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### **Supporting Information**

# Highly Hydrogen Permselective ZIF-8 Membranes Supported on Polydopamine Functionalized Macroporous Stainless-Steel-Nets

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**Figure S1.** Photography of the SSN wafer (a), PDA-functionalized SSN wafer (b), and ZIF-8 membrane supported on PDA-functionalized SSN wafer (c).



**Figure S2.** FESEM image of the ZIF-8 membrane layer prepared on PDA-functionalized SSN after 10 minutes ultrasonic treatment.



**Figure S3**. Top view FESEM image of the zeolite LTA membrane supported on PDA-functionalized SSN prepared at 60 °C for 24 h.



**Figure S4**.  $H_2/CH_4$  selectivity and permeances of the ZIF-8 membrane prepared on PDA-functionalized SSN as function of the  $H_2$  partial pressure at 100 °C.

**Table S1.** Single and mixed gases permeances and separation factors for the ZIF-8 membrane prepared on PDA-functionalized SSN at 100 °C and 1 bar (in mixed gases permeation, equimolar mixtures have been used).

		Separation performances of the ZIF-8 membrane supported on PDA-functionalized SSN						
Gas <sub>i/j</sub>	Knudsen constant	Single gas			Mixed gases			
		Permeances(i) (mol/m <sup>2</sup> ·S <sup>1</sup> ·Pa <sup>1</sup> )	$\begin{array}{l} Permeances(j) \\ (mol/m^2 \cdot S^1 \cdot Pa^1) \end{array}$	ISF	$\begin{array}{l} Permeances(i) \\ (mol/m^2 \cdot S^1 \cdot Pa^1) \end{array}$	$\begin{array}{l} Permeances(j) \\ (mol/m^2 \cdot S^1 \cdot Pa^1) \end{array}$	SF	
$\mathrm{H_2/CO_2}$	4.7	2.66 x 10 <sup>-5</sup>	3.02 x 10 <sup>-6</sup>	8.8	2.38 x 10 <sup>-5</sup>	2.94 x 10 <sup>-6</sup>	8.1	
$H_2/N_2$	3.7	2.66 x 10 <sup>-5</sup>	1.73 x 10 <sup>-6</sup>	15.4	2.46 x 10 <sup>-5</sup>	1.64 x 10 <sup>-6</sup>	15.0	
$\mathrm{H_2/CH_4}$	2.8	2.66 x 10 <sup>-5</sup>	1.08 x 10 <sup>-6</sup>	24.6	2.35 x 10 <sup>-5</sup>	1.01 x 10 <sup>-6</sup>	23.2	
$H_2/C_3H_8$	4.7	2.66 x 10 <sup>-5</sup>	6.01 x 10 <sup>-8</sup>	442.5	2.12 x 10 <sup>-5</sup>	6.43 x 10 <sup>-8</sup>	329.7	

ISF: ideal separation factor; SF: separation factor.

# Table S2

**Table S2**. Separation performances of ZIF-8 membranes prepared on PDA-functionalized SSN for the separation of equimolar  $H_2/CH_4$  mixtures at 100 °C and 1 bar.

Membrane	$\begin{array}{c} H_2 \text{ permeance} \\ (mol \cdot m^{-2} \cdot s^{-1} \cdot Pa^{-1}) \end{array}$	CH <sub>4</sub> permeance (mol·m <sup>-2</sup> ·s <sup>-1</sup> ·Pa <sup>-1</sup> )	H <sub>2</sub> /CH <sub>4</sub> selectivity	Average selectivity	standard deviation of selectivity
M1	2.30 x 10 <sup>-5</sup>	1.02 x 10 <sup>-6</sup>	22.5		
M2	2.26 x 10 <sup>-5</sup>	9.78x 10 <sup>-7</sup>	23.1	22.57	0.50
M3	2.37 x 10 <sup>-5</sup>	1.07 x 10 <sup>-6</sup>	22.1		

## Table S3

**Table S3.** Comparison of the gas separation performances of the ZIF-8 membrane prepared on

 PDA-functionalized SSN in this study with other zeolite and MOF membranes from literatures.

	Pore size (nm)	Temperatur e (°C)	Mixture as separation performances				
Membrane			Selectivity			H <sub>2</sub> permeances	Reference
			H <sub>2</sub> /CO <sub>2</sub>	H <sub>2</sub> /CH <sub>4</sub>	$H_2/C_3H_8$	$(mol/m^2 \cdot S^1 \cdot Pa^1)$	
DDR	0.36 x 0.44	300	3.5	/	/	7.9 x 10 <sup>-6</sup>	S1
Matrix AlPO <sub>4</sub>	/	35	9.7	/	/	1.1 x 10 <sup>-7</sup>	S2
SAPO-34	0.38	200	23	/	/	7.0 x 10 <sup>-8</sup>	S3
LTA AlPO <sub>4</sub>	0.40	25	7.6	4.3	146	2.5 x 10 <sup>-7</sup>	S4
NaA	0.41	20	6.7	4.9	15.8	2.3 x 10 <sup>-7</sup>	S5
ITQ-29	0.41	300	7.8 <sup>a</sup>	6.2 <i>a</i>	127	3.6 x 10 <sup>-7</sup>	<b>S</b> 6
MOF-5	1.40	/	KD <sup>b</sup>	KD <sup>b</sup>	/	4.7 x 10 <sup>-6</sup>	<b>S</b> 7
HKUST-1	0.90	25	6.8	6	7.0	1.0 x 10 <sup>-6</sup>	<b>S</b> 8
HKUST-1	0.90	25	4.6	3.0	/	6.7 x 10 <sup>-7</sup>	S9
IRMOF-3 <sup>c</sup>	/	25	4.1	2.0	2.4	1.1 x 10 <sup>-6</sup>	S10
MIL-53	0.73 x 0.77	/	5.4	4.0	/	5.0 x 10 <sup>-7</sup>	S11
SIM-1	0.34	25	2.4 <sup>a</sup>	2.6 <i>a</i>	/	8.2 x 10 <sup>-7</sup>	S12
ZIF-7	0.30	200	6.5	5.9	/	8.0 x 10 <sup>-8</sup>	S13
ZIF-8	0.34	25	4.5 <i>a</i>	11.3	/	5.1 x 10 <sup>-8</sup>	S14
ZIF-8	0.34	25	6.0	15	300	1.0 x 10 <sup>-7</sup>	S15
ZIF-8	0.34	23	/	/	545	4.4 x 10 <sup>-7</sup>	S16
ZIF-8	0.34	22	3.9	13.0	474	1.5 x 10 <sup>-6</sup>	S17
ZIF-22	0.29	50	7.2	5.2	/	1.9 x 10 <sup>-7</sup>	S18
ZIF-69	4.4	25	2.7 <sup>a</sup>	3.7 <sup>a</sup>	/	6.50 x 10 <sup>-8</sup>	S19
ZIF-90	0.37	200	7.2 <sup>a</sup>	15.3	/	2.51 x 10 <sup>-7</sup>	S20
ZIF-90	0.37	35	1.8 <i>a</i>	2.7 <sup>a</sup>	/	3.19 x 10 <sup>-8</sup>	S21
ZIF-90 <sup>d</sup>	/	200	15.3	18.9	/	2.02 x 10 <sup>-7</sup>	S22
ZIF-90 <sup>e</sup>	/	225	20.1	70.5	458.3	2.85 x 10 <sup>-7</sup>	S23
ZIF-8	0.34	100	8.1	23.2	329.7	$> 2.1 \times 10^{-5}$	This work

<sup>a</sup> ideal separation factor, <sup>b</sup> Knudsen diffusion, <sup>c</sup> AM6 modified IRMOF-3, <sup>d</sup> ethanolamine modified ZIF-90, <sup>e</sup> APTES modified ZIF-90.

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