}^2 A_{bound} \quad (4)$$

$$E_{swell} = \kappa_{swell} H_{swell}^2 A_{swell} \quad (5)$$

where  $\kappa_i$  and  $A_i$  denote the bending rigidity and area, respectively, of a state  $i$ , and  $H_i$  represents the mean curvature of the membrane of the state  $i$ . We also assume energy storage around the hole, which is expressed by

$$E_h = \frac{\lambda(H_{bound} + H_{bound,max})}{2\pi(r_p - r_{swell})} \quad (6)$$

The volume of the buffer solution contained in a vesicle is approximately expressed as

$$V_{swell} = \pi r_{swell}^2 \times 2\pi r_p = 2\pi^2 \left( \frac{1}{2H_{swell}} \right)^2 r_p \quad (a1)$$

Parameters  $r_{swell}$  and  $r_p$  are shown in Figure 7a. Thus,  $E_{swell}$  may be rewritten as

$$E_{swell} = \kappa_{swell} \frac{\pi^2 r_p}{2V_{swell}} A_{swell} \quad (a2)$$

$H_{bound}$  and  $r_p$  are dependent on each other by a geometric constraint:

$$r_p = \left( \frac{A_{bound}}{\pi} \right)^{1/2} \left( 1 - \frac{A_{bound} H_{bound}^2}{4\pi} \right)^{1/2} \quad (a3)$$

Here we use

$$\sin \theta = \frac{r_p}{r_{bound}}, \quad A_{bound} = 2\pi r_{bound}^2 (1 - \cos \theta)$$

The first equation is an approximation. Using eq. a3,  $E_{swell}$  and  $E_h$  are expressed by

$$E_{swell} = \kappa_{swell} \frac{\pi^{3/2} A_{swell} A_{bound}^{1/2}}{2 V_{swell}} \left( 1 - \frac{A_{bound} H_{bound}^2}{4\pi} \right)^{1/2} \quad (a4)$$

$$E_h^{-1} = 2\pi(\lambda(H_{bound} + H_{bound,max}))^{-1} r_p \left\{ 1 - \left( \frac{V_{swell}}{2\pi^2} \right)^{1/2} \left( \frac{A_{bound}}{\pi} \right)^{-3/4} \left( 1 - H_{bound}^* \right)^{-3/4} \right\} \quad (a5)$$

Here we introduce

$$H_{bound}^* = \frac{A_{bound} H_{bound}^2}{4\pi}, \quad p_A^* = \frac{A_{swell} A_{bound}^{1/2}}{V_{swell}} \quad (a6)$$

to obtain

$$\begin{aligned} E^* &= \frac{E_{bound} + E_{swell} + E_h}{2\pi\kappa_{swell}} \\ &= 2\kappa^* H_{bound}^* + \frac{\sqrt{\pi}}{4} p_A^* \left( 1 - H_{bound}^* \right)^{1/2} \\ &\quad + \frac{\lambda^* (H_{bound,max}^* + H_{bound}^*)}{2\pi} \frac{1}{\left( 1 - H_{bound}^* \right)^{1/2}} \frac{1}{1 - \frac{1}{\pi^{1/4}} \frac{1}{(2r_A^* p_A^*)^{1/2}} \left( 1 - H_{bound}^* \right)^{-3/4}} \end{aligned} \quad (a7)$$

where  $E^* = (E_{bound} + E_{swell} + E_h) / (2\pi\kappa_{swell})$ , and dimensionless bending rigidity is defined as  $\kappa^* = \kappa_{bound} / \kappa_{swell}$ .

$V_{swell}$  given by eq. a1 and is conserved. Eqs. a1 and a3 yield

$$r_{swell} = \frac{1}{2H_{swell}} = \frac{V_{swell}^{1/2}}{\sqrt{2}\pi} \left( \frac{A_{bound}}{\pi} \right)^{-1/4} \left( 1 - \frac{A_{bound}}{4\pi} H_{bound}^2 \right)^{-1/4} \quad (a8)$$

Using eqs. a3 and a8, we obtain

$$A_{swell} = 2\pi r_{swell} 2\pi r_p = 2\sqrt{2}\pi V_{swell}^{1/2} \left( \frac{A_{bound}}{\pi} \right)^{1/4} \left( 1 - \frac{A_{bound}}{4\pi} H_{bound}^2 \right)^{1/4} \quad (a9)$$

Eqs. a6 and a9 give

$$p_A^* = 8\sqrt{\pi^3} r_A^* \left( 1 - H_{bound}^* \right)^{1/2} \quad (a10)$$

where  $r_A^*$  is defined as  $A_{bound} / A_{swell}$ .

The substitution of eq. a10 for  $p_A^*$  in eq. a7 gives

$$E^* = 2\kappa^* H_{bound}^* + 2\pi^2 r_A^* \left( 1 - H_{bound}^* \right) + \frac{\lambda^* (H_{bound,max}^* + H_{bound}^*)}{2\pi} \frac{1}{\left( 1 - H_{bound}^* \right)^{1/2}} \frac{1}{1 - \frac{1}{4\pi r_A^*} \frac{1}{1 - H_{bound}^*}} \quad (a11)$$

which generates eq. 7 in the main text.

The total area of the membrane ( $A_{\text{total}}$ ) is conserved. The equation  $A_{\text{total}} = A_{\text{swell}} + 2A_{\text{bound}}$ , eq. a9 and  $r_A^* = A_{\text{bound}} / A_{\text{swell}}$  yield eqs. 9c and 9d in the main text. Here we used  $\alpha_{\text{swell}}^* = 1 - 2\alpha_{\text{bound}}^*$ , that is derived from  $A_{\text{swell}} = A_{\text{total}} - 2A_{\text{bound}}$ .