Supporting Information

# In-situ Formation of LDH Membranes of Different Microstructure with Molecular Sieve Gas Selectivity

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### SI-1 EDXS measurement within the substrate pores of the

### ab-oriented NiAl-CO<sub>3</sub> LDH membrane



Fig. S1 EDXS of the cross-section of the *ab*-oriented NiAl-CO<sub>3</sub> LDH membrane.

# SI-2 Powder XRD pattern of NiAl-CO<sub>3</sub> LDHs



**Fig. S2** Powder XRD pattern of NiAl-CO<sub>3</sub> LDHs which were synthesized according to the published recipe (M. Wei, X. Y. Xu, X. R. Wang, F. Li, H. Zhang, Y. L. Lu, M. Pu, D. G. Evans and X. Duan, *Eur. J. Inorg. Chem.*, 2006, 2831).

SI-3 EDXS of the top side of the randomly oriented NiAl-CO<sub>3</sub>

# LDH membrane



Fig. S3 Surface EDXS of the randomly oriented NiAl-CO<sub>3</sub> LDH membrane.

### SI-4 Calculation of the concentration of CO<sub>2</sub> in different

### precursor solutions

According to *Henry's Law*: At a constant temperature, the amount of a given gas that dissolves in a given type and volume of liquid is directly proportional to the partial pressure of that gas in equilibrium with that liquid.

Herny's Law is well-known and can be expressed as follow:

$$c_{aq} = k_H \cdot p$$

 $c_{aq}$ : concentration of gas component in solution (molL<sup>-1</sup>);  $k_{\rm H}$ : Henry's Constant (molL<sup>-1</sup>Pa<sup>-1</sup>); p: Partial pressure of gas above the solution (Pa).

The  $k_{\rm H}$  value for CO<sub>2</sub> in water is available. For instance, when the temperature is between 273 K 303 K, the  $k_{\rm H}$  value is  $3.4 \times 10^{-7}$  molL<sup>-1</sup>Pa<sup>-1</sup> (J. A. Dean, *Lange's Handbook of Chemistry*, McGraw-Hill, Inc., 1992).

CO<sub>2</sub> exists in Earth's atmosphere as a trace gas at a concentration of 0.039 % by volume. Data were obtained from the Earth System Research Laboratory, Global Monitoring Division (website: <u>www.ersl.nogg.gov/gmd/ccgg/trends/#mlo</u>). Data were collected on Oct. 2013

For the aged DI water, the concentration of dissolved  $CO_2$  in water is calculated as follow:

(aged DI water)  $c_{aq}$ =3.4×10<sup>-7</sup>×1.01×10<sup>5</sup>×3.9×10<sup>-4</sup> mol/L=1.3×10<sup>-5</sup> mol/L.

For the CO<sub>2</sub>-saturated water, the concentration of dissolved CO<sub>2</sub> in water is calculated as follow:

(CO<sub>2</sub>-saturated water)  $c_{aq}$ =3.4×10<sup>-7</sup>×1.01×10<sup>5</sup> mol/L=3.4×10<sup>-2</sup> mol/L.

These data are used in the main text to evaluate the influence of concentration of dissolved  $CO_2$  on the microstructure and gas separation performance of prepared LDH membranes.

# SI-5 Magnified cross-sectional images of the NiAl-CO<sub>3</sub> LDH layer with CO<sub>2</sub>-saturated water as solvent



**Fig. S4** (a) and (b) SEM image of cross-sectional images of LDH layer in-situ grown on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> modified asymmetric  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> substrate with CO<sub>2</sub>-saturated water as solvent. Hydrothermal growth was kept at 85 °C for 40 h.

Fig. S4 showed the magnified images of the cross-sectional images of NiAl-CO<sub>3</sub> LDH membranes prepared with CO<sub>2</sub>-saturated water as solvent. Unlike the LDH membrane prepared with aged DI water as the solvent, no plate-like morphology characteristic of LDH crystallites was observed, implying that a well-intergrown LDH membrane was formed before LDH crystallites had a chance to evolve with specific crystal faces.

# SI-6 Demonstration of the gas separation equipment



**Fig. S5** Measurement equipment for both single and mixed gas permeation. MFC: mass flow controller; PC: permeation cell with mounted membrane; GC: gas chromatograph; f: volumetric flow rate; p: pressure.

### SI-7 Detailed information on the composition and flux of feed,

### retentate and permeate during the gas permeability tests

### For *ab*-oriented NiAl-CO<sub>3</sub> LDH membrane

H<sub>2</sub>/CO<sub>2</sub> mixture:

Feed side: H<sub>2</sub>: 50.00 ml/min; CO<sub>2</sub>: 50.00 ml/min; H<sub>2</sub>/CO<sub>2</sub>=1.00.
Permeate side: H<sub>2</sub>: 0.89 ml/min; CO<sub>2</sub>: 0.15 ml/min; H<sub>2</sub>/CO<sub>2</sub>=5.80.
Retentate side: H<sub>2</sub>: 49.11 ml/min; CO<sub>2</sub>: 49.85 ml/min. H<sub>2</sub>/CO<sub>2</sub>=0.99.

 $H_2/N_2$  mixture:

H<sub>2</sub>/CH<sub>4</sub> mixture:

Feed side:	H <sub>2</sub> :	50.00 ml/min; CH <sub>4</sub> : 50.00 ml/min; H <sub>2</sub> /CH <sub>4</sub> =1.00.
Permeate sid	le:	H <sub>2</sub> : 1.02 ml/min; CH <sub>4</sub> : 0.12 ml/min; H <sub>2</sub> /CH <sub>4</sub> =8.80.
Retentate sid	le:	H <sub>2</sub> : 48.98 ml/min; CH <sub>4</sub> : 49.88 ml/min. H <sub>2</sub> /CH <sub>4</sub> =0.98.

#### For randomly oriented NiAl-CO<sub>3</sub> LDH membrane

H<sub>2</sub>/CO<sub>2</sub> mixture:

Feed side: H	H <sub>2</sub> : 50.00 ml/min; CO <sub>2</sub> : 50.00 ml/min; H <sub>2</sub> /CO <sub>2</sub> =1.00.
Permeate side	: H <sub>2</sub> : 0.30 ml/min; CO <sub>2</sub> : 0.03 ml/min; H <sub>2</sub> /CO <sub>2</sub> =10.70.
Retentate side	:: H2: 49.70 ml/min; CO2: 49.97 ml/min. H2/CO2=0.99.

H<sub>2</sub>/N<sub>2</sub> mixture:

H<sub>2</sub>/CH<sub>4</sub> mixture:

Feed side:  $H_2$ : 50.00 ml/min;  $CH_4$ : 50.00 ml/min;  $H_2/CH_4=1.00$ . Permeate side:  $H_2$ : 0.82 ml/min;  $CH_4$ : 0.01 ml/min;  $H_2/CH_4=78.70$ . Retentate side:  $H_2$ : 49.18 ml/min;  $CH_4$ : 49.99 ml/min.  $H_2/CH_4=0.98$ .

### For randomly oriented ZnAl-NO<sub>3</sub> LDH membrane

H<sub>2</sub>/CO<sub>2</sub> mixture:

Feed side:  $H_2$ : 50.00 ml/min;  $CO_2$ : 50.00 ml/min;  $H_2/CO_2=1.00$ . Permeate side:  $H_2$ : 0.64 ml/min;  $CO_2$ : 0.11 ml/min;  $H_2/CO_2=5.80$ . Retentate side: H2: 49.36 ml/min; CO2: 49.89 ml/min.  $H_2/CO_2=0.99$ .

 $H_2/N_2$  mixture:

Feed side: H	<sub>2</sub> : 50.00 ml/min; N <sub>2</sub> : 50.00 ml/min; H <sub>2</sub> /N <sub>2</sub> =1.00.
Permeate side:	H <sub>2</sub> : 0.71 ml/min; N <sub>2</sub> : 0.08 ml/min; H <sub>2</sub> /N <sub>2</sub> =9.00.
Retentate side:	H <sub>2</sub> : 49.29 ml/min; N <sub>2</sub> : 49.92 ml/min. H <sub>2</sub> /N <sub>2</sub> =0.99.

H<sub>2</sub>/CH<sub>4</sub> mixture:

Feed side:	H <sub>2</sub> :	50.00 ml/min; CH <sub>4</sub> : 50.00 ml/min; H <sub>2</sub> /CH <sub>4</sub> =1.00.
Permeate sid	le:	H <sub>2</sub> : 0.66 ml/min; CH <sub>4</sub> : 0.05 ml/min; H <sub>2</sub> /CH <sub>4</sub> =8.80.
Retentate sid	le:	H <sub>2</sub> : 49.34 ml/min; CH <sub>4</sub> : 49.95 ml/min. H <sub>2</sub> /CH <sub>4</sub> =0.99.

SI-8 The relationship between operation temperature and gas permeation behavior of the H<sub>2</sub>/CH<sub>4</sub> mixture



Fig. S6 H<sub>2</sub> Permeance and the separation factor of equimolecular H<sub>2</sub>/CH<sub>4</sub> mixture on ZnAl-NO<sub>3</sub> LDH membrane as a function of temperature.  $\Delta P = 1$  bar.

SI-9 Thermal stability of prepared ZnAl-NO<sub>3</sub> LDH membrane



**Fig. S7** Thermal stability test on prepared ZiAl-NO<sub>3</sub> LDH membrane. Equimolecular  $H_2/CH_4$  mixture was used as feed gas. Test conditions:  $\Delta P = 1$  bar. T = 180 °C.